

Magnetic Analysis of the Nb₃Sn low-beta Quadrupole for the High Luminosity LHC

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Abstract— As part of the Large Hadron Collider Luminosity upgrade (HiLumi-LHC) program, the US LARP collaboration and CERN are working together to design and build 150 mm aperture Nb₃Sn quadrupoles for the LHC interaction regions. A first series of 1.5 m long coils were fabricated, assembled and tested in the first short model. This paper presents the magnetic analysis, comparing magnetic field measurements with the expectations and the field quality requirements. The analysis is focused on the geometrical harmonics, iron saturation effect and cold-warm correlation. Three dimensional effects such as the variability of the field harmonics along the magnet axis and the contribution of the coil ends are also discussed. Moreover, we present the influence of the conductor magnetization and the dynamic effects.

Index Terms— High Luminosity LHC, Field Quality, Magnetic Measurements, High Field Nb₃Sn Magnet.

I. INTRODUCTION

THE high luminosity LHC upgrade aims at increasing the integrated luminosity of the LHC by a factor of 10 beyond its nominal performance expected for 2023 [1]. Part of the upgrade relies on the replacement of the single aperture quadrupoles in the interaction region (the so called low-β or inner triplet quadrupoles). The design, referred as MQXF, foresees a 150 mm aperture quadrupole based on Nb₃Sn technology [2]. The first MQXF short model (MQXFS1a) has been assembled in LBNL [4] and tested at FNAL [5], using two coils produced by LARP (coils 3 and 5) and two coils produced by CERN (coils 103 and 104). The four coils are made using OST Restacked-Rod-Process (RRP) Nb₃Sn wires, using 108/127 stack for LARP coils and 132/169 stack for CERN coils. This paper presents the results and analysis of the magnetic measurements performed on MQXFS1a.

II. MAGNET DESIGN

The cross-section of the MQXF quadrupole magnet is shown in Fig. 1 and the main dimensional parameters of the magnet are summarized in Table I. The two layer coils are made with a Rutherford-type cable composed of 40 strands of 0.85 mm diameter. The cable incorporates a 12-mm-wide stainless steel core of 25 μm thickness to reduce inter-strand coupling

TABLE I
MAIN DIMENSIONAL PARAMETERS FOR MQXFS1

Parameter	Unit	
Cable bare width (before/after HT)	mm	18.150/18.513
Cable bare mid-thick. (before/after HT)	mm	1.525/1.594
Keystone angle	Deg.	0.55
Cable pitch length	mm	109
Cable core width	mm	12
Cable core thickness	μm	25
Cable insulation thickness per side at 5 MPa	μm	150±5
Coil clear aperture diameter	mm	150
No. turns in layer 1/2 (octant)	--	22/28
Magnet (LHe vessel) outer diameter	mm	630
Magnetic length	mm	1194
Overall coil length	mm	1510
Magnetic yoke length	mm	1550

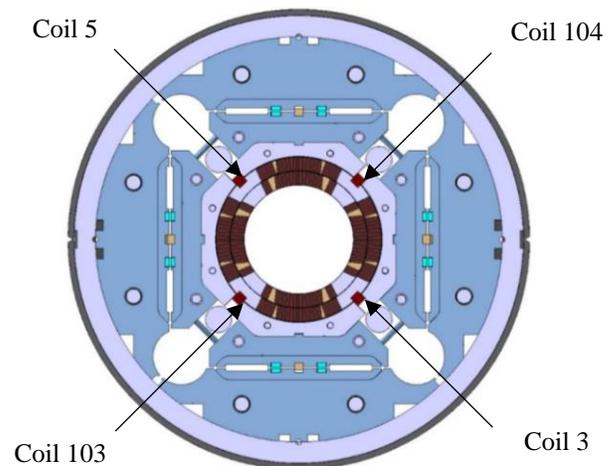


Fig. 1. Magnet cross section viewed from the lead end, including the position of each coil in the magnet assembly.

currents. The operational gradient in nominal conditions is 132.6 T/m with a peak field in the conductor of 11.4 T and a current of 16.48 kA, with an operating temperature of 1.9 K. The physical length of the coil is 1510 mm, corresponding to a magnetic length of about 1.2 m and a good field quality region of 500 mm [6]. The coils are assembled inside a support structure based on an external aluminum shell pre-loaded with bladders and keys [7].

Automatically generated dates of receipt and acceptance will be placed here; Work supported by the USA-DoE and by the High Luminosity LHC project at CERN.

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III. MAGNETIC MEASUREMENTS

The magnetic measurements were performed with a rotating probe based on printed-circuit board (PCB) technology developed by FNAL [8]. For the warm measurements during assembly in LBNL, two coils of 59.5 mm radius, one 110 mm and the other 220 mm long were installed in the magnet bore and supported by a temporary tube. For the cold measurements at FNAL, 50.5 mm radius probes were centered using a new anti-cryostat. During the first thermal cycle, a 30-layer PCB probe was used, requiring the use of an attenuator due to the saturation of the amplifier. For the second thermal cycle, the 30-layer PCB was replaced by a 2-layer probe with no attenuator, mounting two circuits of 50 mm and 100 mm length in the same probe. The data reported here correspond to the measurements taken during the second thermal cycle. The resolution of the probe for cold measurements is on the order of 0.03 units at a radius of 50 mm. For warm measurements, the resolution of the probe is 0.003 units [9].

The field quality in the aperture is described in a standard form of harmonics coefficients defined in a series expansion,

$$B_y + iB_x = B_2 \cdot 10^{-4} \sum (b_n + ia_n) \left(\frac{x + iy}{R_{ref}} \right)^{n-1} \quad (1)$$

where B_x and B_y are the field components in Cartesian coordinates, B_2 is the reference field), and b_n and a_n are the normalized harmonics coefficients at the references radius $R_{ref} = 50$ mm. The right handed measurement coordinate system is defined with the z -axis at the center of the magnet aperture and pointing from the return end to the lead end. Fig. 1 shows the position of each coil in the magnet assembly viewed from the lead-end.

IV. RESULTS AND ANALYSIS

A. Transfer function and Iron Saturation effect

Fig. 2 shows the measured gradient divided by the current during a cycle close to the standard LHC machine operation cycle in a central segment of the magnet. The pre-cycle reaches a flattop current of 16.48 kA at 14 A/s with a flattop current duration of 300 s. The current is ramped down with 14 A/s to 100 A and then it immediately ramps up to the injection plateau at 960 A with 14 A/s. The duration of the injection plateau is 1000 s, followed by the particle acceleration phase using a parabolic ramp. Then it is ramped linearly at 14 A/s up, followed by a deceleration parabola used to reach the nominal current smoothly and to avoid overshoots.

The transfer function decreases by $\sim 9\%$ from injection level to nominal due to the iron saturation effect, which is in very good agreement with ROXIE model. Assuming a radial contraction of the coil during cool down of 3 mm/m, we find that measurements give a 30 units larger transfer function. If the coil deformation as computed using ANSYS is introduced in ROXIE, the measured transfer function is 15 units stronger than expected. The same level of discrepancy was found during the warm magnetic measurements, which would correspond to an inner bore diameter 0.5 mm smaller than nominal. The longitudinal variation of the main field is within 10 units in the straight magnet section.

TABLE II
AVERAGE FIELD HARMONICS IN THE STRAIGHT SECTION.

n	Before Loading (RT)		After Loading (RT)		I = 16.48 kA (1.9 K)		After Cold Test (RT)	
	b_n	a_n	b_n	a_n	b_n	a_n	b_n	a_n
3	-3.02	3.03	-3.24	3.46	-4.39	3.13	-3.89	3.26
4	0.56	-3.86	0.30	-4.18	0.14	-6.9	0.30	-4.72
5	2.68	-0.68	2.47	-0.55	2.75	-0.97	2.57	-0.55
6	2.10	0.49	3.57	0.65	0.68	0.44	4.18	0.50
7	0.14	0.23	0.13	0.27	0.19	0.26	0.24	0.10
8	0.19	-0.24	0.23	-0.25	0.24	-0.67	0.19	-0.16
9	0.17	0.28	0.15	0.31	0.22	0.31	0.05	0.23
10	-0.53	0.12	-0.49	0.12	-0.46	0.15	-0.39	0.13
11	0.04	-0.07	0.03	-0.08	0.04	-0.10	0.04	-0.05
12	-0.04	0.08	-0.04	0.09	-0.03	0.06	-0.05	0.11
13	0.02	0.03	0.03	0.03	0.03	0.05	0.02	0.01
14	-0.60	-0.02	-0.61	-0.03	-0.70	0.02	-0.55	0.03

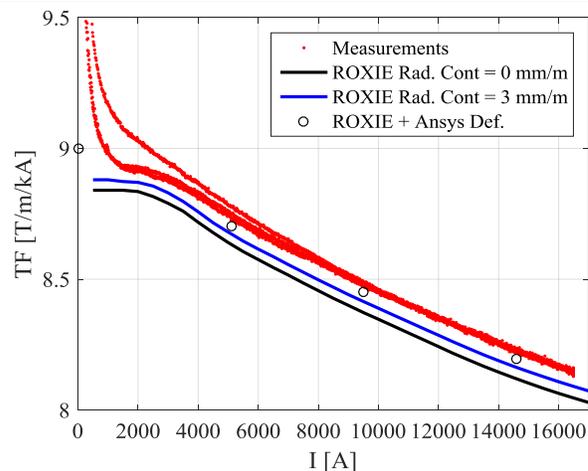


Fig. 2. Current dependence of the transfer function measured during a machine cycle to nominal current compared to ROXIE model assuming no coil deformation during cool down, a radial contraction of 3 mm/m and the coil deformation as computed with ANSYS.

B. Geometric Field Errors

Due to the large beam size and orbit displacements in the final focusing triplet, MQXF have challenging targets for field quality requirements at nominal operation current. The measured geometric field errors, averaged in the magnet straight section are summarized in Table II. The main findings are:

- There is a high degree of cold-warm correlation, and there is not a visible permanent deformation in the coil during powering as the harmonics after cold powering test are not altered.
- At nominal operation current, the allowed harmonics are in very good agreement with ROXIE model, which predicts a $b_6/b_{10}/b_{14}$ of 0.68/-0.39/-0.66 units versus the measured $b_6/b_{10}/b_{14}$ of 0.68/-0.46/-0.70 units.
- Normal and skew sextupole components show a large systematic effect of several units and changes of the same order along the magnet length. The measured average b_3 and a_3 (~ 3 -4 units) can be corrected through the insertion of magnetic shims in four out of the eight bladder slots [10]. Due to the good cold-warm correlation during production such geometrical defects are possible to detect and compensate before the final assembly.

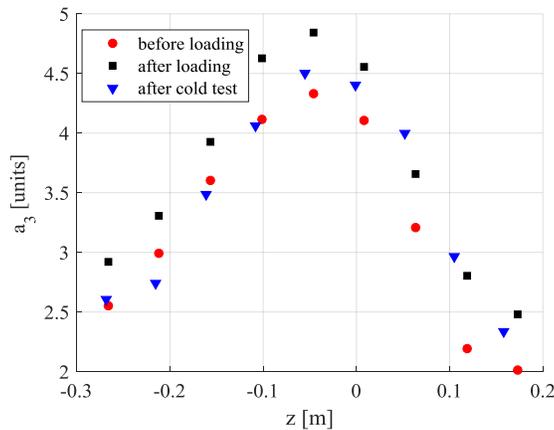


Fig. 3. Evolution of the skew normal component along the magnet axis measured at room temperature before loading, after loading and after cold test. $z=0$ correspond to the magnetic center of the magnet.

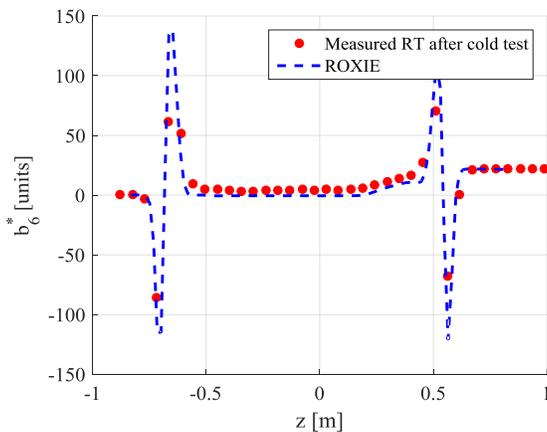


Fig. 4. Measured and calculated profile of the pseudo-harmonic b_6^* along the magnet axis measured at room temperature after cold powering test. $z=0$ correspond to the magnetic axis of the magnet.

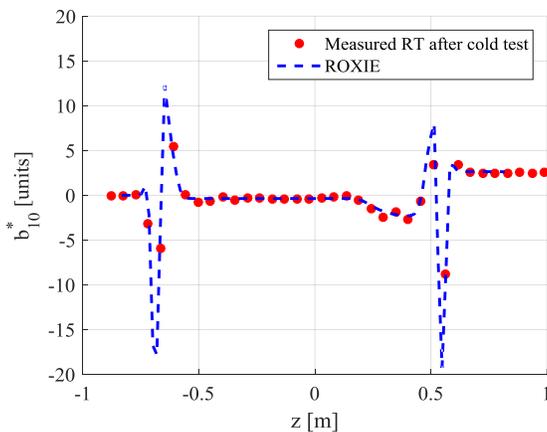


Fig. 5. Measured and calculated profile of the pseudo-harmonic b_{10}^* along the magnet axis measured at room temperature after cold powering test. $z=0$ correspond to the magnetic axis of the magnet.

- About -5 units of a_4 and 0 units of b_4 are expected due to the systematic difference in terms of coils size between LARP and CERN coils (LARP coils were larger than nominal by about 0.050 mm, whereas CERN coils were smaller by about 0.050 mm [4]). Measurements are close to expectations, with 0.3 units of b_4 and -6.8 units of a_4 .

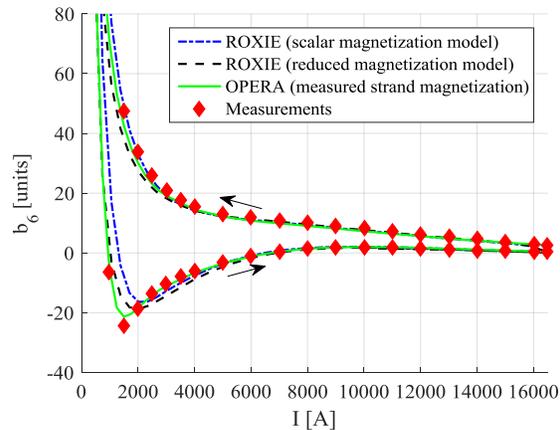


Fig. 6. Measured and calculated b_6 field component as a function of the magnet current. Calculations are shifted by 0.7 units to suppress for the geometric component.

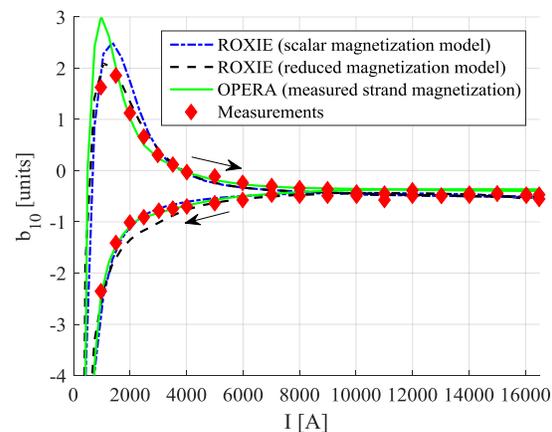


Fig. 7. Measured and calculated b_{10} field component as a function of the magnet current. Calculations are shifted by 0.1 units to suppress the geometric component

The lower degree of cold-warm correlation on a_4 could be linked to the use of a different conductor in LARP and CERN coils, introducing an up-down asymmetry that will be discussed in section C.

- Further investigation is needed to understand the source of the ~ 2.5 units of b_5 .

As it can be observed in Fig. 3, the overall strength and longitudinal structure of the harmonics is not fundamentally altered from the initial assembly before loading to powering, showing that the dominant source of field errors is the coil geometry and its initial assembly in the collared coil. Only the skew sextupole component is shown, but similar effect is observed on b_3 [9]. The spread of the field harmonics along the magnet axis corresponds to a precision of the coil positioning along the magnet axis of 0.050 mm. Fig. 4 and 5 show the measured and calculated profile of the pseudo-harmonics b_6^* and b_{10}^* , using the convention defined in [6]. The contribution of the coil ends is well captured by the ROXIE 3D model.

C. Strand Magnetization Effect

Due to the larger filament size and higher current density, strand magnetization effects are about a factor ten larger than in the LHC-MB dipoles. Fig. 7 and 8 show the persistent current

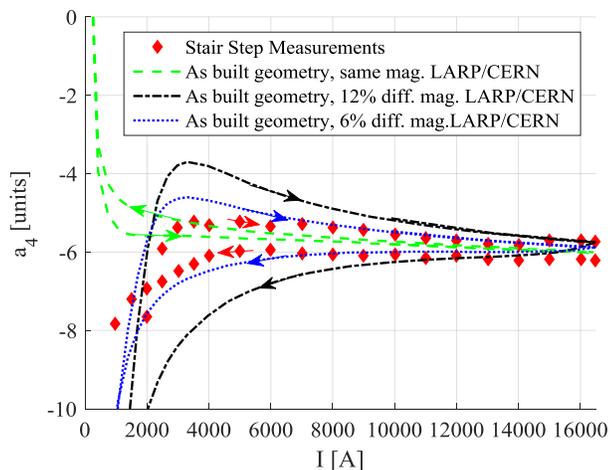


Fig. 8. Measured and calculated a_4 field component as a function of the magnet current.

effects in the first allowed multipoles b_6 and b_{10} measured during the stair step cycle. Measurements are compared to computed values using three methods: i) the semi-analytical scalar hysteresis model for strand magnetization implemented in ROXIE [11]; ii) a modified version of the scalar model, where a 50 % linear reduction of the magnetization for field levels below 2 T is assumed to account for the impact of flux jumps on strand magnetization [12]; iii) a finite element model implemented in OPERA based the on strand magnetization measurements [13]. Measured and computed values are generally in good agreement.

Due to the systematic differences in coil size among CERN and LARP coils and the use of a different stack of superconductor (108/127 for LARP coils and 132/169 for CERN coils), an impact on a_4 is expected. Fig. 8 shows that the hysteresis loop can be foreseen when the difference between strand magnetization for CERN and LARP coils is taken into account. According to ROXIE model, a 6 % difference between strand magnetization for LARP and CERN coils allows to reproduce the measured harmonics.

D. Inter-Strand Coupling Currents Effect

To study the dynamic field errors, after a standard pre-cycle, the current was cycled from injection to nominal at 20 A/s, 40 A/s and 80 A/s with no cleansing quench in between. The ramp rate effect on normal and skew multipoles is summarized in Table III, reporting the difference on the width of the hysteresis loop at 40 A/s and 80 A/s with respect to the 20 A/s cycle for a magnet current of 8 kA and 16 kA. MQXF cable has a stainless steel core which covers 70 % of the available cable width, so as expected, the effect of the ramp rate on the allowed harmonics is small. However, some non-allowed components (a_3 , a_4 , a_7 and a_8) show larger ramp rate dependence. They are a factor 10 times smaller than seen in HQ01 [14] (un-cored cable), a factor 5 times smaller than in HQ02 [15] (core coverage 60 %) and a factor 2 times larger than in the CERN 11 T [16] (core coverage 90 %). When ramping stops during the stair step measurements, multipole decay of the non-allowed harmonics with a stronger dependence on the ramp rate is observed at each measurement level. These effects, also

TABLE III
IMPACT OF THE RAMP RATE ON THE WIDTH OF THE HYSTERESIS LOOP. DIFFERENCE ON THE NORMAL AND SKEW MULTIPOLES WITH RESPECT TO THE 20 A/S CYCLE.

n	RR = 40 A/s				RR = 80 A/s			
	I = 8 kA		I = 16 kA		I = 8 kA		I = 16 kA	
	Δb_n	Δa_n						
3	-0.02	0.80	-0.03	0.27	-0.03	2.00	0.05	0.69
4	-0.03	0.61	-0.01	0.22	0.07	1.87	0.00	0.67
5	0.06	-0.14	0.05	0.03	0.27	-0.01	0.03	0.02
6	-0.31	0.09	-0.02	0.03	-1.12	0.12	-0.29	0.04
7	0.05	0.24	0.00	0.08	-0.05	0.75	0.01	0.27
8	-0.01	0.24	0.04	0.09	0.01	0.66	0.05	0.18
9	0.03	-0.01	0.01	0.00	0.08	0.11	0.05	0.04
10	-0.02	0.03	-0.03	0.01	-0.09	0.05	-0.01	0.01

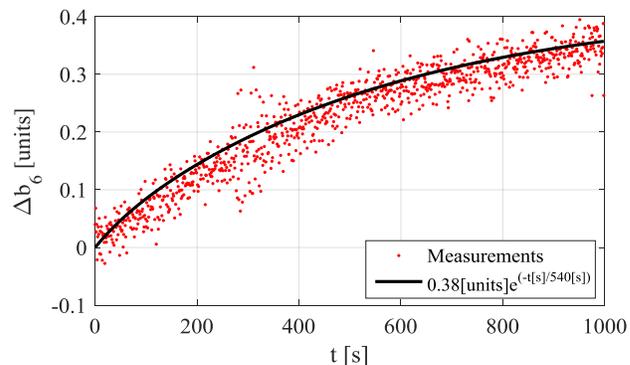


Fig. 9. Decay in the dodecapole field component at injection in MQXFS1a during the accelerator cycle. Measurements in a 100 mm length segment in the center of the magnet.

observed at high current, decay relatively quickly and can be described with a single time constant for a resistive decay process, with a time constant of about 2-4 s. These effects are negligible for magnet operation.

E. Multipole decay

Fig. 9 shows the measured decay of the dodecapole. The amplitude of the decay is 0.4 units, which is very close in amplitude and direction to the decay observed in HQ02 and HQ03 models [17] and comparable to the decay observed in Nb-Ti magnets [18]. The data can be fitted using a single exponential with a time constant of 540 s.

V. CONCLUSION

The first MQXF 1.5 m model has been successfully tested at the Fermilab Vertical Test Facility. The iron saturation effect and allowed harmonics are in very good agreement with ROXIE model. A geometric offset of 15 units on the transfer function is found both at warm and cold, which would correspond to an inner bore diameter 0.5 mm smaller than nominal. The large measured a_4 is expected due to the systematic differences between CERN and LARP coils but further investigations are needed to understand the source of b_5 . The overall strength of the harmonics is not fundamentally altered from the initial coil pack assembly to powering. Thanks to the use of a stainless steel core, the ramp rate dependent effects are negligible.

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