3/29/90

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Subj: Preliminary results on teflon slip planes in DS0307

I have looked briefly at the strain gage data taken during multiple collaring cycles of DSO307 to see what effect, if any, the presence of teflon slip planes has on the force balance between the press (which presumably corresponds to the coil stress at the mid-plane) and the coil stress at the pole. The data discussed here were taken under several conditions: no teflon, 3 mil teflon adhesive tape attached to the coil "caps" similar to the method used by BNL and LBL and non-adhesive teflon plumber's tape burnished into the surfaces of the coils. The adhesive teflon tape was applied to the outer surfaces of the inner and outer coils caps. The plumber's tape was applied to the outer surface of the inner coil and both surfaces of the outer coil.

There are two confounding variable: 1) For the earlier tests every other hydraulic cylinder was valved off, while in later tests the full press load was used and 2) Between the tests with adhesive teflon tape and plumber's tape the outer coils were replace because one of the original coils was damaged during disassembly. Alternate press cylinders are staggered relative to the press center line. With every other cylinder valved off, the press tended to close asymmetrically. This is not believed to compromise the quality of the data. However, because of the model magnet length is not large relative to the spacing between the hydraulic cylinders it is difficult to know what the effective press load was on the active part of the coil in the earlier tests making it difficult to make quantitative measurements of force balance under these conditions. Fortunately a complete set of data exists with the press in this asymmetric configuration so a valid comparison of the different collaring conditions can be made.

More serious is the change of coils between the two different teflon tests. The original coils were molded with fiberglass tape with a high epoxy content (25%?), while the substitute coils used tape with a low epoxy content (18%?). The first coils had a smooth epoxy finish on both surfaces while the second coils had a rougher finish. It is not obvious, however, which one results in a lower friction coefficient against kapton.

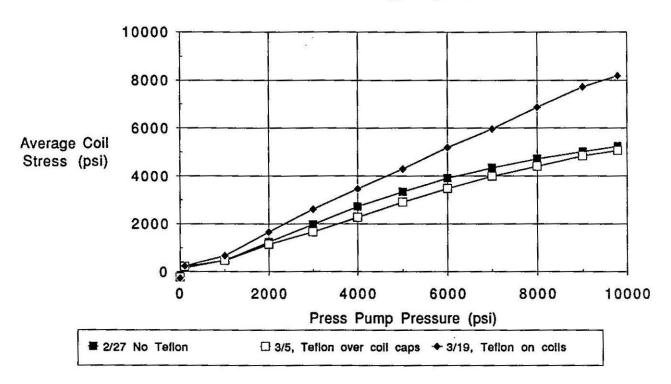
Part of the same set of experiments involved adding several mils of radial shim between the collars and the collaring tooling. Between the time the tooling was design and the collars were designed, the radius of the collars shrank by 2 mils. In addition the collars were punched with a radius 1 mil smaller than the design, making them 3 mils smaller than the tooling. It was conjectured that this allowed the collars to bend outwards

making it harder to insert the keys and wasted some of the vertical press load. To test this DSO307 was compressed in the collaring press with radial shims of 0, 3 and 6 mils. This was done with plumber's tape applied to the coils, once with the press in the asymmetric configuration and once with all cylinders energized.

Figure 1 plots the average coil stress versus the press hydraulic system pressure for the three different teflon configurations with half of the press cylinders turned off. The addition of adhesive teflon tape to the coil caps has no significant effect on the fraction of the press load that appears at the coil pole. With plumber's tape applied to the coils there is an apparent large increase in the force transfer. However, because the outer coils are different for this test, it is not certain that this is a result of the teflon. Figure 2 shows the same data for three different radial shim thicknesses now with the full press energized. There is no significan difference among the three in terms of force balance. Because the keys were inserted only on the third trial it is not know whether collar bending with no shim makes a difference for key insertion. A copy of the portion of the Excel spread sheet that contains the analysed data is attached as Table I.

Because the plumber's tape, once burnished into the coils, cannot be entirely removed, the no-teflon and adhesive teflon experiments cannot be repeated with these coils. A set of 4 new test coils with "junk" ends is currently being wound to allow a complete comparison of the three teflon configurations with a common set of coils and with the press operated in the proper way.

DS0307 Collaring, Assymetric Press



Figurel

DS0307A, Teflon On Coil, Symmetric Press

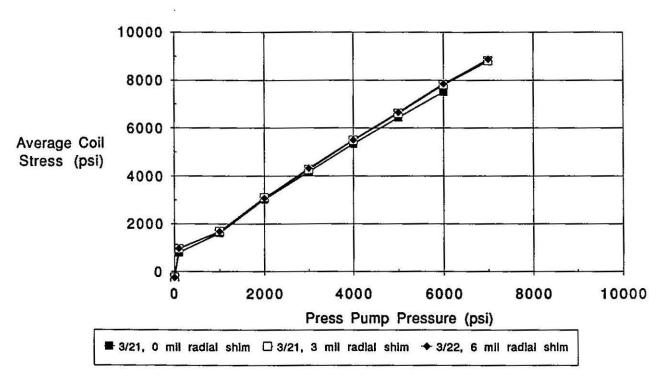


Figure 2

ГТ	AP	T 40	AR	AS	AT	AU	AV	AW	AX	AY	AZ	. BA	BR .	BC BC	80	RF.	86
1	PUMP PSI 2/27/90 A.M. KEYING	7		#169-1 coil psi										AND STORE	d(in)/dPv	d(out)/dPv	d(avg)/dPv
3	No Tellon, Asymmetric Press											2/27 No Tello	2/27 No Tel	2/27 No Tell	2/27 No Tell	2/27 No Tello	2/27 No Tello
3	Press 0	0	0	-29		-78	-180	-270									
4	Line V	100	0	1387		-373 -526	1081	-318 38								0.39	
6	2000 V	2000	0	2231				772									0.76
7	3000 V	3000	0	2807		98		1374								0.89	
	4000 V	4000	0	3481			3615	1902	750							0,87	0.75
8	5000 V	6000	0	3950		1166	4308	2357	1073			2845				0.72	
10	6000 V	7000	0	4468		1679	5040 6848	2707 2987	1824		9353					0.65	
12	8000 V	8000	0	5145	2670	2193	6185	3214	1841							0,43	
13	9000 V	9000	0	5366	2623	2442	6629	3407	2024		11795					0.34	
14	9800 V	9800	0	6648	2948	2637	8998	3529	2132		12310		5976			0.32	0.29
15	9800 V/400 H	9800	400	5841	3159	2918	7467	3784	2343		12953	4646		5592			
16	9800 V/1000 H 4000 V/ 1000 H	4000	1000	6287 5980	3455 3266	3326 2707	8145 7308	4192 4138	2669 2544		13780		6867				
18	Press 0	0	0	5259	2741	1416	5521	3535	1924								
10	press 0	0	0	4901	2505	1100	5183	3324	1768	3908	8038	3422	4407	3916			
20	4000V/400H	4000	400	6029	2702	2173	6296	3281	1898				6191				
31	9800V/400H	8800	1000	6386	3561	3370	8285	4088	2650								
22	9800V/1000H 4000V/1000H	9800	1000	6358	3644	3708 3068	8763 7839	4374	2862 2749				6378				
24	0V/0H	0	0	5403	3008	1911	8074	3911	2167		9817						
26	press 0 2/25/90	0	0	5328	2843	1625	5809	3709	2023		9143		4880				
26	9					-78											
27 28 T	PUMP PSI 3/5/90 KEYING	Press pal (V)	Press pel (H)	#169-1 coli psi	1198-1 coll pa	#184-o coll p	184-0 OON PE	1005- CON PT	11004-1 coll pr	183-0 00# 01	188-e cell pe	Avg in Stees	Avo Out Stress	Avg Stress	d(in)/dPv	d(out)/dPv	
28	ellon Over Coil Caps, Assymetric Press Bench 0 3/5/90		. 0	-33	-462	-80	-222	-225	-542	-68		effor over coi		-223		SHOU OASL OO	ENOU DAM DO
30	Line V	100	0	879	-73	-143	296	-185	-394				222			4.67	4,54
31	1000 V	1000	0	1280	223	-243	470	87	-197	361	1727	432	492	462	0,21	0.30	0.26
32	2000 A	2000	0	2442	1055	-246	901	850	449		2861					0.76	
33	3000 Y	3000	0	3162	1609	-100	1228	1360	885		3734	1475	1849			0.60	
36	4000 V 5000 V	4000 5000	. 0	3880 4601	2158 2751	126 476	1603 2110	1940	1329 1750		4862 - 5992	1942	2588			0.74	
36	6000 V	8000	0	6179	3204	779	2591	2894	2145		7194	2938	3310			0,72	
37	7000 V	7000	ŏ	5705	3592	1092	3201	3271	2508		8222	3397	4588			0.58	
38	8000 V	8000	0	6089	3837	1287	3675	3574	2823	4833	9169	3722	6100			0,61	
39	9000 V	9000	0	6555	4186	1584	4255	3858	3118	5264	9935	4145	5544			0,44	
40	9600 V	9800	0	6752	4320	1710	4525	3990	3257	5529	10414	4327	6797			0.32	0.27
41	\$600 V/400 H	9800	1000	7018 7580	4515 4937	1951 2341	4989 5682	4266 4726	3511 3959	5898 8548	10924	4618 5136	6149				
43	4000 V/ 1000 H	4000	1000	8558	3986	1635	4674	4014	3236	5285	9978	4213	6628				
44	Press 0	0	0	5172	3018	608	3319	3213	2348		7117	3029	4088			100000	2000
45	Press 0 3/6/90	0_	0	4799	2762	388	3013	2955	2140		6523	2740	3769	3250			
45	4000V/400 H	4000	400	5646	3392	1107	3850	3684	2858	4725	8143	3499	4855	4177			SCOTTAGE STOR
48	9800 V/400 H	9800	1000	7655 7916	5179 5284	2506 2768	6821 6226	5138 5331	4265 4466	7426 7699	11661	5290 5548	7120 7402	6205			
40	4000 V/1000 H	4000	1000	6281	3908	1678	4776	4216	3420	5084	9977	4161	5674	4917			
60	Press 0	9	0	5141	3115	843	3585	3380	2488	4124	8892	3176	4721	3948			
11	press 0 3/8/90	0	0	4988	2982	708	3459	3191	2342	3873	7035	3034	4110				
52 53	4000V/400 H	9800	400	5717 6643	3479 4237	1142 1785	4233 5179	3573 4230	2761 3425	4908 6177	8349 9867	3643 4461	4897 6925	4270 5193			
54	9600 V/1000 H	9800	1000	6604	4254	1820	6203	4263	3438	6208	9846	4470	6938	5204			
55	4000 V/1000 H	4000	1000	6741	3587	1282	4400	3710	2876	5131	8412	3763	5082	4417		er e#=	
5.5	Press 0			4997	3046	785	3829	3230	2387	3999	7164	3089	4193	3641			
68	PUMP PSI 3/19/90	Property of the	Breen bel (18	#169-i coli psi				1006.1	11004						etterteto	diametric Co.	diam'idB:
50	Tellon on colls, Asymmetric Press	Lines her (a)	Cises pai (n)	a tank com bar	. se-i con pi	10-4 COR PE	total con be	INVEST CON DI	TOWER CON DE	183-0 00# PE	144-6 CON DE	3/19, Tellon	3/19. Tellon	3/19 Teller	3/19. Teston	d(out)/dPv	3/19 Tellon
60	o v	0	. 0	-158	-550	-115	-212	-356	-494	-118	-121	-259	-273	-266			
61	Line V	100	0	400	-573	137	858	-296	-344	576	1309	166	311	233	4.14	5.84	4.99
63	1000 V	1000	0	686	-367	549	1190	-69	-261		2249	615	835			0,68	0.49
63	2000 V 3000 V	3000	0	1182 1718	30 436	1565 2607	2446 3585	407 797	359	3293 4996	4338 6334	1306	2026 3121		0.79 0.7a	1,19	0.99
66	4000 V	4000		2289	873	3678	4658	1190	660	6528	7782	2875	4040			0,92	0,85
8.6	5000 V	5000	0	2818	1288	4692	6623	1611	956	8127	9329	3605	5004	4308	0.73	0,97	0.85
67	6000 Y	6000	0	3402	1786	4214	6720	2007	1250	9556	10833	4632	5861	6198	0.93	0.88	0.69
68	7000 V	7000	0	3912	2216	6763	7643	2475	1580	11041	12111	6133	6801	5987	0.60	0,94	0.77
70	8000 V	9000	0	4590 5175	2824 3285	7936 8798	9997	2892	1904	12424	13461	6065 6514	7868 8821	6887	0.93	0.87	0.90
71	9000 V	9800	- 0	6519	3542	9245	10840	3601	2310 2514		16019	7285	9081	7717 8184	0,76	0.95	0.86
72	0 v	0	ě	-171	-628	-112	-157	-405	-605		-42	-267	-278			0.95	
_							1-11						7.4			71771	4174

	122112211211	11111111111		9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PULLIP PSI VIZZAG B JOY AMAK EYIMG Telion en Cols, e mil radial shim, 0 V Line V 1000 V 2000 V 2000 V 2000 V 2000 V 4000 V 4000 V 7000 V 1400 H 7000 V 1400 H 3000 V 1000 H	Plan P ES 3/21 no P M. Telon on Cells, 3 mit rodul sten 0 V 1000 V 1000 V 2000 V 2000 V 4000 V 6000 V 6000 V 7000 V 7000 V	3	P-LALP FS; 3-70*90 PM  REPORT OF COME, ALAYM FS; 8 mil rad plan  1000 V  2000 V  2000 V  2000 V  4000 V  4000 V  5000 V	APP PLANE PSI 3/2000 AM PSI 4/2000 AM O V 1000 V
Press pel (V) 100 100 2000 3000 4000 5000 7000 7000 7000 3000	1000 1000 2000 3000 4000 6000 6000 7000	Press pel (V) 0 100 1000 2000 2000 4000 6000	7 Press pti (V) 100 100 2000 3000 4080 6000 6000 6000 6000 6000	Pass pil (V) 0 1000 2000 3000 4000 6000 6000 6000 9000
Press, pd. (H) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Press psi (H)	Press psi [H]	Press pel (V) Press pel (H) 0 0 0 100 0 0 2000 0 0 2000 0 0 4000 0 0 4000 0 0 4000 0 0 4000 0 0 4000 0 0 4000 0 0	Press psi [H]
1147 147 147 147 147 147 147 147 147 147	#1891 ON Pal Ps	-126 -128 -502 -502 -502 -729 -2729 -3592 -3697 -769	-137 -137 -137 -137 -137 -137 -122 -716 -1442 -199 -259 -259 -259 -259 -259 -259 -259 -2	AS #169-1 ONI PAI 
-574 -574 -236 -236 -236 -226 -1202 -1202 -1202 -1202 -1203 -1203 -1204 -1206	-588 -321 -50 -50 -50 -50 -50 -50 -50 -50 -50 -50		1794-1 COH pp11 -523 -328 -328 -328 -328 -1185 -1185 -1184 -1181 -774_UEI -3281 -3281 -3881 -3881	AT 198-1 coll ps1563563563563563563563563564
184-0 coll pp11 -80 -78 -78 -1480 -2948 -2948 -653 -653 -652 -922 -922 -922 -922 -922 -922 -922 -9	- 62 - 62 - 842 - 1580 - 3027 - 4378 - 6714 - 7081 - 8403 - 79	#184-0 coll ## 7-87 7-22 1546 3006 4339 5-858 6967 8967	44-9 coli pri 412 412 407 2030 2044 4013 4082 4082 4082 4082 4082 4082 4082 4082	AU 184-0 coli pei -96 -96 -97 -97 -97 -97 -97 -97 -97 -97 -97 -97
188-8 ody pp 100 -16.7 -18.1 -27.9 -47.02 -9.73 -9.43 -11.09 -12.340 -12.340 -13.12 -10.66 -13.18	184-0 coll p#100 1482 1482 1996 2970 4937 4937 4937 8234 8234 11392 12846 12846	2184-0 cok [#10 -224 1723 2948 4917 4917 4917 4913 9813 19184	784-0 cold pt 184-0 cold pt 1005-1 -76 -1844 -412 1137 -487 1804 -2030 3217 -2030 4316 -4017 4384 -4982 4784 -	AV 1884 o ooil price   1997   1018   1078
1005-1 coll p#1004-1 -32-6 -51 -427 -108-6 -329-6 -329-6 -329-6 -3423 -4423 -4423 -4578 -350-6 -350-	19064 cdi p#19044 -322 35 35 33 33 1474 1474 2197 2978 3311 3331 3348	#1006-1 call p#10 -330 -76 -78 -262 -861 1396 1990 2518 3107 -361	- 286 - 90 - 133 - 1059 - 1059	AW p#10 1005-1 coll p#10 -58.2 -16.7 -6.7 -6.7 -6.7 -6.7 -6.7 -6.7 -6.7 -
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113-0 0-8 pril 1916 1916 1916 1916 1916 1916 1916 191	183-a coli péti 1797 2996 6233 7052 10664 12506 13966 7	100 04 F148 100 100 100	124 00 pt 1 26 2128 2122 4037 4037 4037 4037 4037 10786 10786 1078 1078 1078 1078 1078 1078 1078 1078	AY P1133-0 001 P1133-0 001 P1133-0 001 P1133-0 001 P1133-0 P11
188 - 60H pt. 2940 2940 4495 7438 1888 1888 1888 1888 1888 1888 1888 1	-20 3009 4890 7633 12008 13866 15866 17616	-0 00M 2849 4454 7304 9363 11422 13198 15002 -3	188-0 ool p/Ang in -47 1885 2813 5181 6181 1410 1410 1410 12384 8VA 13380 14053 14053 14053	AZ P161-0 coll p1 1712 1712 2850 5038 6658 6658 10977 1293 13300 14888 14888
Avg in Steas N. 3722, 6 mil rG. 12376 1740 1740 17376	Aig In Stress N 3/21, 3 ml r13 3/21, 3 ml r13 7/41 1369 2569 3599 4792 6902 6902 7987 -226	Avg in Stress A 3/21, 0 m8 r3 -263 -263 -2691 -2691 -2691 -2691 -2691 -2691 -241	-225 421 405 1749 2278 3278 4361 4361 4361 4361	8A 89 Any In Sees key Out Street
Ng Ox Stea 372 6 mil (4) -227 1201 1201 1201 3643 622 622 7524 623 623 623 623 623 623 623 623	Ny Od Stest 3/21, 3 ml r3 1163 1199 3608 4639 6183 7135 8617 -215	I Ayy O.: Seed Ayy	Wg Out Street -213 720 1292 2546 4479 6169 6169 6164 6169 6169 6762	99 Out Stress -267 676 1199 2408 -3452 4353 6217 6048 6816 6816 6816 6816 6816 6816 6816
U. Sires. Any. Sires.  8 mil 13/22, 6 mil 13/22, 12/21 22/1 970 22/4 970 20/4 10/64 36/21 30/66 6/22 4/327 6/24 4/327 6/24 4/327 6/24 4/327 6/24 4/327 6/24 4/327 6/27 6/26 6/27	(4.021, 3 mil 13/2 7 .238 9.52 10 .952 10 .952	Avy Svess (3/21, 0 mll r/3 -242 1 -242 1 -233 1 -3023 1 -3023 1 -315 1 -515 1 -515 1 -525	Avg Sress -219 -565 -607 -1049 -2167 -3079 -4446	Avg Stress -259 446 950 2011 2928 3765 60500 60500 7499 7499
d(in)/dPv 722, 6 mil e 9.77 0.46 1.21 1.08 1.12 1.09 1.12	11.3 mil 1 9.90 9.90 1.22 1.11 1.09 1.01 1.01	1, 0 mil 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	6.34 0.44 0.44 0.75 0.76 0.72 0.72 0.89 0.74 0.89 0.74 0.31 0.31	6.48 0.45 0.45 0.45 0.77 0.77 0.37
deutjdePv 3222, 6 ml r/3 14.27 0,94 1,90 1,20 1,21 1,21 1,21 1,21 1,21	deunydPv 3/21, 3 ml r(3 13.90 0.92 1.23 1.23 1.34 1.16 1.26 1.26 1.40	d(out)/dFv (JZ1, 0 mil r3 11,74 1.06 1.58 1.22 1.22 1.12 1.12	9.32 9.32 0.84 1.25 0.86 0.81 0.83 0.83 0.83 0.83 0.83	0.43 0.43 0.43 0.44 0.44 0.44 0.45 0.44 0.45 0.44 0.47 0.48
0(avg)/dPv 3z2, 0 mil i 12.02 0.79 1.40 1.24 1.18 1.19 1.00	(4.89)/dPv 121, 3 mil r 11.90 0.81 1.42 1.17 1.22 1.17 1.22 1.10 1.10 1.20 1.20	d(avg)4Pv 3/21, 0 mil r 10.37 0.92 1.40 1.16 1.16 1.16 1.16 1.08	7.94 0.54 0.154 0.154 0.170 0.77 0.77 0.78 0.30 0.30	7.05 7.05 0.57 1.05 0.92 0.92 0.92 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93

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