

Commissioning, Performance, and Effect of the Quench Current-boosting Device on a Dedicated Superconducting Magnet

S. Stoynev, M. Baldini, S. Feher

Abstract—Superconducting magnet training is one of the accelerator related issues attracting attention due to significant operational costs and time budget associated to it. It is especially worrisome that magnets based on the “next-generation” Nb₃Sn technology are affected by long training. While various efforts are underway to better understand and resolve the problem a parallel path could also be investigated, a path bypassing the issue. Following the concept of fast induced over-current during magnet powering, FNAL has developed an upgradable capacitor-based device to discharge through a superconducting magnet at quench detection or operator chosen time. The 0.4 F/1 kV device has been tested on a 1-m-long dipole-coil in a “mirror” magnet configuration and conclusive results on magnet training elimination have been observed. In this paper we discuss the main characteristics of the device, compare simulated response and actual performance, elaborate on test drivers and outcomes. Next steps and perspectives for future use are debated.

Index Terms—Accelerator magnets, pulsed power supplies, superconducting magnets.

I. INTRODUCTION

BUILDING state-of-the-art superconducting accelerator magnets is a delicate process and, among other things, it involves a careful “pre-stress” setting aiming to minimize conductor degradation and optimize performance. This step could be considered “pre-conditioning” [1, Chapter 1.2.5] of the magnet. However, one can expand the meaning of “pre-conditioning” to include any process that would affect magnet performance positively. Here we choose to separate action taken before magnet powering and during magnet powering - “pre-conditioning” and “operational conditioning”, respectively. “Pre-conditioning” was considered and experimented with in past [2], [3]. It is known to the authors that “operational conditioning” was conducted in the past too, but we could find no clear reference. That for instance includes manipulating current ramping (levels, rates) to avoid lower current quenches though it is purely an investigative technique.

The work described in the present paper builds up on [2] where capacitors were discharged through a magnet as a “pre-conditioning” step. We do this as “operational conditioning”. In our case, a capacitor is discharged through a magnet being

powered at a user defined time, for instance at quench detection. This boosts the current through the magnet to levels depending on circuit parameters, including magnet parameters. Such a boost could effectively increase the magnet current associated to a given quench although a “quenchless” mode will be debated later too. Given that magnet training is understood as the steady increase of quench current after consecutive spontaneous quenches, changing the current level at quench is a lever to affect training. Authors are aware of possible phase delays between operating current and local force [4] in pulsed mode although expectations pointed to time delays of low tens of milli-seconds at most. Our own measurements of magnetic field in magnet bore and magnet current during the sharp decrease of current during system trips and quenches (with immediate magnet protection) did not indicate any phase delays between magnet current and bore field beyond our resolution of a couple of milli-seconds. If present, significant local phase delays, originating from decaying eddy currents, could suppress the Lorentz force peak experienced by the superconductor/coil and diminish the effect of fast current boosts.

The work to bring the boost ideas to fruition was supported by LDRD funds at FNAL and the resulting device [5] is in effect a pulsed power supply integrated into the main power supply CPS3 [6] with ability to be controlled independently. We call it Quench Current-boosting Device, or QCD. QCD has similarities to CLIQ [7] but is a very different device. Apart from being used for different purposes, there are two other major differences: a) the QCD boost current is the same through the whole magnet, i.e., there is no difference in magnet Lorentz force distribution with respect to “regular” ramp-up; b) QCD has no current/voltage oscillation features. QCD drawings and design/fabrication details are found in [5].

This paper describes the first application of QCD on a dedicated superconducting magnet, points to relevance of simulations before and during testing, reviews choices made during testing and results obtained; those are followed by a discussion on future use of QCD and the technique itself.

II. QCD COMMISSIONING AND MAGNET TESTING

A. QCD preparations and simulations

QCD [5] started working as a unit towards the end of 2021 and was gradually integrated to CPS3. After all major components and sub-circuits were verified and tested, the device went through various full circuit examinations, including

This work was supported by Fermi Research Alliance, LLC, under Contract DE-AC02-07CH11359 with the U.S. Department of Energy, Office of Science, Office of High Energy Physics. (Corresponding author: Stoyan Stoynev.)

The authors are with Fermilab National Accelerator Laboratory, Batavia, IL 60510 USA (e-mail: stoyan@fnal.gov).

Digital Object Identifier will be inserted here upon acceptance.

powering. Before using it on a superconducting magnet, a conventional accelerator magnet (fabricated for use in the FNAL accelerator complex) was utilized as a load to demonstrate operation. Engineers from Accelerator Division of FNAL, who developed the device engineering concepts and worked through the process all the way to commissioning, also helped with circuit simulations. LTspice software [8] was employed allowing to explore sensitivity and responses to various parameters in the circuit, including magnet inductance and ability for time dependent resistance modeling of the load. The simulation was initially successfully verified with the conventional magnet with known inductance and resistance where discharged currents were limited to several kA.

B. Training of Superconducting Magnets and QCD Baseline

Superconducting magnets still train [9], [10], [11] and this remains a major issue to resolve [12]. Since QCD is supposed to affect the training curve, a solid baseline for comparison is desired. A performance summary of magnet series tested at FNAL showed that “11 T” (dipoles) and “LARP” (quadrupoles) short models provided good reproducible training trends [10]. It was also concluded there that, to a good degree, coils inside magnets train independently, and coils in “mirror” magnets [13] train similarly to coils in “complete” (dipole/quadrupole) magnets. Thus, a “mirror” magnet is well suited for QCD testing. We chose to start with the “11 T” series as the training pattern baseline for QCD testing.

There are several features in magnet, or rather coil, training important in the current context, general discussion is found in [10]. When quench current is away from conductor limit coil training is largely independent on liquid helium temperature, i.e., quench current would be the same at 4.2 K and at 1.9 K. The behavior is drastically different close to the conductor limit - transitioning from higher to lower temperature after training, for instance, would initiate an additional training sequence. Damaged coils could exhibit variety of dependencies and features, depending on the nature of the damage, and current may be limited below conductor limit. However, all coils in the “11 T” baseline behaved “normally” in that respect with no abnormal dependencies observed.

C. Superconducting Magnet Testing with and without QCD

A “mirror” magnet [13] from the “11 T” series [1, Chapter 8] was assembled specifically for QCD testing. It employed a coil which was fabricated as the last coil (#12) of the “11 T” program at FNAL many years ago and was never used. It was the third “11 T” “mirror” magnet assembled with similar parameters. The first low-voltage QCD discharges at up to few kA trip-current through this magnet were conducted on March 1st, 2022, as part of magnet check out. The first discharge at a spontaneous quench occurred on March 2nd. All initial magnet training was at 4.5 K following the established baseline.

To compare to the baseline as directly as possible, QCD was discharged at quench detection time while ramping conditions (temperature, ramp rate) were kept nominal with respect

to baseline. Simulations showed that the current boost needed 15-20 ms to reach its peak and that delaying magnet protection by 50 ms is safe for the magnet for quench currents below 12 kA. We did not have complete multi-physics simulation to know the expected effect of quench-back which was inevitable at such large current differential dI/dt . Thus, we did not know the expected resistance growth in the magnet, we conservatively ignored it while making protection assessments.

Before testing at high magnet current, we had to make major decisions based on partial or no information. Among those, we did not know the importance of the “over-current” (levels above the “quench current”) shape or duration on performance/training. We hypothesized there may be some “effective” current, below the peak boost current, which represents the integral boost effect and is more relevant for training than the peak current; the only available reference [2] considered pulse time duration to be of importance. At this time, we had one magnet and one shot (test sequence) to investigate. Our main handle was settable QCD voltage, up to 1 kV, affecting the boost current. There was the possibility that even with high peak boost current we could be too low in “effective” current to observe any effect from QCD. On the other hand, the “effective” current may be close or equal to the peak current which may be high long enough to damage the magnet and halt any further QCD testing. There was also the remote possibility that the fast discharge process at high magnet current and QCD voltage may affect the magnet integrity negatively. In our steps we tried to navigate through those risks.

The first spontaneous quench with immediate QCD application did occur at expected current level (~ 9 kA, [10]) and we chose QCD voltage of 800 V providing a substantial boost. Retrospectively, we found the resistance growth in the magnet to approximately follow linear trends: 0-35 m Ω from 5 to 22 ms after quench detection and 35-50 m Ω from 22 to 42 ms after detection; this dependence was embedded in the LTspice simulation along with negligibly small quench spot resistance. Fig. 1 then compares the updated simulation, with the observed real magnet current shape. The good description of cur-

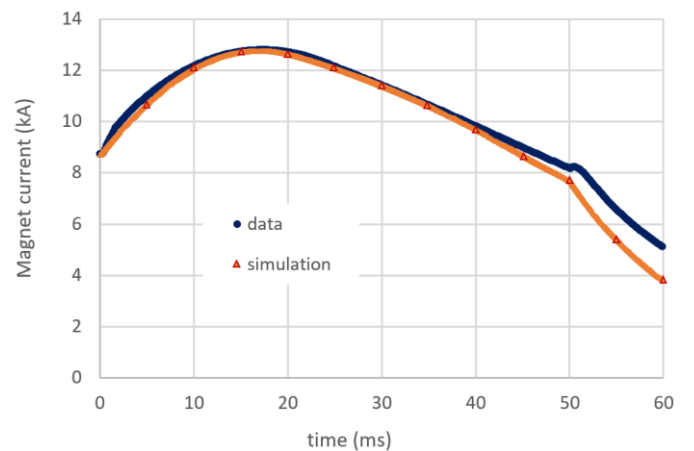


Fig. 1. Magnet current development after quench detection (0 ms) in the first ramp, driven by QCD. There is 50 ms delay of dump resistor firing and 30 ms delay of protection heater firing but the latter has its own response time to affect the conductor. The simulation is not perfect: it assumes constant magnet inductance of 1.4 mH (measured 2.0/1.75 mH at $\sim 4/7$ kA), magnet resistance development is approximate.

rent development gave us confidence to proceed with a higher boost current in the next quench allowing for longer “over-current” time. No abnormal behavior in monitored signals from the magnet was observed.

The second spontaneous quench occurred at current level well above the first one but the third went down, well below the expected level from the baseline. The QCD voltage was at the maximum 1 kV; no abnormal data signals were observed.

After the third quench the QCD voltage was dropped to 500 V, able to boost the current to ~ 11 kA given that quench current level stays the same. Several more quenches confirmed the magnet is at a current plateau, within a wide range. At this point our baseline approach was failing. We continued to follow our test plan and lowered the temperature to 1.9 K for further testing, initially keeping QCD voltage of 500 V. Then we moved on to perform several thermal cycles (TC).

Fig. 2 shows the complete quench history of the “mirror” magnet at nominal ramp rate (20 A/s) and temperatures (4.5/1.9 K). The quenches at 1.9 K in TC1 were all in a narrow current plateau at the same fraction of Short Sample Limit (SSL) as the 4.5 K level, namely $\sim 70\%$. We stopped using QCD in the last two 1.9 K quenches, the quench current levels remained the same. Consequent 4.5 K quenches returned to the current level observed earlier at 4.5 K. Quench current dependence on ramp rate was determined and was consistent with earlier “11 T” magnet coils [1, Chapter 8], including “mirror” magnet coils. Conclusions at this point were that the coil reached conductor limit, albeit very low one, without training between 4.5 K and 1.9 K unlike other “11 T” coils or any other accelerator magnet training ever observed. TC1 and all following thermal cycles ended at room temperature with the magnet remaining in the test facility cryostat.

TC2 training started at 1.9 K without any use of QCD. The magnet forgot its training practically entirely, which is unusual for Nb_3Sn accelerator magnets, and needed 4 training quenches to reach the fraction of SSL observed in TC1. Quenches at 4.5 K re-confirmed conductor limitation as in TC1. QCD discharges were re-introduced for TC3 with capacitor voltage of 800 V and 500 V in the first and second quenches (1.9 K), respectively. The first quench of TC3 was at the same current

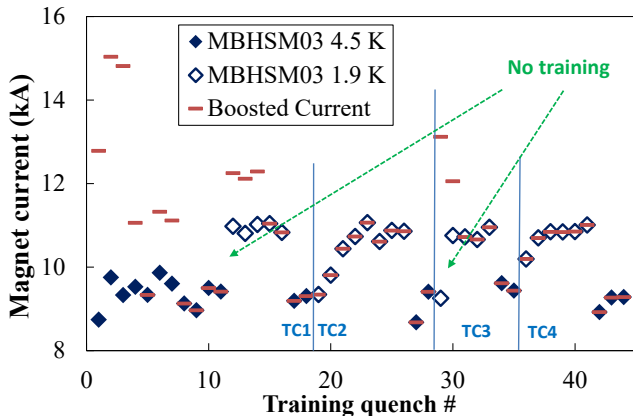


Fig. 2. Spontaneous quenches at nominal ramp rate – magnet current at quench detection vs quench number; boosted current at its peak is shown as well; the two currents differ only if QCD is applied. All four thermal cycles (TC) are included in the plot. Lack of training quenches is indicated.

level as in TC2. The second quench along with few more quenches were at conductor limit clearly indicating the effect of QCD on the training curve; later quenches at 4.5 K confirmed conductor limitation. The picture from TC1 to TC3 is quite unambiguous. In TC4 we did not use QCD and wanted to demonstrate again magnet training, but this time training was not fully forgotten by the magnet. Still, the first two quenches were identified as “training” based on quench location in the first layer. All limiting quenches in all TCs and at both temperatures were identified in the outer coil layer, including the last ones at 4.5 K in TC4.

III. QCD DISCUSSIONS

A. Discussion on Magnet and QCD Performance

The “mirror” magnet coil tested clearly underperformed compared to other “11 T” coils (as presented in [10]). A question arises if this has to do with QCD in any way.

The QCD capacitor discharge in the second quench (highest boost current reached) drove the current rise at $dI/dt \sim 1$ MA/s in the first two ms and ~ 0.5 MA/s in the next 2 ms, easing substantially after that. The average increase to peak was 0.3 MA/s. In comparison, CLIQ discharges, which have somewhat similar dI/dt characteristics in the first 10-15 ms have an average increase to peak of 0.15 MA/s (dependencies exist, data from non-“11 T” magnets). Moreover, regular quench protection itself in small magnets drives dI/dt as ~ 0.5 MA/s in the first 5 ms. All this is to say QCD pushes to higher differential current increases but those are still of the same order as known applications. Analysis of energy flow and energy density in the magnet, including the QCD energy introduced to the system, shows that the magnet bulk temperature never exceeded 150 K and the hot-spot temperature was below 210 K after current dump. We used the cable enthalpy estimates from ([14], Fig 13) and quench integral calculations from [15].

The coil used in the present test featured all improvements made during the “11 T” program. However, it was fabricated by a partially different (new) team at the time. The team assembling the magnet was also different than earlier magnets. Fig. 3 shows a prominent non-planarity feature of the coil and uncharacteristic cracks observed in the non-lead end, outer layer of the coil. This area is consistent with all limiting quench locations as observed by quench antenna [16]. Quenching at this area yielded a characteristic QA signal development pattern, up to quench detection, in several channels. The same pattern was identified immediately after the very

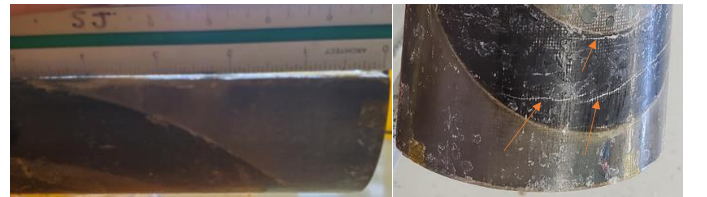


Fig. 3. Unusual non-conformities on the coil. Left: significant non-planarity at the coil mid-plane (non-lead end), since coil fabrication; Right: cracks (pointed to by orange arrows) on the coil non-lead end, outer layer, post-testing.

first quench in the inner layer too, pointing to pre-existing conditions for the under-performance. We hypothesize that the coil shimming corrections with Kapton layers, based on average deviations, could not fix in full the abnormal divergence from flatness observed on the non-lead end and this caused tension and over-stress on the coil non-lead end outer layer.

QCD developments aimed to investigate timing characteristics of accelerator magnet training. The typical magnet ramp rate range is 1-300 A/s (nominally ~ 10 A/s), and data suggest magnets train regardless of ramp rate. Average current gains after spontaneous training quenches vary but they are of the order of 100 A. Thus, training mechanisms act, nominally, within 10 s. With QCD one can test characteristic times up to tens of ms with low limit driven by practical limitations. QCD does not change current distribution across the magnet, and truly emulates known training conditions but at higher ramp rate. QCD results so far show coil training can be affected at ~ 30 ms timescale, it is a significant step from the known seconds-range. If it holds that coils train independently [10] then we can conclude that CLIQ [7] too affects training but training quenches in magnets shall occur predominantly in coils with no over-current (due to CLIQ).

Another effect of QCD in support of training reduction can be seen through the Kaiser effect [17], [18] which is well established in magnets [19] – they become “quieter” at “known” current levels. If the short pulse of QCD affects magnets then the “known” current level is higher than the quench current. Fig. 4 describes a way to visualize mechanical activity during a whole TC by “stitching” plots together, for presentation purposes. We chose this form of data presentation due to complicated signal noise and process transparency considerations. The plot on the left on Fig. 4 shows current and acoustic signals for the first ramp to quench in TC3. Current ramp numbers, Q_i (i is an integer), are enumerated in consecutive order for a given TC and temperature, following Fig. 2. For instance, in TC1 there were 11 consecutive ramps at 4.5 K (Q_1, \dots, Q_{11}) followed by five ramps at 1.9 K (Q_1, \dots, Q_5). Temperatures are not marked when only 1.9 K data are used for a given TC and thus the plot under discussion on Fig. 4 is labeled TC3, Q1. The current signal on the plot has a kink at the time when the ramp rate changes from 50 A/s to 20 A/s, which occurs well before quenching. The ramp rate is initially high

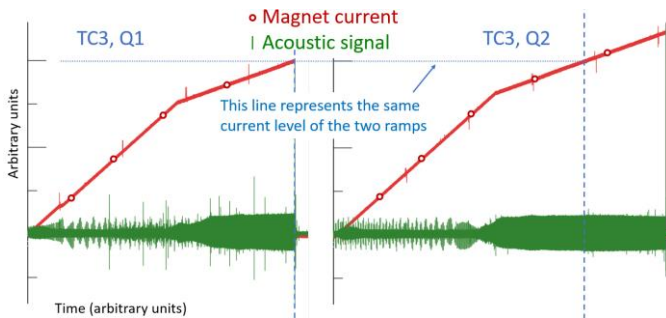


Fig. 4. The procedure of stitching of plots to represent data. The ramp on the left is of the highest current reached before the ramp on the right (for a given TC). Those are not necessarily consecutive ramps. In both, the time on the plots where the horizontal line (highest quench current in the preceding ramp) crosses the current curve is the time where stitching is to be implemented. Data from the ramp on right up to the stitching time is lost after the procedure.

to shorten the duration of the ramp. Spikes can be seen on the current signal in addition to lower random noise which comes from the specific readout line/cable; this noise is of no concern. The acoustic signal shown on the same plot is very noisy which is problematic. The noise is seen as a large nearly symmetrical band around “zero” (in Y-axis direction). It was not well controlled as a function of current and ramp rate, and it was also not consistent over thermal cycles. What is relevant on the plot are the spikes above this noise level – they represent real mechanical activity registered by an acoustic sensor (similar to ones in [19]) placed on a magnet side.

The plot on the right on Fig. 4 shows the second ramp of thermal cycle – TC3, Q2. A horizontal line on the figure indicates the level of quench current seen in Q1, the two ramps are plotted side-by-side at the same scale. Until this current level is reached in Q2 there is very little acoustic activity (spikes) above noise, as expected due to the Kaiser effect. In this sense that part of the plot carries little information, it largely follows what we already know with respect to mechanical activities. Thus, we want to “stitch” the two plots together, as if the ramp Q1 continued to Q2 – such a plot would show non-trivial mechanical behavior up to the higher quench current the magnet reaches in the second ramp. The “stitching” means we discard data from the beginning of the second ramp to the level of current already reached in Q1. This is repeated with following higher current ramps, if any, until the highest quench current is reached. There are only two such ramps for TC3 and the result of the procedure for TC3 is seen on Fig. 5, upper right. More plots are “stitched” in TC2 and TC1 reaching to the highest quench currents in those TCs, Fig. 5. The highest quench currents reached are approximately the same for all TCs (quench plateau), as seen on Fig. 2. Fig. 5 gives relevant multi-ramp and multi-TC information in a single figure. Note that QCD over-current (tens of ms long) cannot be seen at this time scale (minutes for ramps).

With relatively low noise, data from TC1, Fig. 5 upper left,

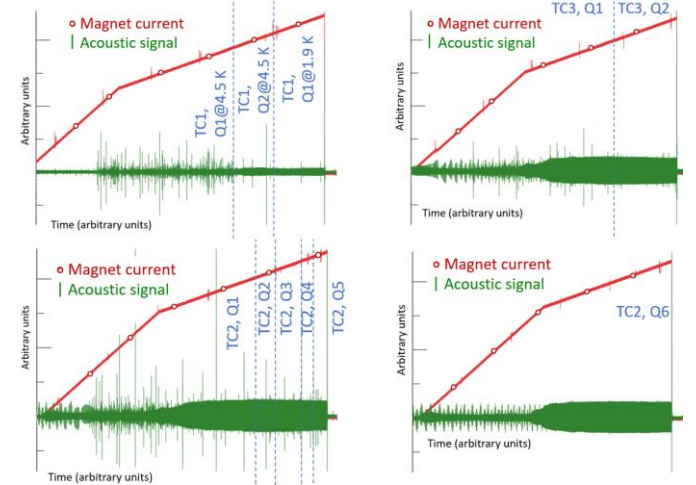


Fig. 5. Acoustics data from the three consecutive thermal cycles. QCD is not applied in TC2. The plots are “stitched” together (note dashed lines representing “stitching” times) from different ramps to quench as described earlier. The lower right plot shows data from the whole ramp to quench after the magnet reached quench current plateau in TC2. The instrumental noise level was not well controlled over time for both current and acoustic signals. Note that the only non-consecutive ramps stitched are in TC1: $Q_2@4.5$ K and $Q_1@1.9$ K.

clearly demonstrates spikes in the first ramp are significantly more per unit of time/current rise, than in the later two ramps shown. Similarly, TC3 on the upper right on Fig. 5, suggests much less mechanical activities in the part of the second ramp shown with respect to the first ramp. In contrast, in TC2, where QCD was not used, significant acoustic activity at higher currents continues up to and including ramp 5 (see bottom plots on Fig. 5 and Fig. 2), followed by a “quiet” ramp 6 shown for comparison. We associate this difference between TCs with the application of QCD at the end of the first ramps in TC1 (Q1@4.5 K) and TC3 (Q1@1.9 K). In other words, the actual forces the coil/magnet sees do associate with the higher boosted current, despite its relatively short duration of few tens of milli-seconds. The Kaiser effect must be associated with this higher boosted current and not the quench current, as confirmed by our data. Present data are not enough to reveal if the maximum of the boosted current is relevant or some lower “effective” value is, but the QCD effect is clearly significant.

B. Discussion on Future of QCD

There are more tests planned to perform with QCD on small magnet models: we still do not know what the relevance of over-current length or shape on training is; nor we know how different magnet designs may behave. However, another important question is on applications to large accelerator magnets. The main hurdle is their larger inductance which limits the current boost level along with the induced by QCD large normal zone. Although the existing QCD can be upgraded in terms of capacitance (C), voltage (U) increase would be more relevant as an upgrade (energy $\sim CU^2$). Fig. 6 shows simulations of QCD with nominal and upgraded parameters for a magnet of 35 mH (a typical HL-LHC Nb₃Sn quadrupole). As seen, a 2-kV-QCD can boost the quench current substantially and thus accelerate magnet training, likely at the expense of magnet insulation requirements. Novel designs with decreased inductance, like bi-filar windings [20], or multi-magnet circuit

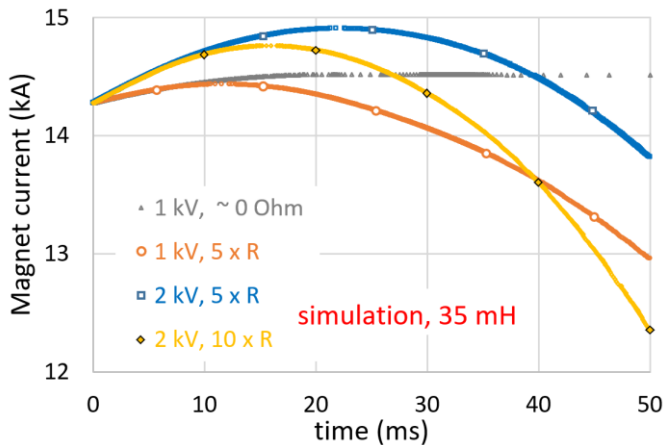


Fig. 6. Magnet current development after quench detection (0 ms): simulations with QCD on a 35 mH load at 14.275 kA “first” quench current (both representing a HL-LHC quadrupole magnet). “R” is the resistance dependence described earlier; actual resistance growth is not known. Compared to the discussed “mirror” magnet, HL-LHC magnets have ~ 15 times the resistance at 300 K, and about twice as large RRR. With 2 kV discharge the current is boosted over 500-600 A with 30-40 ms over-current duration.

designs could benefit more significantly by QCD as is (1 kV).

Although QCD is in effect also a protection device its use does require additional delay for other protection mechanisms – typically protection heaters and dump resistor. The effect of heaters on the conductor comes with a delay of at least 10-20 ms which could be enough for simultaneous operation of QCD and heaters. The main concern of simultaneous operations is voltage developments in parts of the coil. QCD fully discharges (no voltage) soon after reaching maximum boost current and the initial voltage gradient is distributed across the whole magnet [5]. CLIQ [7] drives voltage oscillations until energy is absorbed and the initial voltage gradient is typically applied to half the magnet (asymmetric configuration is unavoidable). A dump resistor is sometimes not used at all with CLIQ due to high-voltage and insulation breakage concerns. QCD does not create issues for quench protection that are different from CLIQ issues, and voltage distributions are easier to control. QCD can operate with no or minimal heaters delay, and a dump resistor can be additionally employed shortly after QCD discharge, within 30-40 ms. More importantly, QCD does not need a quench to operate as a magnet training eliminator. In this mode, there is no hot-spot, per se, and there is no quench detection delay. Operating QCD with series of step-like high-current trips to eventually reach a quench plateau in a magnet will be tested in following magnet experiments. Ultimately, protection issues do not appear to be prohibiting for using QCD though deeper case-by-case analysis may be needed.

IV. CONCLUSIONS

A new device (QCD) aiming to affect superconducting magnet training, has been commissioned, and tested. Results support the notion that QCD-like discharges could eliminate training in superconducting magnets. Possible negative effects of QCD on magnets were investigated but no clear evidence or clues were found. More experiments are needed to determine the limits of capacitor discharges to affect training. Larger accelerator magnets can also benefit from QCD, but they probably need to have better insulation scheme allowing for higher QCD voltage. Novel magnet designs with lower inductance would be more susceptible to QCD. Magnet protection, while applying QCD to reduce training, is not of direct concern due to available options of operation and limited interference between QCD and other methods used for protection.

ACKNOWLEDGMENTS

We thank Howie Pfeffer for actively supporting the phase of QCD commissioning, Matt Kufer for invaluable electrical engineering and help with LTspice simulations, Chris Jensen for leading the overall efforts; AD, MSD and T&I colleagues who contributed to QCD commissioning, data taking and engaged in analysis discussions (D. Durando, L. Elementi, N. Gurley, M. Henry, V. V. Kashikhin, K. Kompiel, S. Krave, A. Makulski, V. Marinozzi, R. Milholland, V. Nikolic, D. Orris, A. Saracino, T. Thode, M. Turenne, G. Velev, A. Yuan); LBNL for help with acoustic instrumentation.

REFERENCES

- [1] “Nb₃Sn Accelerator Magnets”, Schoerling, D., Zlobin, A.V., Eds.; Springer: Berlin/Heidelberg, Germany, 2019.
- [2] Krivykh, A. & Anashkin, O. & Keilin, V., “Elimination of training and degradation of superconducting magnets by electrodynamic treatment”, *Soviet Physics Doklady* (1985). (Available in English on researchgate, record # 241206217)
- [3] M. Tigner, “Magnet R&D for SSC”, *Proceedings of Workshop on Superconducting Magnets and Cryogenics*, p. 6, BNL, May 1986.
- [4] Emmanuele Ravaioli, private communications.
- [5] C. C. Jensen et al., “Pulsed Power Supply for Magnet Quench Training”, *FERMILAB-CONF-22-444-AD-TD*, submitted for publication; <https://lss.fnal.gov/archive/2022/conf/fermilab-conf-22-444-ad-td.pdf>, <https://doi.org/10.2172/1875872>
- [6] R. Carcagno et al., “New 30 kA Power System at Fermilab and Its Use for Measuring the Effects of Ripple Current on the Performance of Superconducting High Field Magnets,” in *IEEE Trans. Appl. Supercond.*, vol. 15, no. 2, pp. 1520-1523, June 2005, doi: 10.1109/TASC.2005.849153.
- [7] E. Ravaioli, “CLIQ A new quench protection technology for superconducting magnets”, PhD Thesis, 2015, 10.3990/1.9789036539081.
- [8] LTspice by Analog Devices, <https://www.analog.com/en/design-center/design-tools-and-calculators/ltspice-simulator.html> (accessed 25 July 2022).
- [9] E. Todesco et al., “Training Behavior of the Main Dipoles in the Large Hadron Collider,” *IEEE Trans. Appl. Supercond.*, vol. 27, no. 4, 4702807, June 2017.
- [10] S. Stoynev et al., “Analysis of Nb₃Sn accelerator magnet training,” *IEEE Trans. Appl. Supercond.*, vol. 29, no. 5, Aug. 2019, Art. no. 4001206, doi:10.1109/TASC.2019.289555.
- [11] P. Ferracin et al., “The HL-LHC Low-β Quadrupole Magnet MQXF: From Short Models to Long Prototypes,” *IEEE Trans. Appl. Supercond.*, vol. 29, no. 5, pp. 1-9, Aug. 2019, Art. no. 4001309, doi: 10.1109/TASC.2019.2895908.
- [12] S. Gourlay et al., The U.S. Magnet Development Program Plan: Lawrence Berkeley National Laboratory. LBNL Report #: LBNL-100604(2016), Retrieved from <https://escholarship.org/uc/item/5178744r>
- [13] N. Andreev et al., “Magnetic Mirror Structure for Testing Shell-Type Quadrupole Coils,” *IEEE Trans. Appl. Supercond.*, vol. 20, no. 3, pp. 288-291, June 2010, doi: 10.1109/TASC.2009.2039704.
- [14] S. I. Bermudez et al., “Analytical method for the prediction of quench initiation and development in accelerator magnets,” *Cryogenics*, Volume 95, October 2018, Pages 102-109, <https://doi.org/10.1016/j.cryogenics.2018.09.004>.
- [15] A. Zlobin et al., “Quench Protection Analysis of a Single-Aperture 11T Nb₃Sn Demonstrator Dipole for LHC Upgrades,” *Conf..Proc..C* 1205201 (2012), 3599-3601.
- [16] S. Stoynev and J. DiMarco, “Assessment and Performance of Flexible Quench Antenna Array Diagnostics for Superconducting Magnets”, *IEEE Trans. Appl. Supercond.*, accepted for publication.
- [17] H. M.Tensi, “The Kaiser effect and its scientific background,” in Proc. 26th 335 Eur. Conf. Acoust. Emission Testing, Berlin, Germany, 2004, pp. 31-42. 336
- [18] J. Kaiser, “A study of acoustic phenomena in tensile test,” Ph.D. dissertation (in German), Tech. Univ., Munich, 1950.
- [19] M. Marchevsky et al., “Acoustic emission during quench training of superconducting accelerator magnets”, *Cryogenics* 49 (2015). 10.1016/j.cryogenics.2015.03.005.
- [20] Steve Krave, private communications.