

SUMMARY OF AC LOSS MEASUREMENT RESULTS FOR LONG MAGNETS
AT FERMILAB

TS-SSC 92-061

J. P. Ozelis
05/14/92

AC loss measurements have been performed on six 15m SSC Collider dipole magnets built at Fermilab. The losses are determined by using the now-standard technique of simultaneously measuring magnet current and voltage using fast DMM's, and integrating their product over a closed current cycle. The standard current cycle is essentially a sawtooth ramp from 500 to 5000 to 500 Amps, with 5 second dwells at the maximum and minimum currents. Measurements are performed at various ramp rates from 30 to 125 Amps/sec, and are taken for two cycles at each ramp rate.

The loss per cycle is typically plotted as a function of ramp rate. A linear least-squares fit is applied to the data, yielding an intercept that can be identified as the hysteresis loss over the current cycle, and a slope that represents the eddy current heating during the current cycle. The errors of a typical measurement are on the order of 10%, and are generally largest for the low ramp rates, where the long cycle time provides a greater opportunity for noise to affect the measurement.

As eddy current heating is responsible for the degradation in quench current at high ramp rates, it is perhaps useful to try to correlate the eddy current heating (as determined from AC loss measurements) with the ramp rate dependence of the quench current of these magnets. One parameterization of the quench current degradation is the slope of the quench current/ramp rate dependence. This factor is an indication of the strength of the eddy current heating effects. For our purposes, we have calculated this slope using the values of quench current for ramp rates greater than or equal to 50 Amps/sec. At lower ramp rates, the dependence varies from a linear one quite markedly, and exhibits both positive and negative curvature, depending upon cable manufacturer. When ramp rate dependence is plotted as a function of eddy current heating, the result is a monotonically decreasing dependence that suggests a direct, linear relationship between these two parameters, as might be expected.

Analysis of the data from this set of six magnets has indicated the possibility of a systematic non-linearity in the loss/cycle versus ramp rate dependence. It appears that the slope decreases as ramp rate decreases below about 50 Amps/sec. This is especially evident in magnets DCA318 and DCA319. This non-linearity at the low ramp rates may be related to the same process or cable characteristic that accounts for the non-linearity and varying curvature in the low ramp rate sections of the quench current/ramp rate dependence.

The relevant data for these six magnets are tabulated below. Numbers in parentheses are from fits to the data where values below ramp rates of 50 Amps/sec have been excluded.

Magnet	Hysteresis Loss (J)	Eddy Current dependence (J/A/s)	Iq vs I-dot dependence (A/A/s)	Cable Manufacturer
DCA311	614 (266)	15.7 (18.5)	-5.9	Supercon

DCA312	1393 (600)	55.4 (65.1)	-30.0	IGC
DCA314	842 (752)	35.1 (36.2)	-20.4	IGC
DCA315	780 (695)	50.9 (52.0)	-25.3	IGC
DCA318	440 (47)	13.7 (17.6)	-3.4	Oxford
DCA319	445 (209)	14.8 (17.2)	-3.5	Oxford

Standard AC loss measurement cycle : 500 A to 5000 A to 500 A at various ramp rates (30 A/s ---> 125 A/s). A least-squares linear fit is applied to the loss data to yield the above figures. Quench current dependence on ramp rate is obtained by performing a least-squares linear fit to the quench current/ramp rate data for ramp rates ≥ 50 A/sec.

The filenames of various Topdrawer files, and a short description of the plots, are listed below. They reside in the directory `USR$ROOT:[OZELIS.EIED_DATA]`, and have world access.

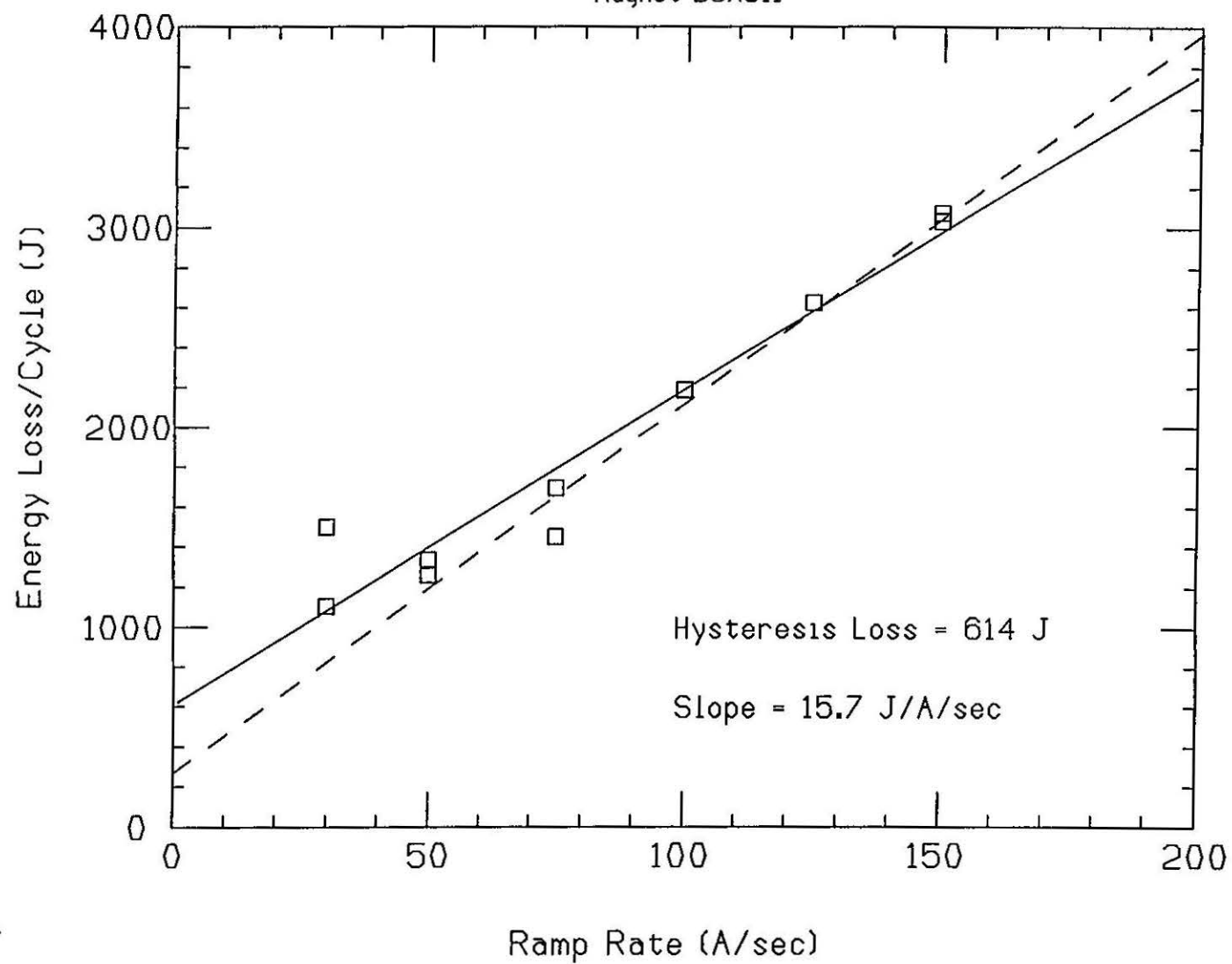
DCA311_SU.TOP	-	AC loss results: ramp rate dependence, magnet DCA311
DCA312_SU.TOP	-	AC loss results: ramp rate dependence, magnet DCA312
DCA314_SU.TOP	-	AC loss results: ramp rate dependence, magnet DCA314
DCA315_SU.TOP	-	AC loss results: ramp rate dependence, magnet DCA315
DCA318_SU.TOP	-	AC loss results: ramp rate dependence, magnet DCA318
DCA319_SU.TOP	-	AC loss results: ramp rate dependence, magnet DCA319

(Note : The solid lines in the six plots above are fits using all of the data, while the dashed lines are fits using only data whose values of $I\dot{}$ are ≥ 50 Amps/sec.)

6LONG_SU.TOP	-	" " , all six magnets
EDDY_LONG.TOP	-	Relationship between eddy current heating and quench dependence on ramp rate, all six magnets
6LONG_SU_50.TOP	-	Same as 6LONG_SU.TOP, except linear fits are for $I\dot{}$ ≥ 50 A/sec data only
EDDY_LONG_50.TOP	-	Same as EDDY_LONG.TOP, except shows both data using only $I\dot{}$ ≥ 50 A/sec values, and using all $I\dot{}$ values in the eddy current heating calculation
DCA_RR.TOP	-	Quench current dependence on ramp rate, for all long magnets (courtesy D. Orris)

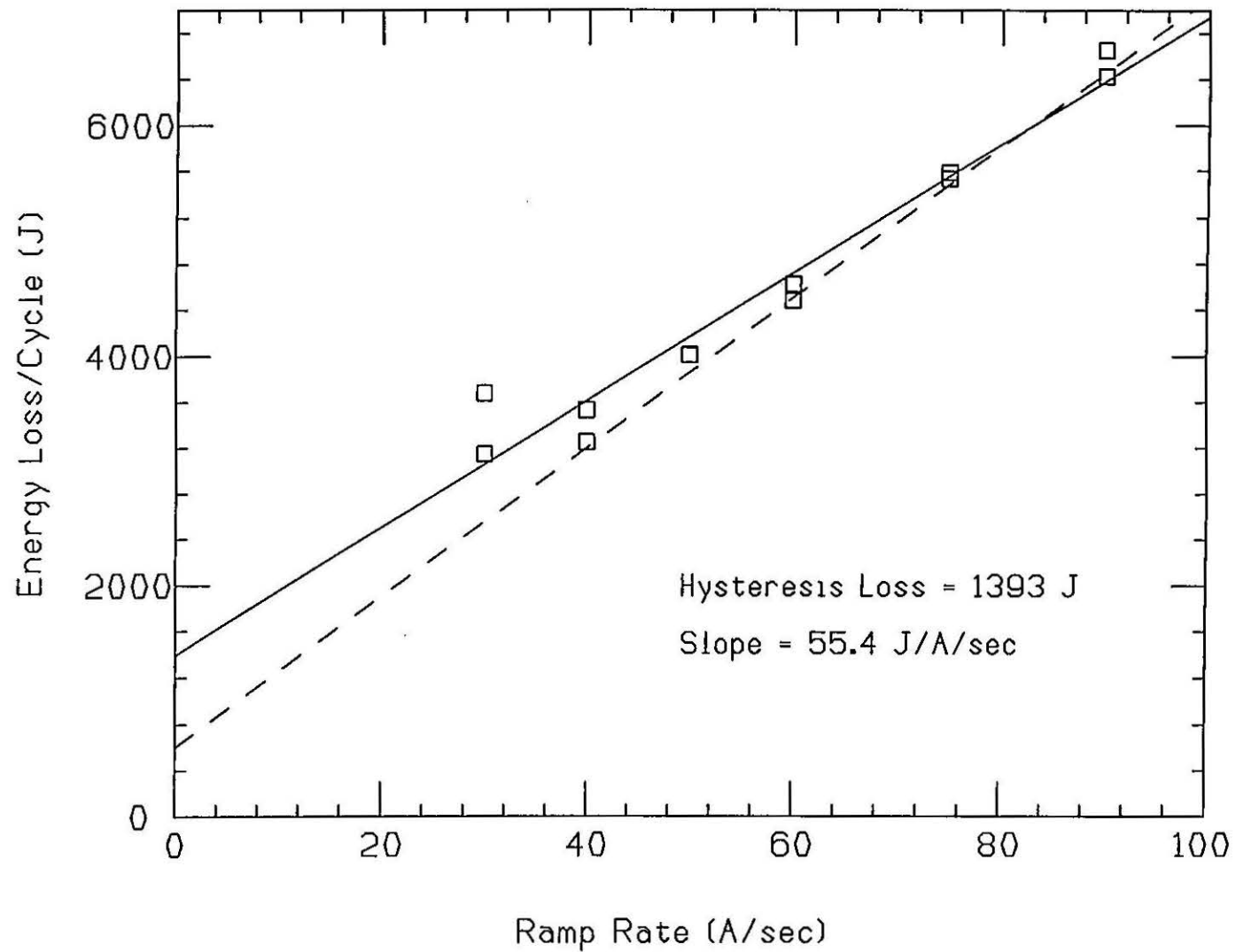
Energy Loss as a Function of Ramp Rate

Magnet DCA311



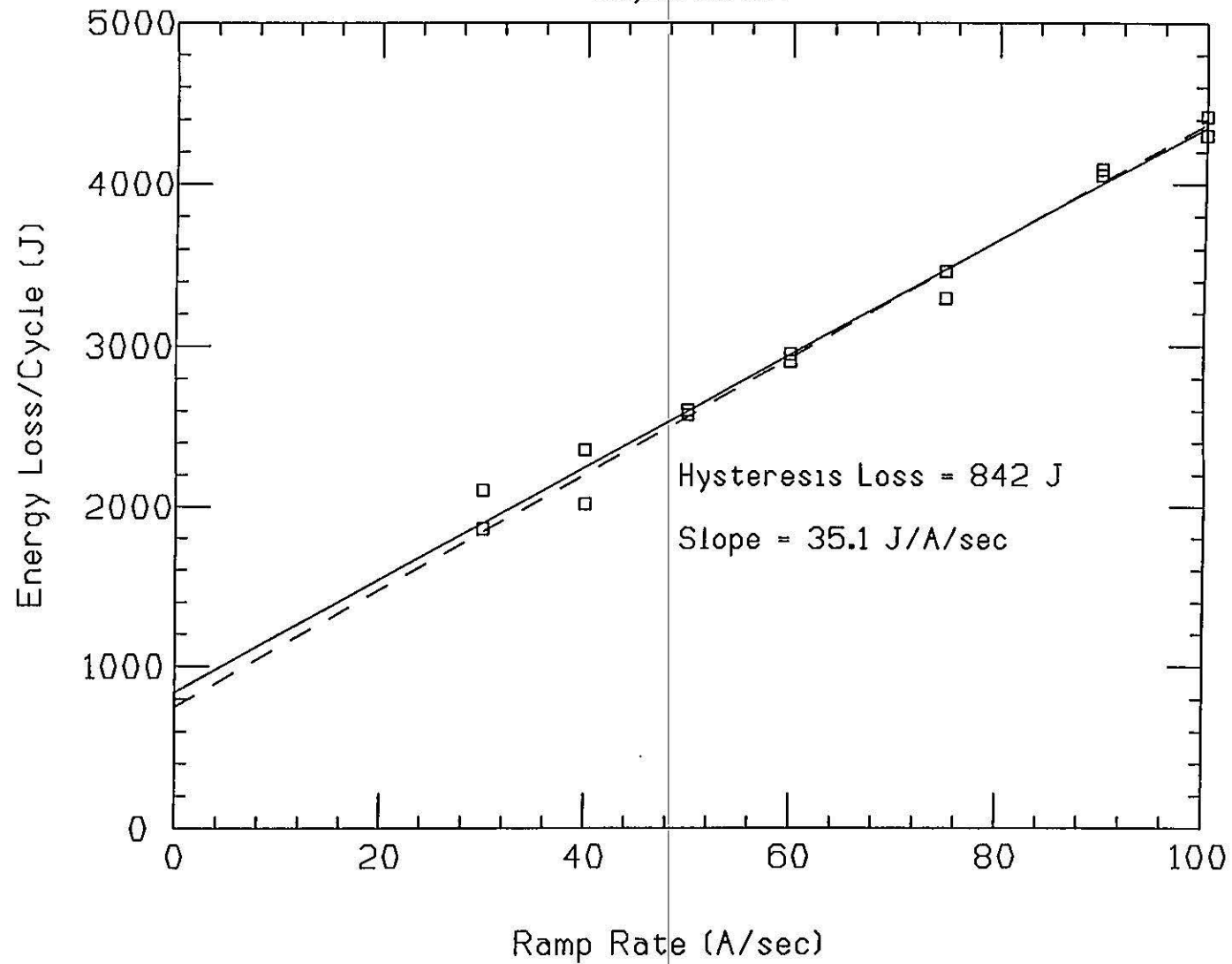
Energy Loss as a Function of Ramp Rate

Magnet DCA312



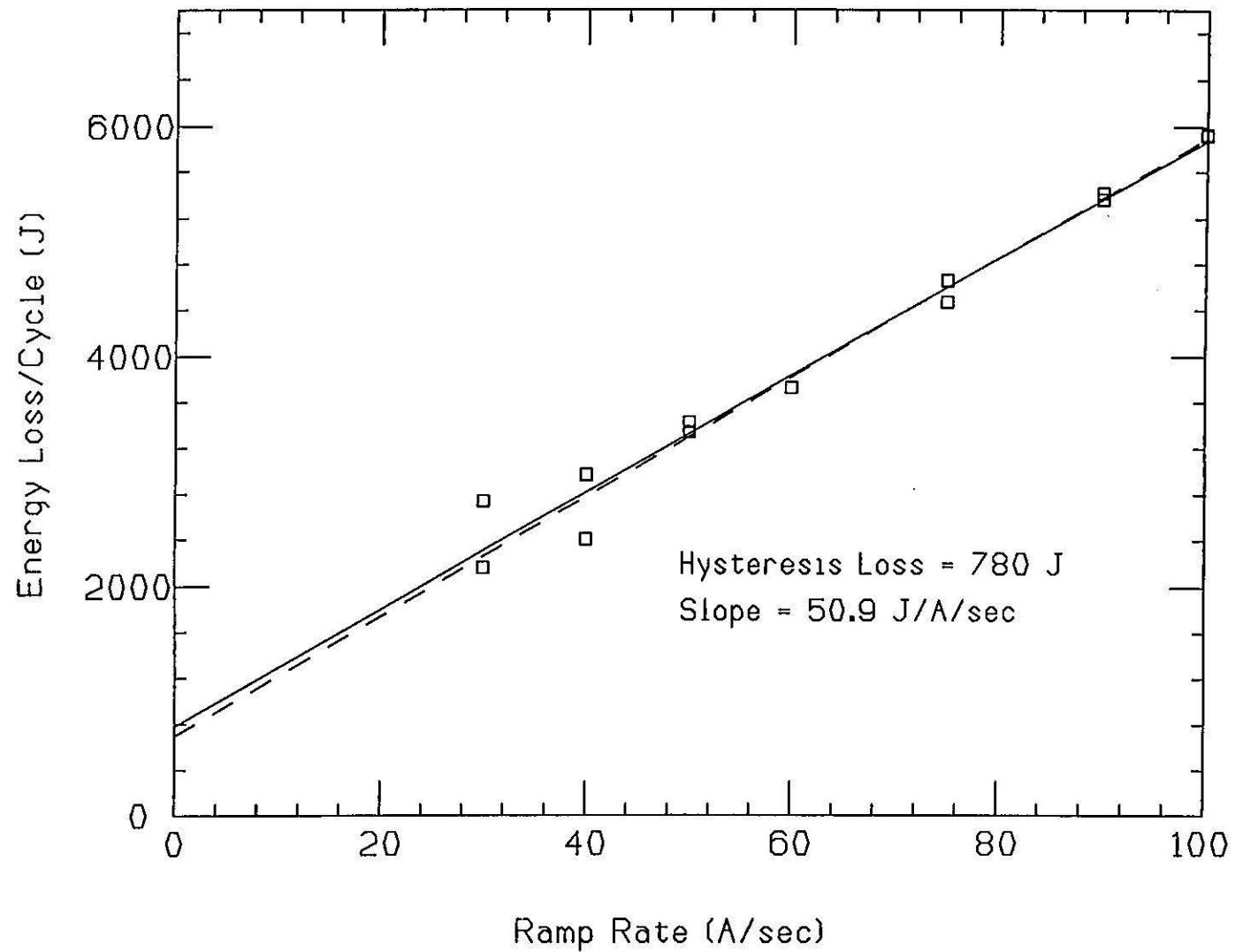
Energy Loss as a Function of Ramp Rate

Magnet DCA314



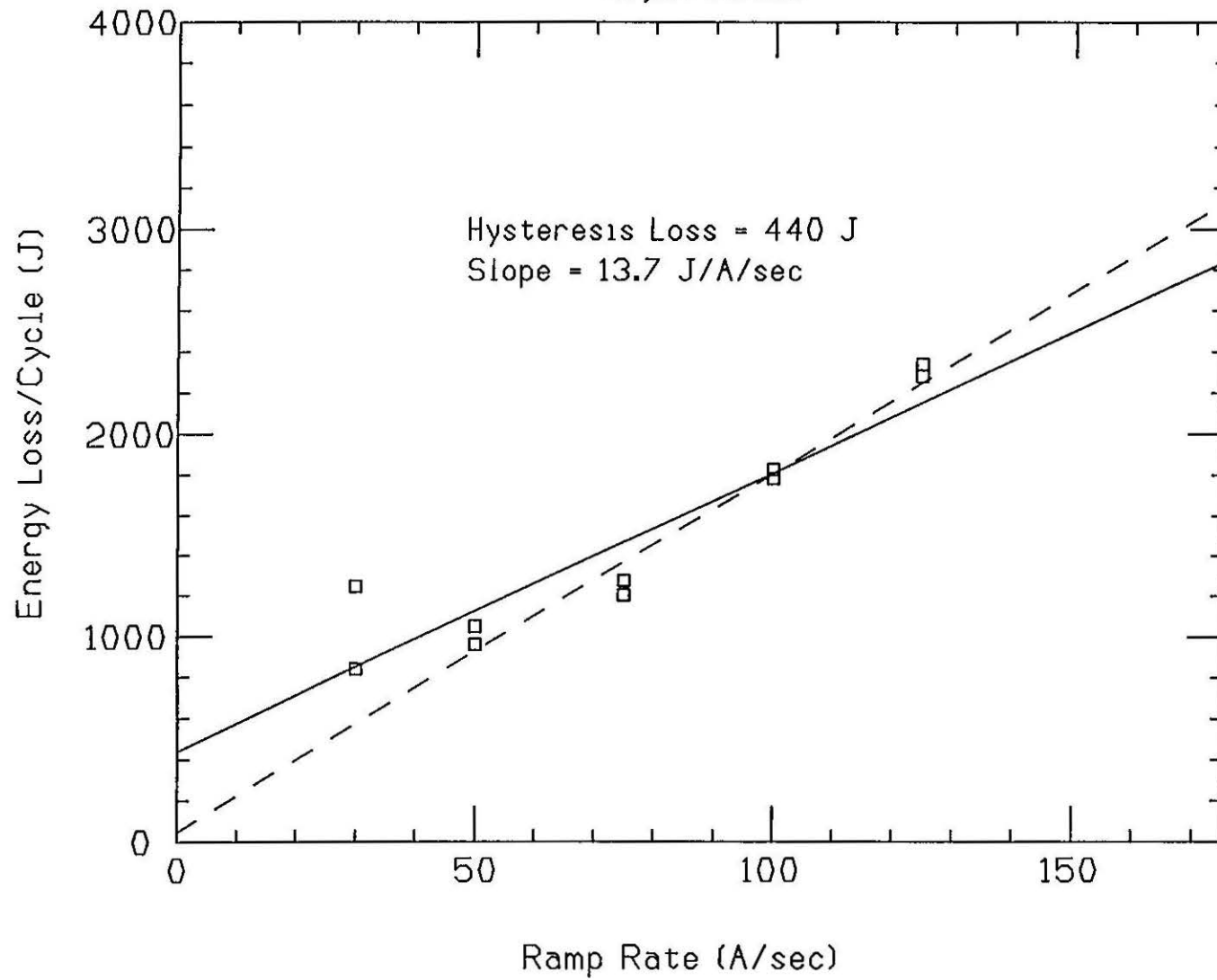
Energy Loss as a Function of Ramp Rate

Magnet DCA315



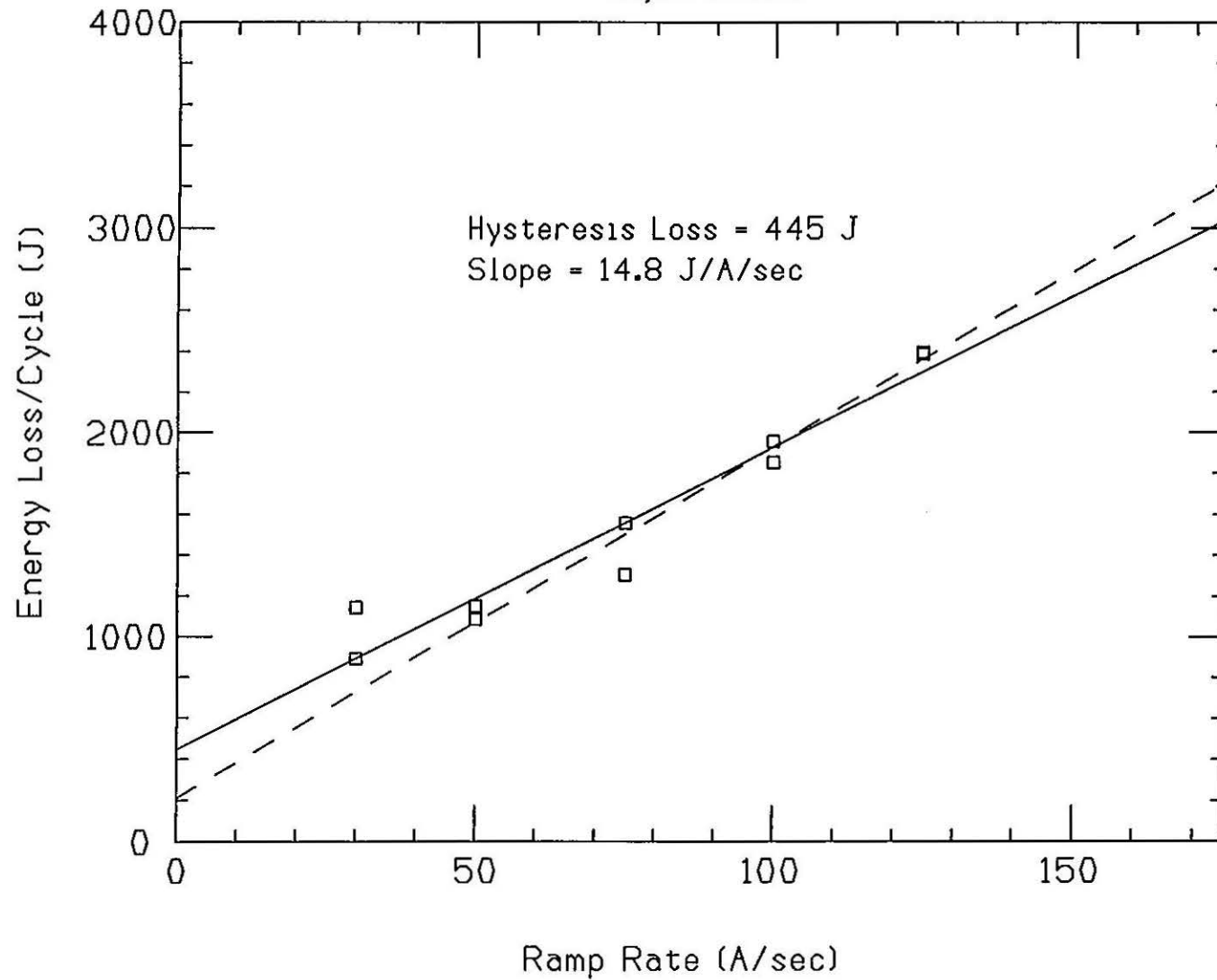
Energy Loss as a Function of Ramp Rate

Magnet DCA318



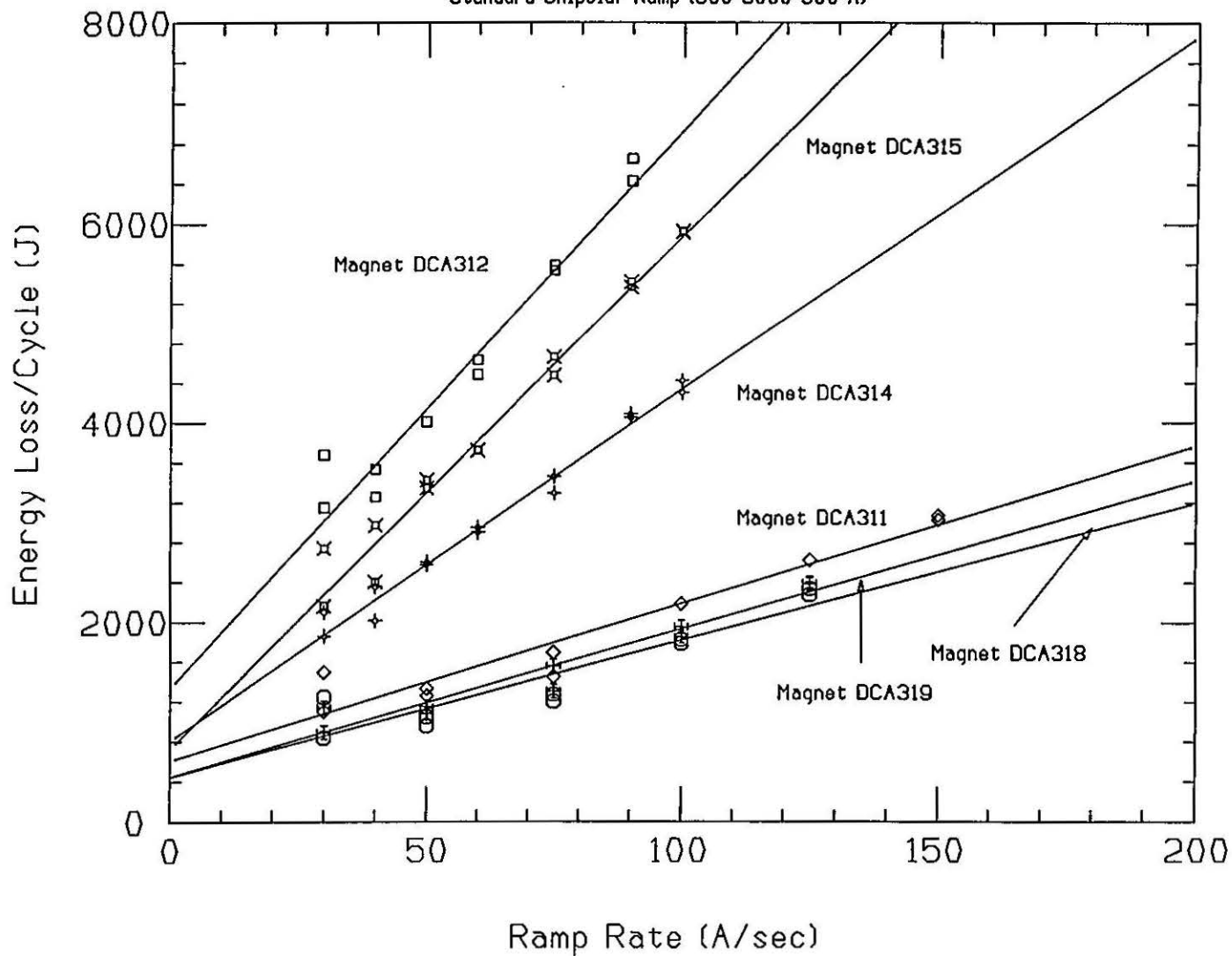
Energy Loss as a Function of Ramp Rate

Magnet DCA319

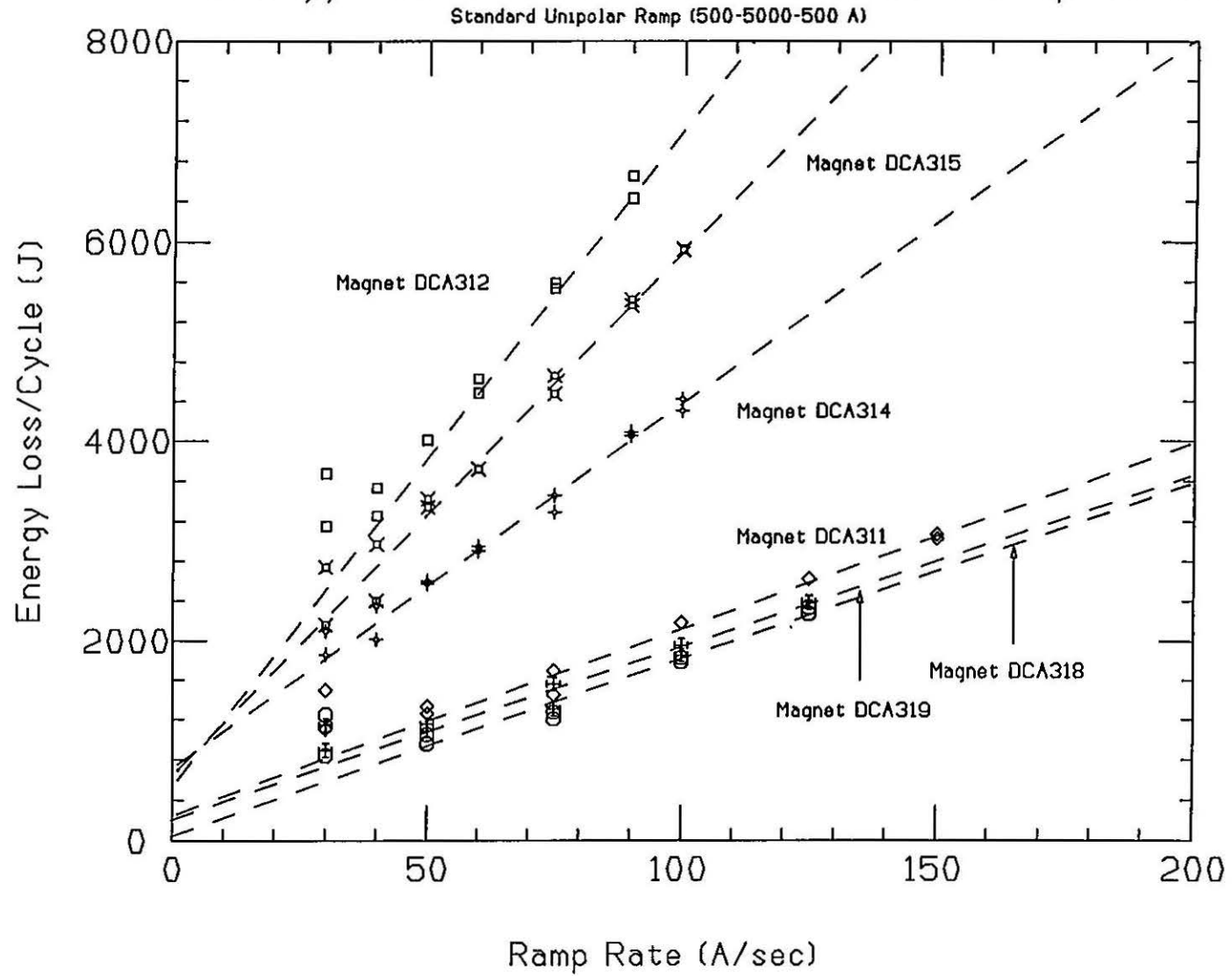


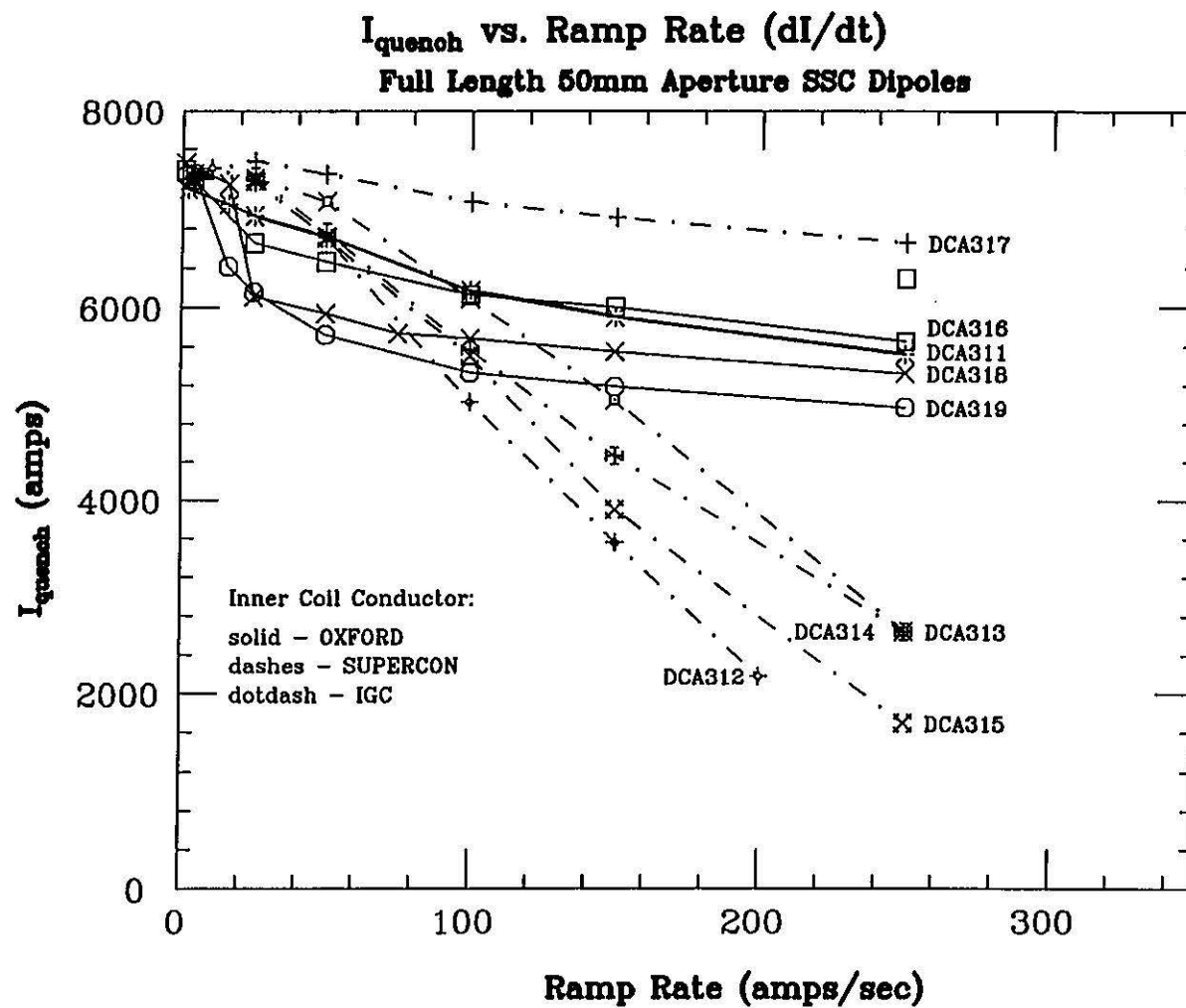
Energy Loss as a Function of Ramp Rate

Standard Unipolar Ramp (500-5000-500 A)

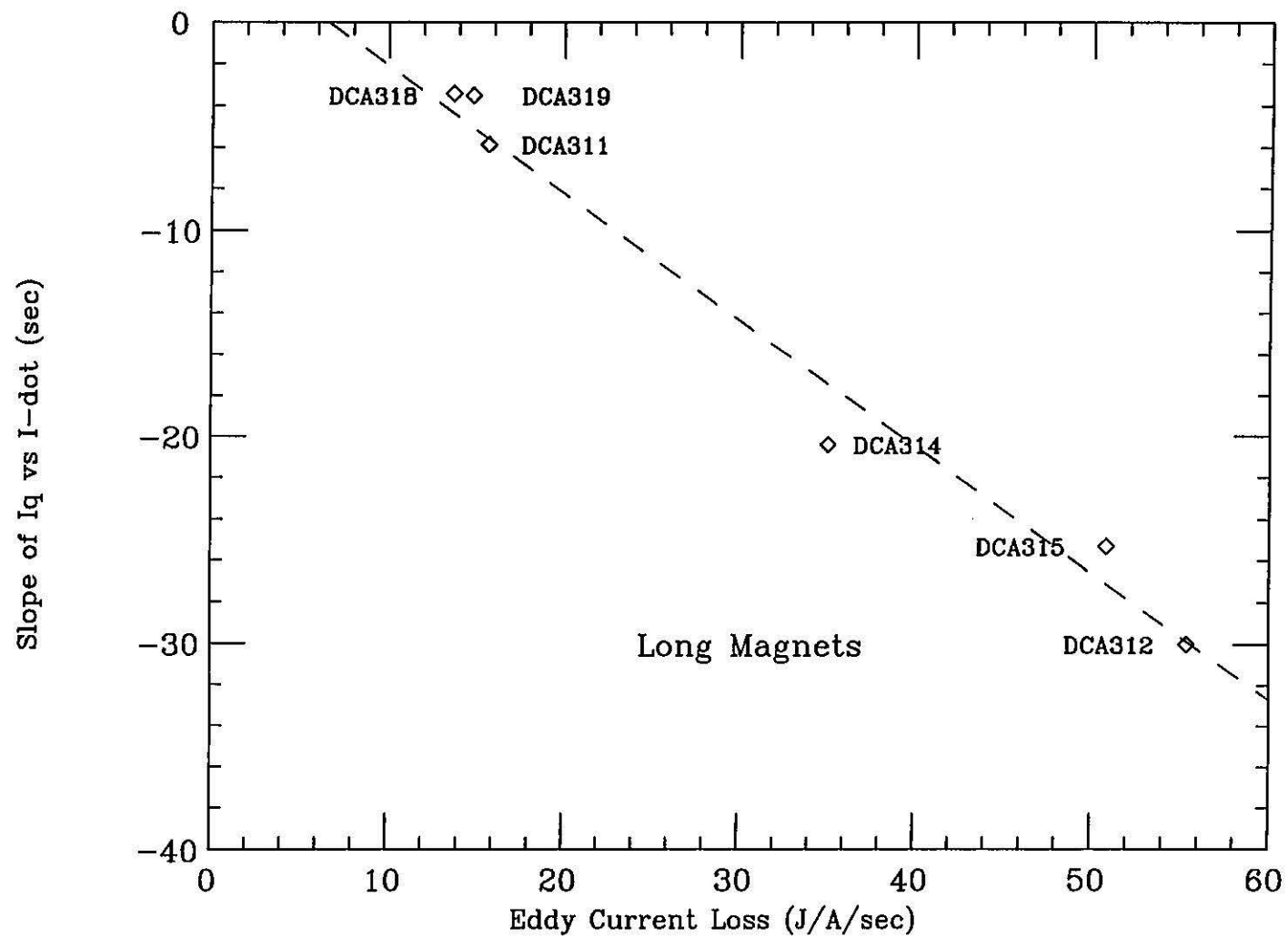


Energy Loss as a Function of Ramp Rate





Relationship Between Eddy Current Heating and I_q



Relationship Between Eddy Current Heating and I_q

