

From: FNAL::JBS 28-MAR-1990 22:31:00.77
To: BOSSERT,CARSON,HANFT,WKOSKA,MANTSCH,MAZUR,PEWITT
CC: MYSELF
Subj: DS0307 and DS0308 preloads explained?

From the measured coil sizes, collar size and amount of Kapton added to the standard ground wrap the expected preload for DS0308 is 8 kpsi in the inner coil and 11 kpsi in the outer coil. The actual prestresses are about 2 and 3 kpsi respectively. This may result from either the coil being smaller than we think it is or the collar cavity being larger than we think it is. The former would result from some as yet not understood systematic error in the coil size measurement. The latter might result from a mis-design or mis-measurement of the collars, poor tolerance on the thickness of the ground insulation or the Kapton ground insulation flowing into the die-break of the collars.

These would have different effects on the harmonics. If the coil is too small but the collar cavity is correct, the coil will require less than the expected prestress but will end up at or near the design location. If, on the other hand, the cavity is too large, the coil will occupy a larger azimuthal space than called for in the magnetic design and therefore the harmonics will be altered.

The measured body field sextupole moment of DS0308 (measurements taken today by Hanft, Koska, et al using the mole) is -6 units. Gerry Morgan calculates that increasing the inner (outer) coil collaring shim by 1 mil increases the sextupole moment by 0.49 (0.41) units. That is, if both the inner and outer coil cavities are 1 mil smaller than the design value, b_2 will be +0.9 units. To generate -6 units would require the inner and outer cavities to be 7 mils too large (assuming an equal error in both).

I put such a collar size error into the spread sheet that is supposed to calculate prestresses from coil sizes. Lo and behold, the predicted prestresses are 2 and 3 kpsi on the inner and outer coils. On the final collaring of DS0307 the measured prestresses are about 5 and 7 kpsi in the inner and outer coils while the predicted prestresses are 11 and 13 kpsi. If I increase the collar cavity by the same 7 mils, the predicted prestresses drop to 5 and 5 kpsi.

The closeness of the agreement between calculation and measurement is probably somewhat fortuitous given all the fine points that I have ignored in this argument. Nonetheless, it suggests that the coil size measurements are more or less correct and that the collar cavity is to blame for the low preload. Stuffing more Kapton at the poles of DS0309 will probably not only increase the preload but also set the harmonics to the correct value. It had been my intention to set the amount of additional Kapton by seeing how much I would have to alter the collars on DS0307 and DS0308 to get the observed preloads. The mole measurement seems to have given me a good way to get the correct value on the first try.

D50308

Pos #	Cell#	106	Magn	DS0308	1/4 sec	Inner	Date	1/6/90	12000			
		5000	5000	coil master								
1		Xxxxxxx	Xxxxxxx	0.0244	0.0198	0.0221	0.0180	0.0200	0.0167	0.0171	0.0152	
2 up		Xxxxxxx	Xxxxxxx	0.0217	0.0185	0.0201	0.0174	0.0185	0.0164	0.0171	0.0152	
2 dn		Xxxxxxx	Xxxxxxx	0.0179	0.0152							
3		Xxxxxxx	Xxxxxxx	0.0190	0.0152							
4		Xxxxxxx	Xxxxxxx	0.0264	0.0196							
5 up		Xxxxxxx	Xxxxxxx	0.0234	0.0191	0.0240	0.0184	0.0214	0.0171	0.0188	0.0155	
5 dn		Xxxxxxx	Xxxxxxx	0.0234	0.0191	0.0216	0.0180	0.0200	0.0167	0.0188	0.0155	
6		Xxxxxxx	Xxxxxxx	0.0170	0.0152							
7		Xxxxxxx	Xxxxxxx	0.0168	0.0152							
8 up		Xxxxxxx	Xxxxxxx	0.0242	0.0192	0.0218	0.0180	0.0194	0.0168	0.0157	0.0158	
8 dn		Xxxxxxx	Xxxxxxx	0.0215	0.0185	0.0195	0.0174	0.0180	0.0164	0.0167	0.0158	
9		Xxxxxxx	Xxxxxxx	0.0160	0.0152							
10		Xxxxxxx	Xxxxxxx	0.0155	0.0152							
11 up		0.0240	0.0192	0.0218	0.0180	0.0194	0.0184	0.0167	0.0167	0.0152	0.0152	
11 dn		0.0213	0.0185	0.0195	0.0174	0.0180	0.0164	0.0167	0.0152			
12		Xxxxxxx	Xxxxxxx	0.0165	0.0152							
13		Xxxxxxx	Xxxxxxx	0.0175	0.0152							
14 up		0.0246	0.0192	0.0221	0.0180	0.0196	0.0168	0.0174	0.0152			
14 dn		0.0220	0.0185	0.0201	0.0174	0.0186	0.0184	0.0174	0.0152			
15		Xxxxxxx	Xxxxxxx	0.0186	0.0152							
16		Xxxxxxx	Xxxxxxx	0.0175	0.0152							
17 up		0.0259	0.0192	0.0286	0.0180	0.0210	0.0188	0.0182	0.0182	0.0153		
17 dn		0.0238	0.0185	0.0214	0.0174	0.0197	0.0184	0.0182	0.0153			
18		Xxxxxxx	Xxxxxxx	0.0175	0.0152							
19		Xxxxxxx	Xxxxxxx	0.0166	0.0152							
20 up		0.0285	0.0192	0.0212	0.0180	0.0188	0.0168	0.0160	0.0160	0.0152		
20 dn		0.0209	0.0185	0.0190	0.0174	0.0178	0.0184	0.0160	0.0160	0.0152		
21		Xxxxxxx	Xxxxxxx	0.0154	0.0152							
22		Xxxxxxx	Xxxxxxx	0.0160	0.0152							
23 up		0.0226	0.0192	0.0208	0.0180	0.0179	0.0168	0.0148	0.0148	0.0152		
23 dn		0.0199	0.0185	0.0180	0.0174	0.0165	0.0164	0.0148	0.0148	0.0152		
24		Xxxxxxx	Xxxxxxx	0.0154	0.0152							
Pos #	6000	9000	10000	12000	S(X=0)	rv	str	avg str				
	coil-master	coil-master	coil-master	coil-master	(collar)	(inner)						
1	0.0061	0.0041	0.0038	0.0019	19.88	6.7	7.9	5.1				
2 up	0.0082	0.0027	0.0021	Xxxxxxx	20.85	7.2	9.1	6.8				
2 dn				Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
3				0.0027	21.72	7.8	9.8	7.9				
4				0.0038	23.59	7.8	11.2	7.7				
5 up	0.0068	0.0057	0.0048	0.0088	22.74	7.4	10.1	7.8				
5 dn	0.0048	0.0036	0.0038	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
6				0.0018	20.18	7.5	7.5	7.5				
7				0.0018	19.88	7.8	7.0	7.9				
8 up	0.0050	0.0038	0.0025	0.0014	19.50	8.9	7.7	8.4				
8 dn	0.0030	0.0021	0.0016	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
9				0.0008	18.48	6.9	6.7	8.2				
10				0.0008	17.68	7.8	5.2	7.8				
11 up	0.0048	0.0038	0.0026	0.0015	19.67	7.2	7.5	7.8				
11 dn	0.0028	0.0021	0.0018	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
12				0.0018	19.88	6.9	7.5	7.7				
13				0.0028	21.03	9.2						
14 up	0.0054	0.0041	0.0028	0.0022	20.96	8.7						
14 dn	0.0035	0.0027	0.0022	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
15				0.0034	22.91							
16				0.0028	21.03							
17 up	0.0067	0.0066	0.0042	0.0029	22.06	10.2						
17 dn	0.0048	0.0040	0.0038	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
18				0.0028	21.08							
19				0.0014	19.50							
20 up	0.0048	0.0082	0.0017	0.0008	18.48							
20 dn	0.0024	0.0016	0.0009	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
21				0.0001	17.28							
22				0.0008	18.48							
23 up	0.0084	0.0028	0.0011	-0.0004	16.48	4.2						
23 dn	0.0014	0.0006	0.0001	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx				
24				0.0002	17.45	6.0						
UP:												
< 2-11>	0.0064	0.0044	0.0082	0.0020								
sig	0.0009	0.0009	0.0008	0.0009								
range	0.0020	0.0019	0.0018	0.0019								
< 14-28>	0.0060	0.0058	0.0025	0.0014								
sig	0.0014	0.0014	0.0014	0.0015								
range	0.0038	0.0038	0.0031	0.0038								
< 2-28>	0.0062	0.0041	0.0028	0.0017								
sig	0.0011	0.0011	0.0011	0.0012								
range	0.0034	0.0034	0.0032	0.0037								
DOWN:												
< 2-11>	0.0088	0.0026	0.0022									
sig	0.0007	0.0007	0.0008									
range	0.0015	0.0015	0.0017									
< 14-28>	0.0080	0.0022	0.0016									
sig	0.0015	0.0015	0.0014									
range	0.0034	0.0034	0.0032									
< 2-28>	0.0082	0.0024	0.0019									
sig	0.0011	0.0011	0.0011									
range	0.0029	0.0030	0.0032									
				All								
				<1-24>	0.0017							
				sig	0.0011							
				range	0.0042							

Cell #	107	Mag#	DS0308	1/4 loc	Inner	Date	1/9/90
Pee #	6000	8000	10000	12000			
	coil meter						
1	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0148	0.0152
2 up	0.0289	0.0190	0.0215	0.0179	0.0190	0.0166	0.0163
2 dn	0.0210	0.0184	0.0192	0.0173	0.0177	0.0168	0.0152
3	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0165	0.0152
4	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0158	0.0152
5 up	0.0234	0.0190	0.0211	0.0180	0.0187	0.0167	0.0164
5 dn	0.0207	0.0185	0.0199	0.0175	0.0175	0.0163	0.0152
6	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0160	0.0152
7	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0156	0.0152
8 up	0.0221	0.0190	0.0198	0.0180	0.0174	0.0166	0.0148
8 dn	0.0198	0.0188	0.0177	0.0173	0.0182	0.0168	0.0148
9	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0141	0.0152
10	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0157	0.0152
11 up	0.0282	0.0190	0.0210	0.0180	0.0185	0.0165	0.0160
11 dn	0.0205	0.0185	0.0186	0.0174	0.0172	0.0168	0.0160
12	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0154	0.0152
13	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0170	0.0152
14 up	0.0250	0.0190	0.0225	0.0180	0.0199	0.0166	0.0174
14 dn	0.0222	0.0188	0.0208	0.0175	0.0186	0.0163	0.0152
15	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0180	0.0152
16	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0198	0.0152
17 up	0.0264	0.0191	0.0241	0.0179	0.0215	0.0166	0.0187
17 dn	0.0236	0.0184	0.0215	0.0174	0.0201	0.0168	0.0187
18	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0186	0.0152
19	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0185	0.0152
20 up	0.0248	0.0187	0.0222	0.0174	0.0198	0.0164	0.0178
20 dn	0.0220	0.0181	0.0202	0.0171	0.0186	0.0160	0.0151
21	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0175	0.0151
22	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0177	0.0151
23 up	0.0244	0.0190	0.0220	0.0180	0.0196	0.0165	0.0169
23 dn	0.0217	0.0185	0.0198	0.0173	0.0182	0.0168	0.0169
24	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	Xxxxxxx	0.0148	0.0151

Pee #	6000	8000	10000	12000	S(X=0)	str
	coil-meter	coil-meter	coil-meter	coil-meter		
1	-0.0004				18.84	5.1
2 up	0.0049	0.0086	0.0024	0.0011	18.84	6.8
2 dn	0.0027	0.0019	0.0014	Xxxxxxx	Xxxxxxx	Xxxxxxx
3				0.0018	19.17	7.0
4				0.0006	18.00	5.8
5 up	0.0044	0.0081	0.0020	0.0012	19.00	6.7
5 dn	0.0022	0.0014	0.0012	Xxxxxxx	Xxxxxxx	Xxxxxxx
6				0.0008	18.84	5.9
7				0.0004	17.67	5.6
8 up	0.0081	0.0018	0.0008	-0.0006	18.00	4.4
8 dn	0.0008	0.0004	-0.0001	Xxxxxxx	Xxxxxxx	Xxxxxxx
9				-0.0011	15.17	3.7
10				0.0006	17.84	6.7
11 up	0.0042	0.0080	0.0020	0.0008	18.84	6.4
11 dn	0.0020	0.0012	0.0009	Xxxxxxx	Xxxxxxx	Xxxxxxx
12				0.0008	17.84	5.8
13				0.0018	20.00	8.4
14 up	0.0060	0.0045	0.0088	0.0022	20.67	8.7
14 dn	0.0037	0.0028	0.0028	Xxxxxxx	Xxxxxxx	Xxxxxxx
15				0.0028	21.67	9.5
16				0.0048	24.87	18.2
17 up	0.0078	0.0062	0.0049	0.0086	23.01	11.4
17 dn	0.0062	0.0042	0.0088	Xxxxxxx	Xxxxxxx	Xxxxxxx
18				0.0084	22.87	10.6
19				0.0088	22.51	10.1
20 up	0.0059	0.0048	0.0084	0.0022	20.67	8.8
20 dn	0.0039	0.0031	0.0026	Xxxxxxx	Xxxxxxx	Xxxxxxx
21				0.0024	21.01	8.8
22				0.0026	21.84	9.2
23 up	0.0054	0.0040	0.0080	0.0018	20.00	8.0
23 dn	0.0032	0.0025	0.0019	Xxxxxxx	Xxxxxxx	Xxxxxxx
24				-0.0008	16.60	5.3

UP:

< 2-11> 0.0042 0.0029 0.0018 0.0006

sig 0.0008 0.0008 0.0007 0.0008

range 0.0018 0.0018 0.0018 0.0018

(14-28) 0.0062 0.0049 0.0087 0.0025

sig 0.0006 0.0009 0.0009 0.0008

range 0.0019 0.0022 0.0019 0.0018

< 2-28> 0.0052 0.0039 0.0027 0.0015

sig 0.0018 0.0018 0.0012 0.0012

range 0.0021 0.0024 0.0080 0.0018

DOWN:

< 2-11> 0.0019 0.0012 0.0009

sig 0.0006 0.0006 0.0007

range 0.0019 0.0015 0.0015

(14-28) 0.0040 0.0032 0.0027

sig 0.0009 0.0007 0.0008

range 0.0020 0.0017 0.0019

< 2-28> 0.0030 0.0022 0.0018

sig 0.0018 0.0012 0.0012

range 0.0019 0.0015 0.0015

NL

<1-24> 0.0015

sig 0.0015

range 0.0067

Coil#	304	Mag#	DS0808	1/4 sec	Outer	Date	1/22/90
Pos #	5000	8000	10000	12000			
	coil master						
1	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0120	0.0140
2 up	0.0211	0.0184	0.0187	0.0167	0.0155	0.0154	0.0141
2 dn	0.0198	0.0178	0.0171	0.0168	0.0156	0.0154	0.0141
3	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0129	0.0140
4	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0118	0.0140
5 up	0.0185	0.0184	0.0161	0.0167	0.0140	0.0158	0.0118
5 dn	0.0166	0.0179	0.0145	0.0162	0.0129	0.0150	0.0113
6	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0117	0.0140
7	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0112	0.0140
8 up	0.0184	0.0185	0.0155	0.0189	0.0188	0.0154	0.0107
8 dn	0.0161	0.0178	0.0184	0.0182	0.0122	0.0151	0.0107
9	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0107	0.0140
10	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0181	0.0140
11 up	0.0183	0.0185	0.0161	0.0169	0.0181	0.0158	0.0114
11 dn	0.0162	0.0178	0.0146	0.0162	0.0130	0.0151	0.0114
12	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0111	0.0140
13	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0180	0.0140
14 up	0.0200	0.0186	0.0175	0.0189	0.0155	0.0154	0.0180
14 dn	0.0184	0.0178	0.0160	0.0162	0.0140	0.0151	0.0180
15	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0182	0.0140
16	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0117	0.0140
17 up	0.0190	0.0186	0.0172	0.0169	0.0150	0.0158	0.0128
17 dn	0.0180	0.0178	0.0160	0.0162	0.0142	0.0151	0.0128
18	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0142	0.0140
19	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0149	0.0140
20 up	0.0215	0.0185	0.0189	0.0168	0.0168	0.0154	0.0145
20 dn	0.0194	0.0178	0.0175	0.0162	0.0159	0.0150	0.0145
21	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0144	0.0140
22	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0181	0.0140
23 up	0.0189	0.0185	0.0164	0.0168	0.0146	0.0155	0.0121
23 dn	0.0172	0.0177	0.0151	0.0162	0.0136	0.0150	0.0121
24	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	Xxxxxx	0.0117	0.0140

Pos #	5000	8000	10000	12000	S(X=0)	str	avg str (outer)
	coil-master	coil-master	coil-master	coil-master			
1	-0.0027	0.0020	0.0011	0.0002	27.82	11.5	10.7
2 up	0.0015	0.0008	0.0006	Xxxxxx	88.18	15.7	11.7
2 dn	-0.0011	Xxxxxx	Xxxxxx	Xxxxxx	80.01	12.8	11.0
4	-0.0027	Xxxxxx	Xxxxxx	Xxxxxx	26.12	8.4	11.2
5 up	0.0001	-0.0006	-0.0018	-0.0027	26.12	8.1	11.5
5 dn	-0.0012	-0.0017	-0.0021	Xxxxxx	27.09	8.9	12.0
6	-0.0028	Xxxxxx	Xxxxxx	Xxxxxx	25.88	8.2	10.8
7	-0.0028	Xxxxxx	Xxxxxx	Xxxxxx	24.66	7.7	9.2
8 up	-0.0005	-0.0014	-0.0028	-0.0038	24.66	7.9	9.2
8 dn	-0.0017	-0.0028	-0.0029	Xxxxxx	25.68	8.7	9.9
9	-0.0038	Xxxxxx	Xxxxxx	Xxxxxx	25.68	8.7	9.9
10	-0.0009	Xxxxxx	Xxxxxx	Xxxxxx	26.36	9.9	10.6
11 up	-0.0002	-0.0008	-0.0026	-0.0026	26.36	12.8	11.1
11 dn	-0.0018	-0.0016	-0.0021	Xxxxxx	26.36	12.8	11.1
12	-0.0029	Xxxxxx	Xxxxxx	Xxxxxx	26.36	12.8	11.1
13	-0.0010	Xxxxxx	Xxxxxx	Xxxxxx	26.36	12.8	11.1
14 up	0.0015	0.0006	-0.0001	-0.0010	26.36	12.8	11.1
14 dn	0.0002	-0.0002	-0.0011	Xxxxxx	26.36	12.8	11.1
15	-0.0008	Xxxxxx	Xxxxxx	Xxxxxx	26.36	12.8	11.1
16	-0.0028	Xxxxxx	Xxxxxx	Xxxxxx	27.09	10.8	11.5
17 up	0.0006	0.0008	-0.0006	-0.0012	27.09	12.9	12.9
17 dn	0.0002	-0.0002	-0.0009	Xxxxxx	27.09	12.9	12.9
18	0.0002	Xxxxxx	Xxxxxx	Xxxxxx	28.18	15.5	15.5
19	0.0009	Xxxxxx	Xxxxxx	Xxxxxx	28.88	16.7	16.7
20 up	0.0080	0.0021	0.0018	0.0006	28.91	15.9	15.9
20 dn	0.0020	0.0018	0.0009	Xxxxxx	28.91	15.9	15.9
21	0.0004	Xxxxxx	Xxxxxx	Xxxxxx	28.67	15.9	15.9
22	-0.0009	Xxxxxx	Xxxxxx	Xxxxxx	28.50	12.8	12.8
23 up	0.0004	-0.0004	-0.0009	-0.0019	28.07	10.6	10.6
23 dn	-0.0006	-0.0011	-0.0014	Xxxxxx	28.07	10.6	10.6
24	-0.0028	Xxxxxx	Xxxxxx	Xxxxxx	27.09	10.8	10.8

UP:
< 2-11> 0.0005 -0.0002 -0.0018 -0.0021
sig 0.0015 0.0015 0.0017 0.0016
range 0.0082 0.0084 0.0086 0.0085

<14-28> 0.0014 0.0007 -0.0001 -0.0009
sig 0.0012 0.0011 0.0010 0.0010
range 0.0026 0.0025 0.0022 0.0024

< 2-28> 0.0009 0.0002 -0.0007 -0.0016
sig 0.0018 0.0018 0.0014 0.0014
range 0.0082 0.0084 0.0086 0.0085

DOWN:
< 2-11> -0.0008 -0.0012 -0.0016
sig 0.0015 0.0014 0.0015 0.0015
range 0.0082 0.0081 0.0083

<14-28> 0.0006 -0.0001 -0.0006
sig 0.0011 0.0010 0.0010 0.0010
range 0.0025 0.0024 0.0023

< 2-28> -0.0001 -0.0006 -0.0011
sig 0.0014 0.0013 0.0013 0.0013
range 0.0082 0.0081 0.0085

All
<1-24> -0.0015
sig 0.0018
range 0.0042

Coil#	306	Magn#	DS0808	1/4 loc	Outer	Date	1/28/90
Pos #	6000	8000	10000	12000			
	coil-meter	coil-meter	coil-meter	coil-meter	coil-meter		
1	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0117	0.0140
2 up	0.0192	0.0184	0.0154	0.0167	0.0144	0.0158	0.0118
2 dn	0.0169	0.0177	0.0148	0.0161	0.0134	0.0150	0.0119
3	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0125	0.0140
4	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0132	0.0140
5 up	0.0201	0.0185	0.0178	0.0168	0.0157	0.0154	0.0138
5 dn	0.0186	0.0177	0.0164	0.0162	0.0148	0.0150	0.0140
6	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0132	0.0140
7	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0132	0.0140
8 up	0.0187	0.0185	0.0162	0.0168	0.0142	0.0154	0.0117
8 dn	0.0168	0.0177	0.0147	0.0162	0.0130	0.0150	0.0117
9	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0118	0.0140
10	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0128	0.0140
11 up	0.0197	0.0185	0.0172	0.0168	0.0152	0.0164	0.0124
11 dn	0.0178	0.0177	0.0156	0.0162	0.0140	0.0150	0.0124
12	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0122	0.0140
13	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0100	0.0140
14 up	0.0186	0.0185	0.0161	0.0168	0.0139	0.0154	0.0115
14 dn	0.0166	0.0177	0.0144	0.0162	0.0127	0.0150	0.0115
15	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0109	0.0140
16	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0112	0.0140
17 up	0.0172	0.0185	0.0145	0.0168	0.0128	0.0154	0.0100
17 dn	0.0151	0.0177	0.0129	0.0162	0.0118	0.0150	0.0100
18	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0104	0.0140
19	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0120	0.0140
20 up	0.0186	0.0185	0.0161	0.0168	0.0140	0.0154	0.0116
20 dn	0.0168	0.0177	0.0146	0.0162	0.0130	0.0150	0.0116
21	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0110	0.0140
22	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0109	0.0140
23 up	0.0186	0.0185	0.0165	0.0168	0.0145	0.0151	0.0122
23 dn	0.0177	0.0177	0.0155	0.0162	0.0136	0.0150	0.0122
24	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	0.0118	0.0140
Pos #	6000	8000	10000	12000	S(X=0)	str	
	coil-meter	coil-meter	coil-meter	coil-meter			
1	0.0008	-0.0008	-0.0009	-0.0022	26.78	10.8	
2 up	0.0008	-0.0008	-0.0018	-0.0017	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	9.9
2 dn	-0.0008				-0.0015	28.63	11.3
3					-0.0008	30.80	18.0
4					-0.0007	30.53	18.0
5 up	0.0016	0.0010	0.0008	-0.0007	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	
5 dn	0.0008	0.0002	-0.0002	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0008	30.80
6					-0.0008	30.90	12.6
7					-0.0008	30.90	18.1
8 up	0.0002	-0.0006	-0.0012	-0.0028	26.78	10.2	
8 dn	-0.0009	-0.0015	-0.0020	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0027	25.78
9					-0.0017	28.16	9.4
10					-0.0018	27.92	11.4
11 up	0.0012	0.0004	-0.0002	-0.0018	28.40	11.4	
11 dn	0.0001	-0.0006	-0.0010	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0020	22.69
12					-0.0025	26.26	9.2
13					-0.0031	24.98	7.6
14 up	0.0000	-0.0007	-0.0015	-0.0025	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	
14 dn	-0.0011	-0.0018	-0.0028	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0026	25.54
15					-0.0038	22.69	9.2
16					-0.0040	22.64	6.2
17 up	-0.0018	-0.0028	-0.0031	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0040	27.44
17 dn	-0.0026	-0.0038	-0.0047	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0040	26.49
18					-0.0046	27.92	9.7
19					-0.0020	26.49	8.9
20 up	0.0001	-0.0007	-0.0014	-0.0024	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	
20 dn	-0.0011	-0.0016	-0.0020	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0030	25.07
21					-0.0041	24.88	7.7
22					-0.0041	24.88	7.5
23 up	0.0008	-0.0001	-0.0006	-0.0019	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	
23 dn	0.0000	-0.0007	-0.0014	Xxxxxxxxxxxxxxx	Xxxxxxxxxxxxxxx	-0.0027	25.78
24							9.8
UP:					26.8808	9.84454	
< 2-11>	0.0010	0.0001	-0.0006	-0.0017			
sig	0.0006	0.0007	0.0007	0.0007			
range	0.0014	0.0018	0.0015	0.0018			
<14-23>	-0.0002	-0.0010	-0.0016	-0.0027			
sig	0.0007	0.0009	0.0011	0.0009			
range	0.0016	0.0022	0.0026	0.0022			
< 2-28>	0.0004	-0.0004	-0.0011	-0.0022			
sig	0.0009	0.0010	0.0010	0.0009			
range	0.0029	0.0038	0.0034	0.0038			
DOWN:							
< 2-11>	-0.0002	-0.0008	-0.0012				
sig	0.0008	0.0008	0.0008				
range	0.0017	0.0017	0.0018				
<14-23>	-0.0012	-0.0019	-0.0024				
sig	0.0011	0.0011	0.0010				
range	0.0026	0.0026	0.0026				
< 2-23>	-0.0007	-0.0018	-0.0018				
sig	0.0010	0.0010	0.0010				
range	0.0034	0.0035	0.0035				
				ALL			
				<1-24>	-0.0028		
				sig	0.0010		
				range	0.0038		

ASSUMING ALL COMPONENTS ARE "AS MEASURED"

Coil# 106 Mag# DS0808 1/4 loc Inner Date 1/6/90
Shim: 0.008 Collar error: 0
stress 6000 8000 10000 12000
size 0.0082 0.0071 0.0068 0.0047

linear fit stress = f(size)
 $\sigma(0) = 19.98 \text{ kpsi}$ $d\sigma/dx = -1.706 \text{ kpsi/mil}$
collared stress
7.7

Coil# 107 Mag# DS0808 1/4 loc Inner Date 1/8/90
Shim: 0.008 Collar error: 0
stress 6000 8000 10000 12000
size 0.0082 0.0069 0.0067 0.0045

linear fit stress = f(size)
 $\sigma(0) = 19.54 \text{ kpsi}$ $d\sigma/dx = -1.668 \text{ kpsi/mil}$
collared stress
7.8

Coil# 804 Mag# DS0808 1/4 loc Outer Date 1/22/90
Shim: 0.010 Collar error: -0.0015
stress 6000 8000 10000 12000
size 0.0094 0.0087 0.0078 0.0070

linear fit stress = f(size)
 $\sigma(0) = 29.08 \text{ kpsi}$ $d\sigma/dx = -2.484 \text{ kpsi/mil}$
collared stress
11.6

Coil# 806 Mag# DS0808 1/4 loc Outer Date 1/23/90
Shim: 0.010 Collar error: -0.0015
stress 6000 8000 10000 12000
size 0.0089 0.0081 0.0074 0.0068

linear fit stress = f(size)
 $\sigma(0) = 27.24 \text{ kpsi}$ $d\sigma/dx = -2.876 \text{ kpsi/mil}$
collared stress
10.2

Collar compliance (in terms of average inner+outer coil stress)
Collar vertical offset (individual collar away from magnet center)
 $dx/ds = 0.56 \text{ mils/kpsi}$ $x(0) = 2 \text{ mils}$

Coil average stress = f(collar deflection)
 $\sigma(0) = -8.57 \text{ kpsi}$ $d\sigma/dx = 1.796 \text{ kpsi/mil}$

Average of 4 coils:
 $\sigma(0) = 28.96 \text{ kpsi}$ $d\sigma/dx = -2.05 \text{ kpsi/mil}$

Collar vertical radius:
7.2 mils

Average inner stress = 7.6
Average outer stress = 10.9

Average coil stress = 9.8

ASSUMING COLLAR CAVITY IS 7 MILS LARGER

Coil# 106 Mag# DS0808 1/4 loc Inner Date 1/6/90
Shim: 0.008 Collar error: -0.007
stress 6000 8000 10000 12000
size 0.0012 0.0001 -0.0012 -0.0028

linear fit stress = f(size)
 $\sigma(0) = 8.05 \text{ kpsi}$ $d\sigma/dx = -1.705 \text{ kpsi/mil}$
collared stress
2.2

Coil# 107 Mag# DS0808 1/4 loc Inner Date 1/6/90
Shim: 0.008 Collar error: -0.007
stress 6000 8000 10000 12000
size 0.0012 -0.0001 -0.0018 -0.0025

linear fit stress = f(size)
 $\sigma(0) = 7.87 \text{ kpsi}$ $d\sigma/dx = -1.668 \text{ kpsi/mil}$
collared stress
2.1

Coil# 304 Mag# DS0808 1/4 loc Outer Date 1/22/90
Shim: 0.010 Collar error: -0.0085
stress 6000 8000 10000 12000
size 0.0024 0.0017 0.0008 0.0000

linear fit stress = f(size)
 $\sigma(0) = 12.04 \text{ kpsi}$ $d\sigma/dx = -2.434 \text{ kpsi/mil}$
collared stress
3.6

Coil# 305 Mag# DS0808 1/4 loc Outer Date 1/28/90
Shim: 0.010 Collar error: -0.0085
stress 6000 8000 10000 12000
size 0.0019 0.0011 0.0004 -0.0007

linear fit stress = f(size)
 $\sigma(0) = 10.60 \text{ kpsi}$ $d\sigma/dx = -2.376 \text{ kpsi/mil}$
collared stress
2.4

Collar compliance (in terms of average inner+outer coil stress)
Collar vertical offset (individual collar away from magnet center)
 $dx/d\sigma = 0.56 \text{ mils/kpsi}$ $x(0) = 2 \text{ mils}$

Coil average stress = f(collar deflection)
 $\sigma(0) = -8.57 \text{ kpsi}$ $d\sigma/dx = 1.796 \text{ kpsi/mil}$

Average of 4 coils:
 $\sigma(0) = 9.84 \text{ kpsi}$ $d\sigma/dx = -2.06 \text{ kpsi/mil}$

Collar vertical radius:
3.4 mils

Average inner stress = 2.1
Average outer stress = 3.0

Average coil stress = 2.6

DS0307A

Collg	104	Mag#	DS0307A 1/4 sec	L1	Date	1/30/90		
Poss #	—	5000	—	8000	—	10000	—	12000
		coil-meter	coil-meter	coil-meter	coil-meter	coil-meter	coil-meter	coil-meter
1		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
2 up	0.0267	0.0198	0.0248	0.0180	0.0218	0.0157	0.0194	0.0152
2 dn	0.0242	0.0185	0.0228	0.0175	0.0208	0.0164	0.0194	0.0152
3		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
4		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
5 up	0.0279	0.0198	0.0225	0.0180	0.0282	0.0167	0.0206	0.0152
5 dn	0.0254	0.0185	0.0285	0.0175	0.0228	0.0164	0.0206	0.0152
6		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
7		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
8 up	0.0261	0.0198	0.0239	0.0180	0.0215	0.0167	0.0191	0.0152
8 dn	0.0249	0.0185	0.0220	0.0175	0.0204	0.0164	0.0191	0.0152
9		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
10		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
11 up	0.0277	0.0198	0.0257	0.0180	0.0227	0.0167	0.0204	0.0152
11 dn	0.0250	0.0185	0.0281	0.0175	0.0215	0.0164	0.0204	0.0152
12		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
13		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
14 up	0.0261	0.0198	0.0287	0.0180	0.0214	0.0167	0.0188	0.0152
14 dn	0.0284	0.0185	0.0217	0.0175	0.0200	0.0164	0.0188	0.0152
15		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
16		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
17 up	0.0262	0.0198	0.0288	0.0180	0.0210	0.0167	0.0186	0.0152
17 dn	0.0234	0.0185	0.0215	0.0175	0.0199	0.0164	0.0186	0.0152
18		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
19		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
20 up	0.0278	0.0198	0.0242	0.0180	0.0218	0.0167	0.0197	0.0152
20 dn	0.0241	0.0185	0.0228	0.0175	0.0205	0.0164	0.0197	0.0152
21		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
22		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
23 up	0.0264	0.0198	0.0289	0.0180	0.0215	0.0167	0.0190	0.0152
23 dn	0.0241	0.0185	0.0222	0.0175	0.0204	0.0164	0.0190	0.0152
24		Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx
Poss #	—	5000	—	8000	—	10000	—	12000
		coil-meter	coil-meter	coil-meter	coil-meter	coil-meter	S(%)=0	rv
		coil-meter	coil-meter	coil-meter	coil-meter	coil-meter	(collar)	str
1		0.0074	0.0068	0.0051	0.0042	0.0029	22.54	8.3
2 up	0.0074	0.0068	0.0051	0.0042	0.0029	25.06	8.7	9.3
2 dn	0.0057	0.0048	0.0039	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	10.0
3		0.0069	0.0060	0.0056	0.0044	0.0029	25.45	8.7
4		0.0069	0.0060	0.0056	0.0056	0.0029	27.68	8.7
5 up	0.0068	0.0045	0.0065	0.0054	0.0042	27.26	8.9	9.8
5 dn	0.0068	0.0045	0.0065	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	10.4
6		0.0068	0.0045	0.0065	0.0054	0.0029	25.06	8.9
7		0.0068	0.0045	0.0065	0.0054	0.0029	24.86	8.7
8 up	0.0064	0.0059	0.0048	0.0039	0.0038	24.54	8.4	10.5
8 dn	0.0054	0.0045	0.0040	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	11.2
9		0.0065	0.0056	0.0051	0.0044	0.0029	23.58	8.2
10 up	0.0084	0.0077	0.0080	0.0061	0.0048	23.58	8.2	10.8
10 dn	0.0065	0.0056	0.0051	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	9.7
11		0.0065	0.0056	0.0051	0.0049	0.0029	26.17	8.5
12 up	0.0068	0.0067	0.0047	0.0036	0.0029	26.72	8.5	11.8
12 dn	0.0061	0.0042	0.0036	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	11.7
13		0.0068	0.0067	0.0047	0.0036	0.0029	26.85	8.8
14 up	0.0068	0.0067	0.0047	0.0036	0.0029	28.99	8.6	11.8
14 dn	0.0061	0.0042	0.0036	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	11.3
15		0.0068	0.0067	0.0047	0.0036	0.0029	22.72	7.8
16		0.0068	0.0067	0.0047	0.0036	0.0029	22.90	8.0
17 up	0.0069	0.0068	0.0048	0.0038	0.0038	23.45	8.1	9.1
17 dn	0.0049	0.0040	0.0035	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	9.1
18		0.0068	0.0067	0.0047	0.0036	0.0029	24.90	8.4
19		0.0068	0.0067	0.0047	0.0036	0.0029	25.45	9.2
20 up	0.0088	0.0062	0.0049	0.0045	0.0045	25.53	9.4	9.4
20 dn	0.0056	0.0048	0.0041	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	9.4
21		0.0056	0.0048	0.0041	0.0035	0.0029	28.85	8.0
22		0.0056	0.0048	0.0041	0.0035	0.0029	28.45	7.7
23 up	0.0070	0.0069	0.0048	0.0038	0.0038	24.86	8.5	9.5
23 dn	0.0056	0.0047	0.0040	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	Xxxxxxxxxxxxxx	9.5
24		0.0056	0.0047	0.0040	0.0019	0.0019	20.90	5.8
UP:							ALL	
< 2-11>	0.0078	0.0061	0.0056	0.0047			<1-24>	0.0040
eig	0.0008	0.0018	0.0008	0.0007			eig	0.0009
range	0.0018	0.0082	0.0017	0.0015			range	0.0087
<14-23>	0.0078	0.0058	0.0047	0.0088				
sig	0.0007	0.0004	0.0008	0.0006				
range	0.0016	0.0009	0.0006	0.0012				
< 2-23>	0.0075	0.0059	0.0051	0.0042				
eig	0.0008	0.0009	0.0007	0.0007				
range	0.0018	0.0032	0.0022	0.0021				
DOMH:								
< 2-11>	0.0061	0.0052	0.0047					
eig	0.0007	0.0007	0.0008					
range	0.0015	0.0015	0.0017					
<14-23>	0.0068	0.0044	0.0038					
sig	0.0004	0.0004	0.0005					
range	0.0007	0.0008	0.0006					
< 2-23>	0.0057	0.0048	0.0042					
eig	0.0007	0.0007	0.0007					
range	0.0020	0.0020	0.0021					

Coil# 106 Mag# DS0807A 1/4 sec UI Date 1/30/90

Pos #	8000	8000	10000	12000	
	coil meter	coil meter	coil meter	coil meter	
1	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0200 0.0151
2 up	0.0257 0.0190	0.0243 0.0176	0.0217 0.0168	0.0191 0.0151	
2 dn	0.0283 0.0182	0.0221 0.0171	0.0208 0.0160	0.0191 0.0151	
3	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0188 0.0151
4	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0178 0.0151
5 up	0.0258 0.0190	0.0284 0.0176	0.0210 0.0168	0.0184 0.0151	
5 dn	0.0283 0.0182	0.0214 0.0171	0.0198 0.0160	0.0184 0.0151	
6	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0189 0.0151
7	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0190 0.0151
8 up	0.0288 0.0190	0.0269 0.0176	0.0244 0.0168	0.0219 0.0151	
8 dn	0.0267 0.0182	0.0247 0.0171	0.0232 0.0160	0.0219 0.0151	
9	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0204 0.0151
10	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0200 0.0151
11 up	0.0251 0.0190	0.0282 0.0176	0.0208 0.0168	0.0184 0.0151	
11 dn	0.0284 0.0182	0.0214 0.0171	0.0197 0.0160	0.0184 0.0151	
12	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0178 0.0151
13	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0186 0.0151
14 up	0.0278 0.0190	0.0249 0.0176	0.0226 0.0168	0.0198 0.0151	
14 dn	0.0250 0.0182	0.0230 0.0171	0.0213 0.0160	0.0198 0.0151	
15	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0197 0.0151
16	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0208 0.0151
17 up	0.0288 0.0190	0.0265 0.0176	0.0240 0.0168	0.0212 0.0151	
17 dn	0.0254 0.0182	0.0244 0.0171	0.0227 0.0160	0.0212 0.0151	
18	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0227 0.0151
19	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0242 0.0151
20 up	0.0318 0.0190	0.0267 0.0176	0.0274 0.0168	0.0249 0.0151	
20 dn	0.0296 0.0182	0.0268 0.0171	0.0258 0.0160	0.0249 0.0151	
21	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0228 0.0151
22	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0219 0.0151
23 up	0.0291 0.0190	0.0267 0.0176	0.0241 0.0168	0.0218 0.0151	
23 dn	0.0262 0.0182	0.0242 0.0171	0.0227 0.0160	0.0218 0.0151	
24	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	XXXXXXXXXXXXXX	0.0222 0.0151

Pos #	8000	8000	10000	12000	S(X=0)	str
	coil-meter	coil-meter	coil-meter	coil-meter		
1	0.0077	0.0067	0.0064	0.0040	25.89	11.3
2 up	0.0061	0.0050	0.0048	XXXXXXXXXX	24.80	9.0
2 dn				XXXXXXXXXX	XXXXXXXXXX	
3				XXXXXXXXXX	22.90	7.7
4				XXXXXXXXXX	21.67	6.3
5 up	0.0068	0.0058	0.0047	0.0038	20.07	7.4
5 dn	0.0051	0.0043	0.0038	XXXXXXXXXX	XXXXXXXXXX	
6				XXXXXXXXXX	20.96	8.2
7				XXXXXXXXXX	24.18	9.9
8 up	0.0098	0.0098	0.0081	0.0068	29.22	14.4
8 dn	0.0085	0.0076	0.0072	XXXXXXXXXX	XXXXXXXXXX	
9				XXXXXXXXXX	26.59	12.2
10				XXXXXXXXXX	25.89	11.0
11 up	0.0061	0.0056	0.0045	0.0033	28.07	8.2
11 dn	0.0052	0.0043	0.0037	XXXXXXXXXX	XXXXXXXXXX	
12				XXXXXXXXXX	22.02	7.4
13				XXXXXXXXXX	23.42	8.8
14 up	0.0088	0.0078	0.0068	0.0047	25.58	10.6
14 dn	0.0068	0.0059	0.0063	XXXXXXXXXX	XXXXXXXXXX	
15				XXXXXXXXXX	25.86	10.4
16				XXXXXXXXXX	26.76	12.4
17 up	0.0098	0.0089	0.0077	0.0061	27.99	18.1
17 dn	0.0082	0.0078	0.0067	XXXXXXXXXX	XXXXXXXXXX	
18				XXXXXXXXXX	30.53	15.4
19				XXXXXXXXXX	38.27	17.5
20 up	0.0128	0.0121	0.0111	0.0098	84.50	18.8
20 dn	0.0114	0.0112	0.0098	XXXXXXXXXX	XXXXXXXXXX	
21				XXXXXXXXXX	30.81	15.5
22				XXXXXXXXXX	29.22	14.0
23 up	0.0101	0.0091	0.0078	0.0065	28.70	18.4
23 dn	0.0080	0.0071	0.0067	XXXXXXXXXX	XXXXXXXXXX	
24				XXXXXXXXXX	29.75	15.1

UP:
< 2-11> 0.0078 0.0069 0.0067 0.0044
sig 0.0016 0.0017 0.0017 0.0017
range 0.0087 0.0087 0.0086 0.0086

<14-23> 0.0108 0.0094 0.0082 0.0068
sig 0.0019 0.0020 0.0020 0.0022
range 0.0045 0.0048 0.0048 0.0061

< 2-23> 0.0069 0.0061 0.0070 0.0066
sig 0.0021 0.0022 0.0022 0.0022
range 0.0058 0.0058 0.0058 0.0085

DOWN:
< 2-11> 0.0080 0.0068 0.0048
sig 0.0017 0.0016 0.0017
range 0.0084 0.0083 0.0085

<14-23> 0.0066 0.0079 0.0071
sig 0.0020 0.0028 0.0019
range 0.0046 0.0058 0.0045

< 2-23> 0.0078 0.0066 0.0069
sig 0.0022 0.0028 0.0021
range 0.0084 0.0083 0.0085

ALL
<1-24> 0.0068
sig 0.0020
range 0.0078

Cell# 806 Magf DS0807A 1/4 loc 0 Date 3/2/90

Pos #	6000	8000	10000	12000	
	coil meter	coil meter	coil meter	coil meter	
1	1.0049	1.0000	1.0038	0.9991	1.0021 0.9984 1.0008 0.9975
2 up	1.0085	0.9996	1.0022	0.9987	1.0010 0.9981 1.0003 0.9975
2 dn					1.0005 0.9975
3					1.0002 0.9975
4					1.0002 0.9975
5 up	1.0056	1.0000	1.0038	0.9991	1.0024 0.9984 1.0008 0.9975
5 dn	1.0041	0.9996	1.0027	0.9987	1.0016 0.9981 1.0008 0.9975
6					1.0010 0.9975
7					1.0011 0.9975
8 up	1.0045	1.0000	1.0029	0.9991	1.0016 0.9984 0.9998 0.9975
8 dn	1.0081	0.9996	1.0018	0.9987	1.0007 0.9981 0.9998 0.9975
9					0.9996 0.9975
10					1.0008 0.9975
11 up	1.0061	1.0000	1.0042	0.9991	1.0028 0.9984 1.0011 0.9975
11 dn	1.0044	0.9996	1.0029	0.9987	1.0019 0.9981 1.0011 0.9975
12					1.0009 0.9975
13					0.9988 0.9975
14 up	1.0089	1.0000	1.0028	0.9992	1.0007 0.9985 0.9991 0.9975
14 dn	1.0028	0.9997	1.0008	0.9989	0.9998 0.9991 0.9978
15					0.9996 0.9976
16					0.9992 0.9976
17 up	1.0088	1.0000	1.0022	0.9992	1.0008 0.9988 0.9988 0.9976
17 dn	1.0021	0.9998	1.0005	0.9989	0.9986 0.9988 0.9976
18					0.9996 0.9976
19					1.0008 0.9976
20 up	1.0060	1.0000	1.0038	0.9991	1.0016 0.9984 1.0001 0.9976
20 dn	1.0084	0.9997	1.0020	0.9989	1.0009 0.9982 1.0001 0.9976
21					1.0004 0.9976
22					1.0004 0.9976
23 up	1.0069	1.0000	1.0038	0.9991	1.0025 0.9984 1.0008 0.9978
23 dn	1.0089	0.9997	1.0025	0.9989	1.0014 0.9982 1.0006 0.9978
24					0.9996 0.9976

Pos #	6000	8000	10000	12000	S(X=0)	str	avg str (outer)
	coil-meter	coil-meter	coil-meter	coil-meter			
1					0.0022	35.76	18.0 12.6
2 up	0.0049	0.0042	0.0087	0.0028		35.26	18.5 18.9
2 dn	0.0040	0.0085	0.0029	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
3					0.0080	35.76	14.1 14.1
4					0.0027	35.01	13.2 13.6
5 up	0.0055	0.0047	0.0040	0.0038		36.51	14.2 13.0
5 dn	0.0045	0.0040	0.0035	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
6					0.0035	37.01	14.6 13.9
7					0.0036	37.26	15.5 18.4
8 up	0.0045	0.0038	0.0082	0.0028		34.01	12.9 11.8
8 dn	0.0085	0.0081	0.0026	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
9					0.0020	38.26	12.7 11.8
10					0.0033	36.51	15.8 18.3
11 up	0.0061	0.0061	0.0044	0.0036		37.26	15.1 13.4
11 dn	0.0048	0.0042	0.0038	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
12					0.0034	36.76	16.0 12.8
13					0.0008	30.25	9.5
14 up	0.0089	0.0081	0.0022	0.0015		32.01	10.8
14 dn	0.0026	0.0019	0.0016	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
15					0.0022	35.76	12.5
16					0.0018	32.26	11.7
17 up	0.0088	0.0080	0.0020	0.0012		31.25	10.1
17 dn	0.0028	0.0016	0.0014	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
18					0.0019	33.01	11.3
19					0.0027	35.01	12.8
20 up	0.0050	0.0042	0.0086	0.0025		34.51	12.2
20 dn	0.0087	0.0081	0.0027	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
21					0.0028	35.26	13.5
22					0.0028	35.26	13.8
23 up	0.0069	0.0047	0.0041	0.0030		35.75	14.0
23 dn	0.0042	0.0046	0.0082	XXXXXXXXXX	XXXXXXXXXX	XXXXXXXXXX	
24					0.0020	38.26	12.5

UP:

< 2-11>	0.0058	0.0045	0.0088	0.0080
sig	0.0007	0.0006	0.0005	0.0006
range	0.0016	0.0018	0.0012	0.0018
<14-23>	0.0047	0.0088	0.0080	0.0021
sig	0.0010	0.0008	0.0010	0.0008
range	0.0021	0.0017	0.0021	0.0018
< 2-23>	0.0050	0.0041	0.0084	0.0025
sig	0.0009	0.0008	0.0009	0.0008
range	0.0028	0.0021	0.0024	0.0024

ALL

<1-24>	0.0025
sig	0.0008
range	0.0028

DOWN:

< 2-11>	0.0042	0.0087	0.0082
sig	0.0006	0.0006	0.0006
range	0.0018	0.0011	0.0012
<14-23>	0.0082	0.0086	0.0022
sig	0.0009	0.0010	0.0009
range	0.0019	0.0020	0.0018
< 2-23>	0.0087	0.0081	0.0027
sig	0.0009	0.0009	0.0008
range	0.0025	0.0026	0.0024

Coil# 307 Magf DS0807A 1/4 loc 0 Date 8/8/90
 Pos # — 6000 — 8000 — 10000 — 12000 —

	coil master										
1	0.0048	1.0000	1.0026	0.9991	1.0012	0.9984	0.9996	0.9974			
2 up	1.0027	0.9994	1.0014	0.9987	1.0004	0.9980	0.9996	0.9974			
2 dn											
3								1.0001	0.9974		
4									0.9995	0.9974	
5 up	1.0042	1.0000	1.0025	0.9991	1.0010	0.9984	0.9994	0.9975			
5 dn	1.0026	0.9994	1.0018	0.9987	1.0001	0.9981	0.9994	0.9975			
6									0.9997	0.9975	
7										0.9999	0.9975
8 up	1.0037	1.0000	1.0021	0.9991	1.0004	0.9984	0.9987	0.9975			
8 dn	1.0021	0.9994	1.0005	0.9988	0.9994	0.9981	0.9987	0.9975			
9									0.9998	0.9975	
10									0.9994	0.9975	
11 up	1.0068	1.0000	1.0084	0.9991	1.0028	0.9984	1.0008	0.9975			
11 dn	1.0038	0.9996	1.0028	0.9988	1.0015	0.9981	1.0006	0.9975			
12									1.0004	0.9975	
13									0.9989	0.9975	
14 up	1.0046	1.0000	1.0028	0.9991	1.0018	0.9984	0.9996	0.9975			
14 dn	1.0030	0.9996	1.0015	0.9989	1.0004	0.9982	0.9996	0.9975			
15									1.0002	0.9975	
16									0.9998	0.9975	
17 up	1.0063	1.0000	1.0084	0.9991	1.0020	0.9984	1.0008	0.9975			
17 dn	1.0037	0.9996	1.0024	0.9989	1.0011	0.9982	1.0003	0.9975			
18									1.0008	0.9976	
19									1.0021	0.9976	
20 up	1.0068	1.0000	1.0048	0.9992	1.0029	0.9985	1.0012	0.9975			
20 dn	1.0047	0.9996	1.0031	0.9989	1.0021	0.9982	1.0012	0.9975			
21									1.0014	0.9975	
22									1.0011	0.9975	
23 up	1.0065	1.0000	1.0048	0.9992	1.0081	0.9983	1.0015	0.9975			
23 dn	1.0049	0.9996	1.0084	0.9989	1.0024	0.9982	1.0015	0.9975			
24									0.9999	0.9975	

Pos # — 6000 — 8000 — 10000 — 12000 — S(x=0) str

	coil-master	coil-master	coil-master	coil-master	coil-master		
1	0.0048	0.0085	0.0028	0.0022	0.0017	31.16	11.7
2 up	0.0088	0.0027	0.0024	X000000X	X000000X	52.88	12.0
2 dn						0.0027	33.50
3						0.0021	32.09
4						0.0019	31.68
5 up	0.0042	0.0084	0.0026	X000000X	X000000X	32.88	10.8
5 dn	0.0082	0.0025	0.0020			0.0022	32.88
6						0.0024	32.80
7						0.0024	32.80
8 up	0.0087	0.0080	0.0020	0.0012	0.0012	29.99	10.8
8 dn	0.0026	0.0017	0.0018	X000000X	X000000X	29.76	10.8
9						0.0011	31.63
10						0.0019	31.63
11 up	0.0056	0.0045	0.0089	0.0081	0.0081	34.43	14.6
11 dn	0.0042	0.0087	0.0084	X000000X	X000000X	30.46	11.1
12						0.0029	38.95
13						0.0014	30.46
14 up						0.0021	32.09
14 dn						X000000X	X000000X
15						0.0027	38.50
16						0.0018	31.89
17 up	0.0062	0.0048	0.0086	0.0028	0.0028	33.73	14.0
17 dn	0.0041	0.0084	0.0029	X000000X	X000000X	34.66	14.4
18						0.0045	37.70
19						0.0087	35.98
20 up	0.0068	0.0061	0.0044	X000000X	X000000X	36.30	15.0
20 dn	0.0061	0.0042	0.0089			0.0089	36.30
21						0.0046	35.60
22						0.0046	35.60
23 up	0.0065	0.0058	0.0046	0.0040	0.0040	36.53	16.2
23 dn	0.0068	0.0045	0.0042	X000000X	X000000X	36.90	18.4
24						0.0024	32.80

UP: 88.1751 18.1444

< 2-11> 0.0045 0.0086 0.0028 0.0021
 sig 0.0008 0.0006 0.0008 0.0008
 range 0.0019 0.0015 0.0019 0.0019

<14-23> 0.0080 0.0049 0.0042 0.0082
 sig 0.0007 0.0006 0.0006 0.0009
 range 0.0018 0.0010 0.0010 0.0019

< 2-23> 0.0062 0.0048 0.0085 0.0026
 sig 0.0011 0.0009 0.0010 0.0009
 range 0.0019 0.0015 0.0022 0.0019

DDWN:
 < 2-11> 0.0088 0.0027 0.0028
 sig 0.0007 0.0008 0.0009
 range 0.0017 0.0020 0.0021

<14-23> 0.0046 0.0040 0.0087
 sig 0.0006 0.0006 0.0007
 range 0.0012 0.0011 0.0018

< 2-23> 0.0041 0.0088 0.0080
 sig 0.0010 0.0010 0.0010
 range 0.0017 0.0020 0.0021

ALL
 <1-24> 0.0026
 sig 0.0009
 range 0.0084

ASSUMING ALL COMPONENTS ARE "AS MEASURED"

Coil# 104 MagDS0807A 1/4 loc LI Date 1/30/90
Shim: 0.008 Collar error: 0
stress 6000 8000 10000 12000
size 0.0106 0.0089 0.0081 0.0072

linear fit stress = f(size)
 $s(0) = 24.82 \text{ kpsi}$ $ds/dx = -1.817 \text{ kpsi/mil}$
collared stress 9.1

Coil# 106 MagDS0807A 1/4 loc UI Date 1/30/90
Shim: 0.008 Collar error: 0
stress 6000 8000 10000 12000
size 0.0119 0.0111 0.0100 0.0098

linear fit stress = f(size)
 $s(0) = 27.25 \text{ kpsi}$ $ds/dx = -1.758 \text{ kpsi/mil}$
collared stress 12.1

Coil# 806 MagDS0807A 1/4 loc 0 Date 8/2/90
Shim: 0.008 Collar error: -0.0015
stress 6000 8000 10000 12000
size 0.0115 0.0106 0.0099 0.0090

linear fit stress = f(size)
 $s(0) = 34.61 \text{ kpsi}$ $ds/dx = -2.501 \text{ kpsi/mil}$
collared stress 18.0

Coil# 807 MagDS0807A 1/4 loc 0 Date 8/8/90
Shim: 0.008 Collar error: -0.0015
stress 6000 8000 10000 12000
size 0.0117 0.0108 0.0100 0.0091

linear fit stress = f(size)
 $s(0) = 38.31 \text{ kpsi}$ $ds/dx = -2.337 \text{ kpsi/mil}$
collared stress 18.1

Collar compliance (in terms of average inner+outer coil stress)
Collar vertical offset (individual collar away from magnet center)
 $dx/de = 0.56 \text{ mil/kpsi}$ $x(0) = 2 \text{ mils}$

Coil average stress = f(collars deflection)
 $s(0) = -8.57 \text{ kpsi}$ $ds/dx = 1.798 \text{ kpsi/mil}$

Average of 4 coils:
 $s(0) = 30.00 \text{ kpsi}$ $ds/dx = -2.10 \text{ kpsi/mil}$

Collar vertical radius:
8.6 mils

Average inner stress = 10.6

Average outer stress = 18.1

Average coil stress = 11.8

ASSUMING COLLAR CAVITY IS 7 MILS OVERSIZE

Coil# 104 Mag#DS0807A 1/4 loc LI Date 1/30/90
Shim: 0.008 Collar error: -0.007
stress 6000 8000 10000 12000
size 0.0085 0.0019 0.0011 0.0002

linear fit stress = f(size)
 $\sigma(0) = 12.10 \text{ kpsi}$ $d\sigma/dx = -1.817 \text{ kpsi/mil}$
collared stress
8.3

Coil# 106 Mag#DS0807A 1/4 loc UI Date 1/30/90
Shim: 0.008 Collar error: -0.007
stress 6000 8000 10000 12000
size 0.0049 0.0041 0.0030 0.0018

linear fit stress = f(size)
 $\sigma(0) = 14.95 \text{ kpsi}$ $d\sigma/dx = -1.758 \text{ kpsi/mil}$
collared stress
6.4

Coil# 808 Mag#DS0807A 1/4 loc O Date 3/2/90
Shim: 0.008 Collar error: -0.0085
stress 6000 8000 10000 12000
size 0.0045 0.0036 0.0029 0.0020

linear fit stress = f(size)
 $\sigma(0) = 17.10 \text{ kpsi}$ $d\sigma/dx = -2.501 \text{ kpsi/mil}$
collared stress
5.0

Coil# 807 Mag#DS0807A 1/4 loc O Date 3/3/90
Shim: 0.008 Collar error: -0.0085
stress 6000 8000 10000 12000
size 0.0047 0.0038 0.0030 0.0021

linear fit stress = f(size)
 $\sigma(0) = 16.95 \text{ kpsi}$ $d\sigma/dx = -2.387 \text{ kpsi/mil}$
collared stress
5.6

Collar compliance (in terms of average inner+outer coil stress)
Collar vertical offset (individual collar away from magnet center)
 $dx/d\sigma = 0.56 \text{ mils/kpsi}$ $x(0) = 2 \text{ mils}$

Coil average stress = f(collar deflection)
 $\sigma(0) = -8.57 \text{ kpsi}$ $d\sigma/dx = 1.786 \text{ kpsi/mil}$

Average of 4 coils:
 $\sigma(0) = 15.28 \text{ kpsi}$ $d\sigma/dx = -2.10 \text{ kpsi/mil}$

Collar vertical radius:

4.8 mils

Average inner stress = 4.9

Average outer stress = 5.8

Average coil stress = 5.1

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*Magnet Systems Division
Business Management Group*

MEMORANDUM

To: **R. Briggs and T. Bush**
From: **R.B. Palmer**
Date: **March 26, 1990**
Subject: **MAGNET TASK FORCE, INTERIM REPORT #3**

This report reflects discussion of the Task Force at its meeting on 3/21/90, held at SSCL, and other discussions.

Modification to previous recommendation

The recommendation (1) in report #1 on the od yoke (13 in.) should be modified to define the OD of the shell. The OD of the shell should be 13-3/8 in. or 340 mm.

Recommendations:

1) the ratio of copper to superconductor for the cables should be:

inner: 1.5:1 outer: 1.7:1

These choices give: short sample field, field margin, and copper current densities at 6.6 and 7.2 Tesla of:

inner: 7.26 T 10% 712 A/mm sq 782 A/mm sq

outer: 7.46 T 13% 866 A/mm sq 953 A/mm sq

The copper current densities in the outer cable are higher than some of us would like, but the observed rarity of training quench in the outer layer, in current SSC magnets, suggests that this should not be a problem.

In addition, the development of an outer cable with ratio of 2.0 :1 (which would have matched the margins in inner and outer layers) was considered to be a significant task, and not worth the possible small improvement in first quench field.

The cost savings in further raising the copper ratio (eg about 5 m\$ for a change from 1.5: 1 to 1.7: 1) were not considered to be worth the loss in field margin.

Note that this field margin of 10% will probably be reduced by subsequent decisions (see, for instance, recommendation #3).

2) An intermediate temperature Beam Tube Liner should be inserted within the bore of the magnet. Cooling, at around 20 degrees, should have the potential capacity of removing at least 10 times the present design synchrotron radiation loss.

Such a liner will allow future upgrades of machine luminosity, by allowing an order of magnitude higher currents.

Such a liner will also allow operation of the magnets at lower than design temperature, thus increasing either the operating field or operating margin.

If such a liner is not designed in at this time, it will be either impossible, or very expensive to retrofit it later.

A study of the design of this bore tube liner should be initiated, at once, jointly by the magnet and accelerator departments.

3) The quadrupole aperture should be raised to 5 cm.

The change will make it possible to insert, within the bore of the quadrupoles (as is now possible in the dipoles), the intermediate temperature beam tube liner.

It will reduce the contributions to field errors from the quadrupoles and make the contribution per meter, or per magnet end, approximately the same as those from the dipoles. Note that the effects on aperture, per meter, or per magnet end, will still be greater for the quadrupoles than for the dipoles, because the beta functions are at their maxima in the quads.

The change will ease the possible problems in winding the pole turns with the wide cable.

The change will make the tooling radii the same for quadrupoles and dipoles. It will also ease the design of interconnects between quadrupoles and dipoles.

4) The new quadrupole design should use the same cable as specified for the outer layer of the dipole. The iron yoke should be allowed to come relatively close to the coil, in order to maximize the gradient and match, as nearly as possible, the droop in the transfer function of the dipole. The field margin should not be less than that in the dipole inner (now 10%) at operating energy.

It is recognized that the resulting quadrupole will have a somewhat lower gradient than that of the present 4 cm design. It will, as a result, have to be somewhat longer. The dipoles will have to be a little (perhaps of the order of 1%) shorter, and will have to operate at a slightly higher field. This, in view of the current design field margin, seems reasonable.

5) A priority engineering study is needed on the vertically split yoke design. In order to specify the shell thickness, and thus yoke outside diameter, the loss of stress in the shell during cool down must be calculated. The differential coefficients of expansion and the changing yield strength of the aluminum must be tracked with temperature, and, the effects of friction between the shell and yoke must be included. It might be useful to construct and instrumented short section to observe the behavior of this design.

It is recognized that calculations on the fast track horizontal split yoke must have the highest priority, in as far as they may effect the yoke or collar specifications. But studies on that design, beyond those required for the specification, should give way to those needed for the vertically split yoke.\

6) For the moment, all 5 cm magnets should use kapton and epoxy fiberglass insulation (the standard insulation).

Nevertheless, the BNL studies of alternatives should be continued, and FNAL should try, within reason, to make their tooling capable of using them.

7) In order to allow continuing study of alternatives (all kapton insulation, aluminum bar yoke, aluminum collars etc.), and to have a real horizontally split yoke, BNL end, backup design; the BNL program should be expanded to include full length 5 cm magnets.

The FNAL program will be hard pressed to produce the required magnets for the string test, and does not have the capability to simultaneously pursue possible serious improvements.

If the alternatives are not pursued actively, and with full length magnets, it will not be possible to incorporate them without significant later delay. To try and pursue these alternatives only in industry, or at SSCL, will be too late, and will lack the BNL experience.

If problems should arise in the FNAL magnets, due to any of the changes that they are introducing, a serious delay will be introduced unless we have a real, and tested, backup. For FNAL not to adopt these changes, because there is no backup, would mean accepting serious compromises.

We need, and will continue to need, all the expertise we can get. The BNL group has built all the currently tested full length 4 cm coils and associated yokes. They have their 5 cm work to short magnets will greatly reduce their overall involvement and commitment, and limit our access to their expertise.

Recommended Studies

1) Study of the aluminum collar, aluminum bar, vertically split iron yoke, should continue with relatively high priority. This is a very attractive possibility, but will have to be rapidly developed if it is to be available for use in time. The magnetic design of the yoke is being studied at BNL. If a reasonable solution is found, then a stress analysis should be done as soon as possible. This has less priority than that needed for the BNL or FNAL track specifications, but a higher priority than analysis of those designs, after they are specified.

- 2)Studies (already in progress at BNL and LBL) of alternative methods of correcting the saturation sextupole (with holes, shims, elliptical or other yoke shapes should also continue).
- 3) Study of the fishbone an and quench venting problem should continue, but this does not now seem to be a high priority question.
- 4) Studies should also continue of alternative coil arrangements to lower peak fields, simplify construction, and have wedge in the inner layer opposite the pole shim of the outer layer. But these too can continue with relatively low priority. They can be incorporated with little perturbation at a later time.

Subjects For Next Task Force :

slip planes, teflon and shoes.

End questions: iron, clamping, splice, spacers, interconnects etc.

Review of ongoing studies

Future Meetings:

April 10, 1990	at SSCL	10:00 am to 6:00 pm	Building 1, Suite 285
May 3, 1990	at LBL	9:00 am to 4:00 pm	
May 9-10, 1990	at SSCL		

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