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A SMALL DRIFT SCAN SURVEY FOR GALAXIES IN THE NORTHERN SKY¹⁾

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ABSTRACT

CCD photometry has been obtained for 1054 galaxies to a limiting magnitude $r_W = 18.0$ in a narrow strip of the sky $12'$ wide by 60° long. The data are being used to calibrate photographic photometry as part of a parallel redshift survey, but can also be used to study the projected distribution of galaxies on large angular scales free from systematic effects that are present in photographic surveys. Fluctuations in the number density of order 20% are seen on angular scales of 5° and apparently correlate with the distribution of Abell Clusters that lie within 2° of the strip.

1. INTRODUCTION

The Century Survey (Geller *et al.* 1991) is a project to measure redshifts for approximately 2000 galaxies in a strip 1° wide by 100° long to a limiting magnitude $R_K = 16.4$ (where R_K is on the Kron-Cousins system). The strip is centered at $\delta = 29.5^\circ$ and extends from $8^h 30^m$ to $16^h 45^m$ (epoch 1950). The purpose is to study the large scale distribution of galaxies in a two-dimensional slice in a manner analogous to that of de Lapparent, Geller, and Huchra (1986) but to approximately twice the distance. Galaxies are selected by scanning the Palomar Sky Survey E plates. The survey is currently in progress.

A key problem with this and any other galaxy surveys derived from photographic plates is getting an accurate magnitude calibration. Typically one obtains CCD photometry of several galaxies per plate to establish a zero-point. Since the internal

r.m.s. error of photographic galaxy photometry is of order 15%, a dozen or more galaxies are needed. Still more are needed if it is desired to calibrate sensitivity and vignetting variations across a plate or nonlinearities in the magnitude scale. The Century Survey spans 14 Palomar Sky Survey plates, so about 200 objects would be needed for a proper calibration. The most efficient way to obtain the requisite data is with a CCD operating in drift-scan (TDI) mode.

This paper reports the results of a small CCD drift scan survey that passes down the center of the Century Survey strip. The purpose of the survey is two-fold. One is to provide an accurate calibration of the Century Survey photographic data. The other is to examine the fluctuations in galaxy density on angular scales of tens of degrees. The portion of the survey presented here covers a region 12' in width (or 1/5 the width of the complete Century Survey strip) by 60° long. It is complete to a limiting magnitude of approximately $r_W = 18$ (and extends 1/2 mag fainter). Ultimately the survey will cover the entire length of the Century Survey strip. Since the remaining portion will use a different telescope and detector combination, it is appropriate to present the results of the first part separately here.

Studies of just the angular distribution of galaxies (without redshifts) also provide information on the clustering properties of galaxies. Heretofore virtually all studies of the angular distribution of galaxies on large scales have been done photographically (*e.g.*, Groth and Peebles 1977; Collins *et al.* 1988; Maddox *et al.* 1990). The two-point angular correlation function has now been measured several times on angular scales between 0.1° and 10°. All studies are in agreement that on small scales the correlation function is a power law with slope of ≈ -0.7 and that the correlation function shows a break on larger scales, but the position of this break and the angular correlation function on scales greater than about 10° to 20° are poorly known. Studies of the large scale angular galaxy distribution require that one calibrate photographic plate zero-points consistently to an accuracy of a few percent. Ideally one would like have accurate independent calibrations of each plate, but more commonly such calibrations are done by using plate overlap regions to adjust the zero-points of adjacent plates to a common value. Consequently any measurements of the fluctuation in galaxy density on the scale of plate-to-plate separations are suspect. CCD drift-scan data provide an alternative way to study the angular distribution of galaxies in a way that avoids the problems of photographic material.

2. OBSERVATIONS

The observations were carried out on the night of May 23, 1990. A Ford Aerospace 2048 × 2048 front-side illuminated CCD was used on the 61 cm telescope of the Whipple Observatory, located on Mt. Hopkins, AZ. The CCD was operated with on-chip binning, giving an effective format of 1024 × 1024 pixels with a scale of 0.72" per pixel. In drift scan mode, the CCD columns are aligned in the east-west direction. The telescope tracking is stopped, and the CCD is clocked at the sidereal rate in synchronism with a star image as it trails across the CCD. The

CCD is read out continuously, building up an image of a strip of the sky. At a declination of 29.5° , the effective integration time for each pixel on the sky was 57 seconds.

The telescope focal ratio is quite slow, $f/13$, so in order to get the highest signal/noise ratio possible, the observations were made through a wide "W" filter that transmits $4000 - 9000\text{\AA}$. Observations of Thuan & Gunn (1976) standard stars were used to calibrate the data. Although the W filter matches no standard bandpass, the effective wavelength for objects that have the color of galaxies closely matches that of the Thuan & Gunn (1976) r filter, and all magnitudes will be reduced to that system. It should be recognized that the photometry is not true r band photometry, and to indicate that fact we will label all magnitudes as r_W . This is not crucial, however, because the purpose of the survey is more to maintain uniformity across the sky than to reach a well-known, absolute zero-point. For reference $R_K \approx r - 0.4$.

Due to the need to refocus periodically, the strip was broken into several overlapping segments. A computer crash caused the loss of data in the range $15^h45^m < \alpha < 16^h17^m$. Thus the data actually cover two contiguous strips, $11^h50^m < \alpha < 15^h45^m$ and $16^h17^m < \alpha < 16^h45^m$, which have angular extents of 51.0° and 6.4° respectively.

To check the reliability of our data, repeat observations in both pointed and drift scan mode were obtained in 1991 May and 1992 February using a different CCD and a 1.2 m telescope (that has now replaced the 0.61 m telescope). The new drift scans overlap the old in the regions of 11^h45^m and 16^h20^m for a total of about 15^m . Pointed observations were made of several fields spaced uniformly along the extent of the strip.

For reference the survey passed over 6 NGC galaxies, the centers of 2 Abell clusters (A1495 and A1878), and several fields with known radio galaxies, BL Lac objects, QSO's, etc. for which fragmentary bits of data have been published.

3. DATA REDUCTION AND ANALYSIS

Initial data processing followed standard methods with a couple of variations. Bias frames were replaced with "drift dark" frames where the CCD is operated in drift scan mode with the shutter closed. Flatfields were generated by forming a median average of data frames. Frames were combined typically in groups of 15. The CCD had no bad columns. The only cosmetic corrections made to the data were for occasional rows dropped by the computer and for some frames with shifted rows caused by loss of readout synchronization.

Astrometry was accomplished by using stars with known positions from the Guide Star Catalog (Lasker *et al.* 1990). All stars in a single segment of frames were used to determine the scale factors in right ascension and declination. The rms residuals in the fits were $0.5''$ in right ascension and $0.9''$ in declination. The larger error in declination was caused by a charge transfer problem that will be discussed

next. The residuals in right ascension were correlated with right ascension in a fashion that reflects the boundaries of the plates that were used to construct the Guide Star Catalog catalog. Because each segment of CCD images covered more than one plate typically, these systematic errors in the guide star catalog ought to be partially removed. To be conservative, we will assume that the rms errors in the standard star fits apply to the galaxy positions as well.

The analysis was complicated greatly by a charge transfer problem discovered only after the CCD was installed at the telescope. This problem caused star images to be smeared into cometary shapes reminiscent of comatic aberration. Furthermore, the amount of smearing increased linearly with column number across the CCD. Figure 1 shows isophotal plots of two stars from different column positions on the CCD, illustrating the nature of the problem. This problem affected both the photometry and the star/galaxy separation. Several steps were taken to ameliorate the damage.

In spite of the charge smearing, the photometric quality of the data was still preserved. This was checked in two ways. First, the galaxy NGC 4278 fell in the strip, and surface photometry was compared with published R-band photometry of Peletier *et al.* (1990). No significant differences were found over a surface brightness range $17 < \mu_r < 23$ mag arcsec⁻². Second, the pointed observations obtained in 1991 and 1992 were used to randomly check the photometry of stars in several fields spaced along the strip. No significant problems were found as a function of magnitude or position on the CCD at the level of 0.05 mag.

Because of the variable charge smearing, traditional star/galaxy separation routines could not be used. However, we found that the FWHM of star profiles taken in the east-west direction (perpendicular to the smearing) were nearly constant everywhere on the CCD (Fig. 2). Consequently, we classified stars and galaxies solely on the basis of single-cut profile widths. This procedure worked reasonably well, although it failed to identify edge-on galaxies oriented north-south. The critical width separating stars and galaxies was set high so that we erred in the direction of missing compact galaxies rather than including stars erroneously. This is necessary to avoid any artifacts in the galaxy counts due to variations in star density with Galactic latitude. We still found it necessary to visually inspect all frames and throw out objects erroneously classified as galaxies arising from close pairs of stars, smearing from saturated images of bright stars, and uncorrected artifacts in the data. We estimate that our star/galaxy separation is reliable to $r_W = 18.0$. We have actually classified galaxies to a limit $r_W = 18.5$ (and then cut the list at 18.0 after the fact), although we are certainly incomplete at the fainter limit. We were able to check the reliability of our classifications by comparing them with the images from 1991 that had a much higher quality. Brighter than our completeness limit $r_W = 18.0$, we identified 40 galaxies in the 1990 survey; the 1991 data showed only 1 to be in error, and additionally 1 compact galaxy was missed. Fainter than our completeness limit, we identified 24 galaxies. Again, only 1 was in error, but 9

were missed. Hence the 18.0 mag limit for completeness appears to be reasonable.

Another measure of incompleteness due to the charge smearing problem is to compare the galaxy counts in the lower and upper halves of the CCD. Indeed, among the galaxies brighter than 18.0 we find more galaxies in the lower than the upper half by the ratio 569/479. The difference of 90 galaxies is considerably larger than the rms difference of 33 that one would expect for Poisson fluctuations. However, following an analysis given in the Appendix, we find that the expected rms difference in counts between the two half-strips is actually dominated by large scale structure in the galaxy distribution and not Poisson fluctuations; the expected rms difference in counts is in fact 50. Hence this test is not conclusive in showing whether or not incompleteness is a problem. Again, repeat images of the survey with the 1.2 meter telescope show no pattern of missing galaxies anywhere.

Finally, we need to estimate the fraction of galaxies lost to overlapping stars and/or other galaxies. Ideally, we would add artificial galaxies randomly to real images and determine the detection efficiency, but given the need to deal with a variable point-spread function, this would be a laborious procedure. Instead, we simply smoothed each image and computed the fractional area that had an intensity 10% or more above the sky background. Excluding those frames with very bright stars, this area ranges from 1% to 2%, depending primarily on galactic latitude. We conservatively estimate that any galaxy with a center within 3 pixels of such bright pixels is likely to be missed. The total fractional area so excluded is found to range from 4% to 7%. Given the tentative nature of this calculation, the number densities derived below will not be corrected for this incompleteness. However, the variation in incompleteness across the survey is expected to be only a few percent and will turn out to be unimportant.

As a practical convenience the raw data were divided into square frames and then reduced frame-by-frame. A constant sky value was derived for each frame and used in computing object magnitudes. This procedure is not technically correct because the sky intensity varies continuously throughout the strip. However, the frame-to-frame variations in sky intensity show that the variation within a single frame is negligible.

Object magnitudes were computed iteratively. Given a preliminary estimate of an object's magnitude, an aperture was chosen such that the mean surface inside is approximately $23.5 \text{ mag arcsec}^{-2}$. For all except the very lowest surface brightness galaxies, we estimate that this aperture will include at least 98% of the total galaxy light. The one exception to this choice of aperture was that the minimum aperture allowed was $7.2''$ in radius. The uncertainties in galaxy magnitude due to statistical noise were 15% at $r_w = 18.5$ and less at brighter magnitudes. Charge smearing causes some light to be missed. This was rectified by applying aperture corrections measured from several bright stars at different positions on the CCD. In all cases the aperture size is sufficiently large that the galaxies are essentially point sources as far as the aperture corrections are concerned. The largest correction was 0.15

mag. Figure 3 shows the corrections as a function aperture size for two y positions that span the CCD.

Because the survey region was scanned in several short, overlapping strips, a number of objects in the overlap regions were observed twice. Figure 4 shows the magnitude difference for all objects observed twice as a function of magnitude. The magnitudes of bright objects are quite repeatable, while the error increases rapidly fainter than $r_W = 17$. However, even at $r_W = 18$, the rms error is still only 0.06 mag. This error refers only to the repeatability of magnitudes measured in fixed apertures; the galaxy magnitudes will be somewhat worse due to the need to adjust the aperture size as a function of magnitude as well. A comparison of the galaxy magnitudes with those from the 1991 data shows an rms difference of 0.12 mag. We consider this to be a more realistic estimate of the true error at the survey limit.

Although the night was photometric to the eye, small variations in atmospheric transparency could not be ruled out. Therefore, as a final check on the magnitude zero-point, four fields spaced evenly along the survey were reobserved in rapid succession during May 1991. Aside from a small zero-point difference between the 1990 and 1991 observations (likely due to a change in the filter being used), the peak deviation among the four fields was only 0.02 mag. Hence we feel confident that the magnitude zero point is indeed uniform along the entire length of the strip.

The final list of galaxies is given in Table I. We include only objects with total magnitudes brighter than 18.0. A colon after a magnitude indicates that it may be uncertain due to the presence of a second object in or near the aperture.

4. DISCUSSION

The total survey (to $r_W = 18.5$) contains 1495 galaxies, and at the completeness limit of $r_W = 18.0$, there are 1054 galaxies. In the 51° contiguous region these numbers are 1392 and 978 respectively. The total area covered by the survey is 11.5 deg^2 . The mean density of galaxies at our completeness limit of $r_W = 18$ is 92 gal deg^{-2} ; at $r_W = 18.5$, the measured density is 130 gal deg^{-2} , but this figure is certainly low because of incompleteness. The first density can be compared with other galaxy surveys: the Zwicky (1961) catalog has as mean density of 3; the Lick Survey (Shane & Wirtanen 1967) reaches to a density of 54; the Edinburgh/COSMOS survey (Collins *et al.* 1988) goes to 279 and 449 in two different areas; and the Oxford/APM survey (Maddox *et al.* 1990) goes to 465.

The data of de Lapparent *et al.* (1986) show that the Zwicky Catalog detects galaxy clusters to a characteristic redshift of about $z = 0.03$. Since our survey goes approximately 3 times deeper, we should be sensitive to clusters out to a redshift of $z \approx 0.1$.

With only 1054 galaxies in the complete survey and 978 in the largest contiguous strip, the two-point angular correlation function cannot be measured to very high accuracy. Still, in Fig. 5 we show the two-point correlation function for those

galaxies that lie in the 51° contiguous portion of our strip. The function was computed using the method outlined by Peebles (1980): we count the number pairs of galaxies with a given separation and divide by the number of pairs that one would get for a perfectly random distribution. The latter number was determined by a series of Monte Carlo simulations. The error bars show in Fig. 5 measure the scatter in the determination of the correlation function as derived from the simulations. The simulations also allow us to estimate the effects of observational selection biases on the measured correlation function. In particular, we find that the suspected bottom/top asymmetry in finding galaxies on the CCD as discussed in §3 is quite negligible.

Also shown in Fig. 5 is the power-law portion of the correlation function derived by Groth and Peebles (1977) based on the Lick Survey and scaled to our depth. We find virtually the same slope (≈ 0.7) for scales $\theta < 1^\circ$ albeit with lower amplitude. We are unable to measure the location of any break in the correlation function on larger scales as was claimed to exist by Groth and Peebles.

Probably the most interesting result of our survey is the variation in number density in the contiguous 51° strip across the sky. It is on these scales that photographic surveys are the most unsure. What problems we had with the data are not expected to correlate with right ascension, so the variations we measure should be real. Figure 6 shows the galaxy density binned by every 5.1° in right ascension. The mean number of galaxies per bin is 98. Two features can be gleaned from the figure: first, there is no large scale gradient in the galaxy density, and second, the bin-to-bin fluctuations are much larger than expected from Poisson statistics. The former is reassuring; the latter is not unexpected, and it reflects the fact that galaxy positions are correlated. In fact, the expected rms can be estimated using the angular two-point correlation function $w(\theta)$. In the Appendix we show that the variance in the number of galaxies in randomly placed bins is $\sigma^2 = N[1 + N\langle w \rangle]$, where N is the mean number of galaxies per bin, and $\langle w \rangle$ is the correlation function averaged over the interior of a bin. To determine the mean of w , use the Lick correlation function $w(\theta) = .0684/\theta^{0.73}$ (Groth & Peebles 1977) and scale to our depth by assuming that we reach a factor 1.19 greater in distance: this scaled function is $w(\theta) = .051/\theta^{0.73}$. We have calculated σ under two different assumptions: first, that the power-law correlation function is valid to very large angular scales, and second, that the power-law is cut off at a finite radius (2.5° for the Lick survey or 2.1° for our CCD survey). For the two cases, we predict that $\sigma = 31$ and 21 respectively. The observed rms is 20 galaxies per bin, with an uncertainty of 5 if the bins are uncorrelated. The accuracy is not quite sufficient to distinguish between the two cases (although being in the direction of favoring a cutoff), but the rms is over twice that predicted by Poisson statistics. We can also estimate the contribution of uncertainties in limiting magnitude and foreground dust extinction to the fluctuations. Fluctuations in the limiting magnitude are apparently 0.02 mag at most and hence can be ignored. Also, from the *IRAS* map of high-latitude cirrus (Boulanger and Perault 1988), we estimate that the peak extinction over the survey is less

than $A_V = 0.14$ mag. This corresponds to a peak-to-peak fluctuation in number counts of about 17% or approximately 5% rms. Hence neither contribution should be making a significant contribution to the observed galaxy count rms fluctuations.

It is also of interest to match Fig. 6 to the distribution of Abell clusters near the Century Survey strip. The survey is expected to be able to detect Abell clusters reaching out to distance classes 4 or 5. Figure 6 overlays the galaxy counts with a plot of the number of Abell clusters with distance classes 1 to 5 that lie within 2° of the strip. A fair degree of correlation appears to be present. Using Spearman's rank-order correlation test (Press *et al.* 1986), we find that the two distributions are correlated at the 90% confidence level, suggestive although not overwhelming. In contrast, Fig. 7 makes the same comparison with D=6 clusters; here, no correlation is seen, indicating that these clusters are too distant to influence the survey counts.

The significance of the correlation in Fig. 6 is somewhat subtle: only 2 Abell clusters actually have centers that lie in the strip, and they contribute only 2 galaxies total. Hence what we are seeing are fluctuations due to an enhancement in the density of galaxies in the neighborhood of clusters rather than the individual clusters directly. The enhanced density in the zone $15^h < \alpha < 16^h$, for example, may be caused by the Coronal Borealis supercluster (Postman *et al.* 1988). Galaxy redshifts, once available, will undoubtedly reveal the clustering properties more clearly.

It is interesting to note that because the bin-to-bin fluctuations are dominated by large scale structure rather than Poisson statistics, we would not have measured the rms fluctuations any better if we had simply, say, doubled the width of the survey. Rather, to do better, we would have to survey an independent portion of the sky. In fact, with a dozen or so CCD drift scan swaths, we could extract virtually as much information on the very large scale angular correlation function as one could derive from a filled photographic survey.

Our results can also be compared with those of Picard (1991). Using photographic plates, Picard measured the galaxy density for two fields separated by about 128° . Each field was approximately 15° on a side, and the total area surveyed was 386 deg^2 . His survey reached to a limiting magnitude $r = 19.0$ and recorded a density of 400 gal deg^{-2} . He found a difference of 30% in number density between the two fields. Our survey provides only ≈ 3 independent samples on the scale of 15° , but we estimate that the rms fluctuations on this scale are only of order 12% or so to our shallower limiting magnitude; these fluctuations should be reduced further by a factor 2 or so in the deeper survey of Picard. Consequently, we would expect to find a much smaller variation between the two fields than he actually does. However, since our survey spans only half the angular scale of his, we could easily miss a large scale gradient in the galaxy density on that scale. Further observations would settle the issue.

5. CONCLUSIONS

We have conducted a drift-scan CCD survey over a 60° swath of sky (51° con-

tiguous) and found 1495 galaxies total to $r_W = 18.5$ (1054 to $r_W = 18.0$ in a complete sample) in an area of 11.5 deg^2 . The data are being used to calibrate a larger photographic survey (to be presented in a future paper) but also form a deeper galaxy survey in their own right. The principal result is that fluctuations in galaxy counts on the scale of 5° and greater can be measured and may be correlated with fluctuations in the number density of Abell clusters.

The present CCD survey covers a little more than half the range in right ascension of the full Century Survey. Data have now been obtained for the remaining right ascension range using a new 1.2 meter telescope and a Ford CCD with much better performance. Those data also will be presented in a future paper.

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APPENDIX

Here we give a more detailed derivation of the bin-to-bin galaxy count fluctuation computation, following Peebles (1980). We assume that a bin has width W and length L with $W \ll L$. For simplicity, we will perform only a 1-dimensional calculation. We let $w(\theta)$ be the two-point correlation function and λ be the (constant) mean density of galaxies per unit angle along the bin.

Break the bin up into K cells such that there are 0 or 1 galaxies per cell. Let $\epsilon = L/K$ be the size of one such cell. Let n_i be the number of galaxies in cell i . Then n_i is a discrete random variable with a probability distribution function $P(n_i)$ given by $P(0) = 1 - \lambda\epsilon$ and $P(1) = \lambda\epsilon$. The first and second moments are given by $\langle n_i \rangle = \lambda\epsilon$ and $\langle n_i^2 \rangle = \lambda\epsilon$ respectively. Given 2 cells separated by θ_{12} with densities n_1 and n_2 , the correlation function $w(\theta_{12}) = w(|\theta_1 - \theta_2|)$ is defined so that $\langle n_1 n_2 \rangle = \langle n_1 \rangle \langle n_2 \rangle [1 + w(\theta_{12})]$.

The total number of objects in a bin is

$$N = \sum n_i,$$

and the second moment is

$$N^2 = \sum n_i^2 + \sum_{i \neq j} n_i n_j.$$

Then

$$\begin{aligned} \langle N \rangle &= K \lambda \epsilon = \lambda L, \\ \langle N^2 \rangle &= K \lambda \epsilon + K^2 \lambda^2 \epsilon^2 [1 + \langle w \rangle] \\ &= \langle N \rangle + \langle N \rangle^2 [1 + \langle w \rangle] \end{aligned}$$

where

$$\begin{aligned}\langle w \rangle &= \frac{1}{L^2} \int_0^L d\theta \int_0^L w(|\theta - \theta'|) d\theta' \\ &= \frac{2}{L^2} \int_0^L d\theta \int_0^\theta w(\theta - \theta') d\theta'.\end{aligned}$$

Let $\theta' = \theta \sin \phi$. Then

$$\langle w \rangle = \frac{2}{L^2} \int_0^L \theta d\theta \int_0^{\pi/2} w[\theta(1 - \sin \phi)] \cos \phi d\phi.$$

The variance is

$$\sigma^2 = \langle N^2 \rangle - \langle N \rangle^2 = \langle N \rangle [1 + \langle N \rangle \langle w \rangle]. \quad (A1)$$

We take

$$\begin{aligned}w(\theta) &= \frac{A}{\theta^\alpha}, & \theta < \theta_c \\ w(\theta) &= 0, & \theta > \theta_c\end{aligned}$$

Then

$$\begin{aligned}\langle w \rangle &= \frac{2A}{L^2} \int_0^{\theta_c} \frac{\theta d\theta}{\theta^\alpha} \int_0^{\frac{\pi}{2}} \frac{\cos \phi d\phi}{(1 - \sin \phi)^\alpha} + \frac{2A}{L^2} \int_{\theta_c}^L \frac{\theta d\theta}{\theta^\alpha} \int_0^{\sin^{-1}(1 - \theta_c/\theta)} \frac{\cos \phi d\phi}{(1 - \sin \phi)^\alpha} \\ &= \frac{A}{L^\alpha} \left[\frac{2}{(1 - \alpha)(2 - \alpha)} \right] \left[1 - (2 - \alpha) \left(\frac{\theta_c}{L} \right)^{1 - \alpha} \left(1 - \frac{\theta_c}{L} \right) \right].\end{aligned} \quad (A2)$$

Equations (A1) and (A2) are the desired results. If $\theta_c > L$, we drop the factor inside the right set of brackets in Eq. (A2).

A parallel analysis can be done to compute the rms difference in counts between two parallel strips separated by a distance s . Omitting the details, we find that

$$\sigma^2 = \langle (N_1 - N_2)^2 \rangle = N[1 + N \langle w'_{12} \rangle] \quad (A3)$$

where

$$\langle w'_{12} \rangle = \frac{A\alpha}{(1 - \alpha)s^\alpha} \left(\frac{s}{L} \right). \quad (A4)$$

Here, N_1 and N_2 are the counts in each strip, $N = N_1 + N_2$, s is the separation of the strips and L is their length.

REFERENCES

- Boulanger, F., & Perault, M. 1988, ApJ, 330, 964
 Collins, C. A., Heydon-Dumbleton, N. H., and MacGillvray, H. T. 1988, MNRAS, 236, 7p

- de Lapparent, V., Geller, M. J., & Huchra, J. P. 1986, ApJL, 302, L1
- Geller, M. G., Huchra, J. P., Fabricant, D., Kurtz, M., & Thorstensen, J. 1991, private communication
- Groth, E., & Peebles, P. J. E. 1977, ApJ, 217, 385
- Lasker, B. et al. 1990, AJ, 99, 2019
- Maddox, S. J., Efstathiou, G., Sutherland, W. J., & Loveday, J. 1990, MNRAS, 242, 43p
- Peebles, P. J. E. *The Large-Scale Structure of the Universe* (Princeton University Press, Princeton), p. 152
- Peletier, R. F., Davies, R. L., Illingworth, G. D., Davis, L. E., & Cawson, M. 1990, AJ, 100, 1091
- Picard, A. 1991, AJ, 102, 445
- Postman, M., Geller, M. J., & Huchra, J. P. 1988, AJ, 95, 267
- Press, W. H., Flanner, B. P., Teukolsky, S. A., & Vetterlink, W. T. *Numerical Recipes* (Cambridge, Cambridge University Press)
- Thuan, T. X., & Gunn, J. E. 1976, PASP, 88, 543
- Zwicky, F. et al. 1961-1968 *Catalogue of Galaxies and of Clusters of Galaxies*, 6 vols. (Pasadena, California Institute of Technology).

FIGURE CAPTIONS

Fig. 1.—Isophotal contour plot of 2 star images, illustrating the variable amount of charge smearing. Column number increases vertically. The units are pixels (0.72"). The upper star was actually located around column number 800 on the CCD and has been shifted down for the figure.

Fig. 2.—Full width at half maximum (FWHM, in pixels) for bright objects as a function of column number. The FWHM is measured from east-west cuts that are perpendicular to the direction of the charge smearing. Note that in spite of the smearing, the width is nearly independent of column number. The line separating stars from galaxies is shown. All objects with widths greater than this were further inspected visually to eliminate double stars and other artifacts.

Fig. 3.—Correction to object magnitudes versus aperture radius for two y positions on the CCD.

Fig. 4.—Comparison of repeat magnitude measurements for stars and galaxies between two CCD frames.

Fig. 5.—Solid line: two-point angular correlation function for the complete sample of galaxies (to $r_W = 18.0$). Only galaxies in the contiguous 51° strip are used. The vertically-distributed points show the expected error in each bin used to com-

pute the correlation function. Dashed line: power-law portion of the correlation function given by Groth and Peebles (1977) scaled to the depth of the CCD survey.

Fig. 6.—Solid line: number galaxies in bins $11'$ wide by 5.1° long as a function of right ascension. Dotted line: number of Abell clusters with distance class $D = 0 - 5$ that lie within $\pm 2^\circ$ of declination from the galaxy strip.

Fig. 7.—Same as Fig. 6 except that Abell clusters $D = 6$ are shown instead.

Table 1
Galaxy Catalog

<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
1	11 48 30.13	29 33 57.6	16.56	15.4	46	12 0 39.43	29 32 53.9	17.50	9.2
2	11 48 36.12	29 36 52.8	17.77	8.8	47	12 0 46.42	29 31 3.7	16.38	16.6
3	11 48 36.73	29 39 2.1	17.78	8.8	48	12 0 46.93	29 41 38.0	16.02	18.2
4	11 48 42.78	29 40 56.1	17.47	5.8	49	12 0 55.59	29 32 3.6	17.78:	8.4
5	11 48 56.67	29 31 24.2	16.41	16.4	50	12 1 18.96	29 33 56.0	17.78	8.8
6	11 49 9.43	29 33 17.9	15.52	34.6	51	12 1 26.90	29 31 20.2	17.30	10.6
7	11 49 26.25	29 37 31.9	17.20	11.6	52	12 1 53.44	29 36 16.6	17.88	8.4
8	11 49 54.18	29 36 34.5	16.77:	13.2	53	12 1 55.77	29 36 33.4	17.37	10.4
9	11 50 8.06	29 35 40.5	17.03	12.4	54	12 2 6.76	29 34 11.1	17.94	8.0
10	11 50 12.28	29 36 25.0	13.44	63.4	55	12 2 8.87	29 33 20.9	17.22	11.2
11	11 50 13.76	29 37 2.5	17.29	5.8	56	12 2 31.41	29 31 14.6	17.94	8.0
12	11 50 32.82	29 36 14.3	17.81	8.6	57	12 3 46.59	29 33 32.5	17.24	11.2
13	11 51 8.91	29 31 46.7	15.45	28.8	58	12 3 50.92	29 32 5.3	17.72	8.6
14	11 51 38.62	29 32 42.0	17.82:	7.8	59	12 4 1.47	29 31 40.9	17.88	8.0
15	11 52 0.99	29 32 4.3	16.87	13.4	60	12 4 6.24	29 39 54.5	17.71	8.8
16	11 52 21.08	29 37 13.0	16.29	17.8	61	12 4 8.91	29 40 44.9	17.70	9.0
17	11 52 40.52	29 32 25.7	16.34	17.0	62	12 4 10.79	29 34 26.7	17.31	10.8
18	11 52 45.51	29 36 26.2	17.11	11.6	63	12 4 42.88	29 34 31.7	17.32	10.6
19	11 53 2.00	29 37 44.2	15.85	20.8	64	12 4 52.15	29 31 50.3	17.38:	9.8
20	11 53 4.62	29 29 46.7	17.41	10.2	65	12 5 9.20	29 30 44.2	17.54	9.6
21	11 53 11.44	29 33 0.1	16.90	13.0	66	12 5 14.03	29 30 15.1	17.55	9.2
22	11 54 6.13	29 37 41.1	16.49	16.2	67	12 5 15.75	29 32 1.4	16.95:	13.0
23	11 54 47.77	29 38 9.2	17.42	10.4	68	12 5 32.35	29 37 47.9	17.41	10.6
24	11 54 55.32	29 39 48.5	17.34	10.8	69	12 6 14.88	29 34 56.6	13.15	59.2
25	11 55 0.37	29 36 40.8	17.92	8.0	70	12 6 16.77	29 38 9.3	17.11	12.0
26	11 55 1.09	29 37 12.1	17.98	8.0	71	12 6 18.55	29 39 31.7	14.98	34.6
27	11 55 1.48	29 30 47.9	16.34	16.8	72	12 6 28.43	29 36 12.8	16.55:	14.2
28	11 56 35.86	29 41 7.3	17.43	10.6	73	12 6 29.04	29 31 38.3	13.88	37.4
29	11 56 53.08	29 40 20.2	17.99	8.0	74	12 6 29.32	29 36 19.0	17.65:	9.0
30	11 57 36.22	29 30 14.1	17.33	10.6	75	12 6 35.31	29 37 58.7	17.84	8.4
31	11 57 43.10	29 34 18.7	17.16	11.6	76	12 6 35.59	29 35 35.1	17.97	7.8
32	11 57 58.70	29 32 2.4	17.66	9.0	77	12 6 37.25	29 33 0.2	15.91	33.2
33	11 58 1.14	29 39 47.5	17.44	10.0	78	12 6 44.53	29 32 24.8	17.53	9.6
34	11 58 24.35	29 33 57.8	17.46	10.0	79	12 6 54.64	29 40 7.3	17.66	9.0
35	11 58 28.90	29 37 33.2	16.81	14.0	80	12 6 54.75	29 40 59.9	17.86	8.4
36	11 58 34.84	29 37 17.4	17.50	10.0	81	12 7 2.35	29 36 47.4	17.36	10.4
37	11 58 35.29	29 37 37.1	17.70	9.0	82	12 7 10.24	29 39 49.6	16.16	18.2
38	11 58 36.29	29 33 58.5	16.33	17.2	83	12 7 12.35	29 39 6.4	17.68	9.2
39	11 58 38.29	29 39 45.5	17.92	8.2	84	12 7 24.11	29 34 45.1	15.87	20.6
40	11 58 54.39	29 30 11.3	17.64	9.0	85	12 7 29.17	29 38 32.1	17.61	9.2
41	11 59 12.65	29 39 38.1	17.76	8.4	86	12 7 31.17	29 40 56.2	16.79	13.2
42	11 59 27.14	29 36 54.0	17.75	5.8	87	12 7 41.10	29 33 45.0	17.55	9.6
43	11 59 51.13	29 39 15.8	16.51	14.6	88	12 8 18.47	29 33 29.2	17.58:	9.6
44	11 59 58.62	29 31 10.9	17.17	10.0	89	12 8 30.13	29 41 11.9	17.96	8.0
45	12 0 12.67	29 39 38.7	16.45	16.0	90	12 8 41.56	29 32 9.5	17.54	9.4

<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
91	12 8 42.73	29 39 19.4	17.26	5.8	151	12 17 50.23	29 35 16.7	12.14	57.6
92	12 8 43.68	29 39 2.8	16.99:	12.6	152	12 17 56.40	29 41 10.0	17.96	8.0
93	12 9 3.88	29 33 59.2	17.81	8.6	153	12 18 5.28	29 34 33.4	16.68	14.6
94	12 9 12.60	29 36 8.0	17.77	8.6	154	12 18 11.67	29 37 20.9	13.53	63.4
95	12 9 20.98	29 30 37.0	16.86	13.2	155	12 18 44.81	29 36 6.6	16.67	14.0
96	12 9 21.48	29 35 36.6	16.48	15.8	156	12 19 15.19	29 40 30.6	17.23	11.4
97	12 9 31.65	29 41 39.0	16.44	16.4	157	12 19 20.30	29 40 6.6	16.90	13.0
98	12 9 33.87	29 39 39.8	17.87	8.4	158	12 19 25.84	29 32 26.9	16.79	13.6
99	12 9 48.19	29 41 2.7	17.80	8.8	159	12 19 26.52	29 38 49.5	17.44	10.2
100	12 9 48.68	29 30 36.7	17.83	8.4	160	12 19 44.22	29 30 18.4	17.74	8.8
101	12 9 51.07	29 30 57.0	17.90	8.0	161	12 20 39.70	29 37 33.7	14.76	50.4
102	12 9 51.35	29 31 17.7	17.26	11.0	162	12 20 55.75	29 39 10.6	17.95	8.2
103	12 10 10.46	29 41 6.9	15.98	20.0	163	12 21 37.90	29 41 22.1	17.25	11.4
104	12 10 33.04	29 32 31.4	17.94	7.8	164	12 21 43.88	29 36 5.4	17.96	8.0
105	12 10 40.71	29 39 5.9	17.60	9.4	165	12 21 45.28	29 38 37.7	17.81	8.4
106	12 10 41.60	29 37 57.8	17.79	8.4	166	12 21 46.28	29 41 33.0	16.47	16.2
107	12 10 47.93	29 40 30.9	17.03	12.4	167	12 22 10.87	29 35 52.2	17.55	9.8
108	12 10 54.97	29 32 9.8	16.12:	15.6	168	12 22 25.25	29 36 14.8	17.67:	5.8
109	12 10 56.58	29 31 59.0	15.97	21.6	169	12 24 59.17	29 36 17.9	17.98	8.0
110	12 10 59.14	29 32 25.0	17.94	7.8	170	12 25 0.38	29 30 21.6	16.63	14.2
111	12 11 1.52	29 32 40.5	16.61:	14.8	171	12 25 37.08	29 34 5.3	17.98	7.8
112	12 11 4.19	29 31 29.6	17.97	7.4	172	12 25 45.81	29 37 41.7	17.06	10.6
113	12 11 4.30	29 34 31.2	17.47	9.6	173	12 25 47.86	29 36 29.7	17.79	8.6
114	12 11 10.85	29 29 45.8	17.04	12.0	174	12 25 57.81	29 40 11.8	17.17	11.8
115	12 11 11.35	29 31 29.3	17.91	8.0	175	12 27 11.49	29 38 42.3	17.86	8.4
116	12 11 12.13	29 32 49.3	17.93	8.0	176	12 27 19.32	29 37 32.0	17.36:	10.2
117	12 11 12.18	29 30 21.0	17.61	9.2	177	12 27 49.56	29 31 37.0	17.22	10.6
118	12 11 15.35	29 31 14.4	17.63	9.0	178	12 27 52.79	29 35 36.5	17.39	10.4
119	12 11 23.68	29 36 51.9	17.69	9.0	179	12 28 44.88	29 37 41.6	17.97	7.8
120	12 12 1.88	29 37 31.6	17.96	8.0	180	12 29 14.41	29 32 44.3	17.85	8.0
121	12 12 2.88	29 38 11.2	17.42	10.2	181	12 29 51.67	29 33 27.8	16.31	17.2
122	12 12 8.82	29 33 54.2	16.19	24.6	182	12 29 53.24	29 41 12.3	16.58	15.6
123	12 12 13.93	29 35 29.3	16.23	18.0	183	12 30 7.99	29 32 43.1	17.52	9.6
124	12 12 14.31	29 32 31.1	17.22	11.2	184	12 30 12.67	29 39 32.2	17.15:	11.8
125	12 12 44.74	29 31 39.6	16.25	16.8	185	12 30 15.11	29 39 23.7	14.96	27.4
126	12 13 1.28	29 36 3.1	17.87	8.2	186	12 30 19.67	29 39 58.0	17.11:	10.6
127	12 13 3.72	29 33 13.2	17.92	8.0	187	12 30 37.53	29 34 25.0	17.21	11.0
128	12 13 19.22	29 40 10.3	17.86	8.4	188	12 31 14.96	29 34 47.7	17.88	8.4
129	12 14 3.02	29 32 24.3	17.84	8.0	189	12 31 56.49	29 34 7.5	17.87	8.0
130	12 14 5.01	29 30 0.7	17.88	8.0	190	12 32 16.85	29 30 31.7	16.28	17.2
131	12 14 27.45	29 34 52.2	17.14	11.4	191	12 33 5.46	29 38 55.7	17.97	8.0
132	12 14 57.65	29 35 53.2	17.32	10.8	192	12 33 19.11	29 35 7.1	17.79	8.8
133	12 15 0.82	29 34 52.5	17.87	8.2	193	12 33 20.06	29 37 37.7	17.16	11.6
134	12 15 3.82	29 36 57.2	17.81	8.6	194	12 33 58.58	29 33 5.6	17.73	8.4
135	12 15 31.92	29 41 16.8	17.01	12.6	195	12 34 13.52	29 34 39.7	17.53	9.8
136	12 15 33.86	29 40 21.6	16.66	14.8	196	12 35 54.93	29 40 2.7	17.72	8.4
137	12 15 41.28	29 31 37.2	15.98:	19.2	197	12 38 9.17	29 32 24.3	17.42	10.0
138	12 15 42.84	29 34 15.3	17.71	8.6	198	12 38 44.02	29 34 49.5	17.47	10.0
139	12 15 44.17	29 30 6.7	17.58	5.8	199	12 38 48.03	29 38 26.3	17.47	10.0
140	12 15 46.67	29 31 57.2	17.51:	9.0	200	12 39 2.87	29 39 55.2	16.39	15.0
141	12 15 48.45	29 31 46.1	14.79	43.2	201	12 39 29.58	29 36 48.5	17.70	9.0
142	12 15 49.33	29 31 18.3	16.98	12.0	202	12 39 48.56	29 29 38.6	17.48	9.8
143	12 15 50.29	29 39 7.5	17.98	8.0	203	12 41 15.77	29 39 13.9	17.81	8.4
144	12 16 13.66	29 39 23.0	16.69:	13.2	204	12 41 28.72	29 38 33.4	17.30	11.0
145	12 16 30.27	29 30 53.9	17.77	8.6	205	12 42 4.13	29 30 15.9	16.63	14.6
146	12 16 32.33	29 37 43.3	16.62	15.2	206	12 42 40.10	29 34 20.1	17.50	10.0
147	12 17 7.95	29 31 51.5	17.60	21.6	207	12 42 50.95	29 39 19.8	17.93	8.2
148	12 17 13.57	29 29 33.0	17.54	9.6	208	12 42 59.18	29 40 19.1	17.22	11.6
149	12 17 20.37	29 41 6.8	17.89	8.4	209	12 43 7.66	29 37 6.0	17.06	12.0
150	12 17 36.24	29 33 29.0	10.21	129.8	210	12 43 11.27	29 34 43.5	16.33	17.2

<i>ID</i>	<i>R.A.</i> ₍₁₉₆₀₎	<i>Decl.</i> ₍₁₉₆₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₆₀₎	<i>Decl.</i> ₍₁₉₆₀₎	<i>Mag.</i>	<i>Rad.</i> (")
211	12 43 16.61	29 36 14.6	16.46	16.2	271	12 59 46.17	29 34 18.3	17.68	8.8
212	12 43 23.56	29 37 52.0	17.95	8.0	272	12 59 53.28	29 32 44.9	17.05	12.0
213	12 43 44.96	29 39 48.4	17.98	8.0	273	13 0 49.12	29 34 11.1	17.42	13.0
214	12 43 48.18	29 41 2.0	17.99	8.0	274	13 0 50.73	29 34 8.3	17.88	8.2
215	12 44 20.13	29 39 40.0	16.56	15.0	275	13 1 13.79	29 33 59.2	17.28:	10.6
216	12 44 45.76	29 30 54.6	17.58	9.4	276	13 1 17.06	29 32 23.4	17.40	10.2
217	12 45 1.52	29 39 32.2	17.60	9.6	277	13 1 32.15	29 38 11.0	17.76	8.8
218	12 45 10.51	29 36 35.1	17.48	10.0	278	13 1 59.99	29 39 2.6	16.21:	17.2
219	12 45 41.87	29 30 36.0	17.27	10.8	279	13 2 15.55	29 29 21.8	16.31	16.4
220	12 46 4.38	29 31 49.5	16.85:	12.6	280	13 2 26.99	29 29 46.7	17.32	10.6
221	12 46 16.77	29 30 31.5	16.22:	16.2	281	13 3 2.02	29 33 47.9	14.36	40.4
222	12 46 57.96	29 35 35.3	17.04	11.2	282	13 3 15.16	29 29 46.1	17.52	9.6
223	12 47 13.13	29 35 59.5	15.83	21.4	283	13 3 15.31	29 36 59.7	17.44:	9.0
224	12 47 18.93	29 40 35.7	17.84	8.4	284	13 3 28.13	29 33 23.7	17.60	9.4
225	12 47 30.50	29 30 48.6	17.60	9.2	285	13 3 36.46	29 32 42.8	14.18	46.2
226	12 48 10.60	29 40 23.4	17.84	8.4	286	13 4 3.90	29 32 11.7	17.90	7.8
227	12 48 30.51	29 33 11.6	16.37:	14.4	287	13 4 9.99	29 37 55.4	16.19	16.8
228	12 48 50.60	29 41 5.4	17.86	8.0	288	13 4 21.99	29 38 16.4	16.29	17.0
229	12 48 59.43	29 40 9.1	17.22	11.4	289	13 4 22.42	29 36 9.3	16.71	13.4
230	12 48 59.74	29 33 17.6	17.67	8.6	290	13 4 31.03	29 35 29.1	17.98	7.8
231	12 49 4.74	29 33 21.5	17.91	8.2	291	13 4 31.67	29 31 12.6	17.43	26.0
232	12 49 39.63	29 33 29.5	17.34	10.2	292	13 5 0.11	29 40 3.1	16.75	13.8
233	12 49 43.87	29 36 54.8	17.49	10.0	293	13 5 10.14	29 35 37.3	17.46	10.0
234	12 49 59.80	29 34 48.0	17.33	10.0	294	13 5 19.30	29 32 46.9	17.73	8.4
235	12 50 19.21	29 38 56.0	17.18	11.0	295	13 5 39.56	29 29 44.1	17.62	9.0
236	12 50 27.78	29 29 34.3	16.67	14.2	296	13 5 58.89	29 29 29.6	16.05:	16.8
237	12 50 40.10	29 37 37.4	17.70	9.0	297	13 6 5.06	29 40 18.4	15.00	20.2
238	12 50 40.66	29 39 58.7	15.75	13.0	298	13 6 11.21	29 36 45.5	17.74	8.2
239	12 50 42.39	29 40 17.6	17.35	10.8	299	13 6 12.22	29 29 4.6	17.30	10.6
240	12 50 56.63	29 32 48.9	17.35	10.6	300	13 6 33.95	29 29 59.7	17.68	14.4
241	12 51 31.45	29 40 42.7	17.97	8.0	301	13 6 50.12	29 40 25.1	17.73	8.8
242	12 51 40.45	29 40 43.2	17.75	9.0	302	13 6 53.50	29 37 59.0	14.84	31.8
243	12 51 41.24	29 30 40.5	16.46	15.0	303	13 7 3.18	29 40 3.5	17.26	11.0
244	12 51 49.49	29 36 10.4	17.53	9.8	304	13 7 11.80	29 33 25.2	16.71	7.4
245	12 53 36.97	29 31 19.4	15.54	27.4	305	13 7 18.00	29 29 9.4	16.51	0.4
246	12 53 37.19	29 31 55.7	16.87	12.6	306	13 8 14.95	29 29 45.4	17.97	7.6
247	12 53 41.87	29 33 19.5	17.81	8.4	307	13 9 55.48	29 34 36.1	17.76	8.6
248	12 53 55.54	29 34 10.4	15.19	41.8	308	13 9 59.28	29 37 29.7	16.93	12.8
249	12 54 26.57	29 38 52.1	15.32	43.2	309	13 10 1.68	29 39 36.0	17.70	9.2
250	12 55 39.56	29 37 2.1	17.60	9.6	310	13 10 11.92	29 33 43.0	17.47	9.8
251	12 55 50.42	29 30 36.5	17.67	9.0	311	13 10 27.70	29 34 3.2	17.78	8.4
252	12 57 13.55	29 32 43.5	17.98	7.6	312	13 11 17.55	29 35 56.0	17.19	0.4
253	12 57 21.92	29 29 28.1	16.92	12.4	313	13 11 30.10	29 34 37.7	16.44	16.0
254	12 57 39.08	29 38 40.2	17.65	9.2	314	13 11 39.58	29 40 15.1	15.43	31.8
255	12 57 57.07	29 36 18.8	15.46	26.0	315	13 12 15.88	29 34 51.4	16.15:	46.2
256	12 58 6.79	29 36 33.7	17.65	9.2	316	13 13 4.71	29 34 40.8	17.92	8.0
257	12 58 17.83	29 33 17.5	17.32	10.8	317	13 13 19.49	29 35 32.5	15.57	33.2
258	12 58 29.77	29 31 50.5	17.39	5.8	318	13 13 24.20	29 40 57.2	17.67	9.2
259	12 58 48.89	29 33 53.4	17.75	8.4	319	13 13 28.49	29 35 2.6	17.75	8.6
260	12 58 51.53	29 38 18.3	16.37:	16.2	320	13 13 37.03	29 32 31.7	16.14:	18.2
261	12 58 53.36	29 38 22.3	17.72:	9.0	321	13 13 42.41	29 30 54.2	17.39	10.0
262	12 58 58.13	29 36 27.9	16.62	14.6	322	13 13 42.46	29 38 40.2	16.80	13.6
263	12 59 0.09	29 38 45.3	16.96:	14.4	323	13 13 49.63	29 31 16.3	17.99	7.4
264	12 59 0.62	29 34 36.4	13.58:	14.4	324	13 14 51.58	29 31 13.1	17.32	10.6
265	12 59 1.40	29 34 53.7	14.92:	10.0	325	13 15 12.41	29 30 54.4	17.13	11.6
266	12 59 15.74	29 36 17.9	16.49	12.2	326	13 15 23.27	29 34 18.5	17.80	8.6
267	12 59 17.70	29 38 58.7	16.78	13.2	327	13 16 28.14	29 39 19.4	16.56	15.4
268	12 59 31.34	29 34 16.3	17.24	10.8	328	13 16 31.03	29 39 48.7	17.99	8.0
269	12 59 32.01	29 35 26.1	15.63	27.4	329	13 16 32.32	29 33 46.8	17.95	8.0
270	12 59 40.38	29 31 16.9	13.78	40.4	330	13 16 33.62	29 36 36.4	17.59	9.2

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331	13 16 51.29	29 30 16.8	17.03	31.8	391	13 33 2.82	29 35 55.8	16.68	14.6
332	13 16 54.95	29 36 40.5	17.69	9.0	392	13 33 6.22	29 36 56.3	17.19	10.2
333	13 16 54.97	29 31 5.0	17.86	8.0	393	13 33 6.66	29 37 1.6	17.56	8.4
334	13 17 39.17	29 35 57.4	16.90:	12.6	394	13 33 14.10	29 30 16.4	17.53	9.6
335	13 17 47.22	29 34 54.2	17.86	8.2	395	13 33 40.96	29 33 12.4	16.16	18.8
336	13 18 12.41	29 38 31.9	16.70	13.6	396	13 33 42.41	29 40 12.4	17.54	9.2
337	13 18 24.62	29 28 55.4	17.83	8.0	397	13 33 52.95	29 38 53.7	15.95	18.2
338	13 18 28.96	29 30 25.1	17.09:	10.6	398	13 34 11.29	29 39 58.4	15.44	34.6
339	13 18 29.29	29 30 8.8	17.75:	8.2	399	13 34 30.63	29 40 34.0	17.97	8.0
340	13 18 33.40	29 37 30.5	16.55:	15.6	400	13 34 30.76	29 36 33.0	17.69	9.0
341	13 18 34.41	29 30 17.8	17.78	8.4	401	13 34 34.10	29 30 54.6	17.65	9.2
342	13 18 35.86	29 31 0.1	17.42	10.0	402	13 34 45.68	29 40 20.9	17.02	12.4
343	13 18 41.51	29 29 27.3	17.99	7.6	403	13 34 59.12	29 39 12.1	16.85	13.6
344	13 18 45.01	29 37 32.8	15.66	21.6	404	13 35 26.45	29 39 16.8	17.95	8.0
345	13 18 48.71	29 33 37.0	17.99	7.8	405	13 35 29.85	29 34 13.5	17.67	9.0
346	13 18 56.27	29 33 59.6	16.96	12.4	406	13 35 30.03	29 28 51.7	17.83	8.4
347	13 19 5.77	29 34 34.5	16.74	13.8	407	13 35 31.36	29 35 3.0	17.70	9.0
348	13 19 8.14	29 39 59.4	17.65	8.2	408	13 35 34.47	29 35 17.3	16.05	19.0
349	13 19 8.38	29 34 26.6	17.54:	9.0	409	13 35 35.98	29 36 33.0	17.98	8.0
350	13 19 8.55	29 34 20.4	17.37:	10.0	410	13 35 50.67	29 39 21.9	17.01	12.6
351	13 19 22.40	29 29 12.0	16.83:	12.6	411	13 36 5.37	29 36 22.7	17.26	10.8
352	13 19 37.69	29 31 36.3	17.66	8.8	412	13 36 6.78	29 39 3.2	17.55	9.8
353	13 19 43.63	29 31 8.4	17.02	12.2	413	13 36 48.90	29 34 13.0	16.85	13.6
354	13 19 59.56	29 29 7.3	17.65	8.4	414	13 37 2.26	29 30 21.0	15.82:	13.6
355	13 20 20.06	29 36 10.4	16.60	15.0	415	13 37 2.42	29 30 13.1	16.53	14.4
356	13 20 23.59	29 40 11.8	16.52	15.6	416	13 37 11.70	29 36 42.8	16.30	15.6
357	13 20 42.51	29 38 5.3	16.47	15.8	417	13 37 13.59	29 36 37.0	14.60	28.8
358	13 20 42.52	29 38 4.2	16.43	16.0	418	13 37 22.65	29 37 32.7	17.40	10.4
359	13 21 15.80	29 32 23.1	17.92	7.8	419	13 37 23.70	29 30 19.5	17.49	9.8
360	13 21 17.25	29 32 48.5	17.99	7.8	420	13 37 23.88	29 38 26.0	15.50	39.0
361	13 22 16.50	29 36 38.5	15.97:	14.0	421	13 37 27.69	29 29 1.0	17.19	11.6
362	13 22 36.97	29 40 7.9	17.47:	10.0	422	13 37 32.35	29 34 45.1	17.26	1.6
363	13 22 53.74	29 40 25.3	15.68	20.2	423	13 37 34.60	29 37 49.3	16.56:	15.2
364	13 23 14.63	29 31 45.1	17.25	11.0	424	13 37 34.88	29 37 56.0	16.59:	15.2
365	13 23 28.41	29 39 42.1	17.55	9.8	425	13 37 36.48	29 30 25.5	17.72	8.8
366	13 23 47.97	29 33 50.6	17.61:	9.4	426	13 37 37.59	29 36 41.5	15.75	23.0
367	13 23 53.84	29 38 36.0	17.77	8.4	427	13 37 41.25	29 36 17.5	17.57	9.6
368	13 23 56.01	29 39 2.4	17.65:	9.4	428	13 37 52.66	29 32 11.4	17.67	9.0
369	13 23 58.91	29 40 21.4	17.97:	8.0	429	13 37 58.44	29 39 29.5	17.73	9.0
370	13 24 33.52	29 33 11.2	17.59	9.6	430	13 38 3.27	29 32 26.7	17.75:	8.6
371	13 25 2.24	29 39 15.3	17.78	8.6	431	13 38 3.71	29 32 18.3	17.58:	34.6
372	13 25 32.10	29 36 16.8	17.37	10.6	432	13 38 6.22	29 38 44.0	17.36	10.6
373	13 26 2.46	29 39 29.6	16.40	1.6	433	13 38 15.89	29 32 45.1	17.78	8.6
374	13 28 58.28	29 37 29.7	14.51	54.8	434	13 38 24.45	29 40 4.3	15.85:	20.8
375	13 29 26.97	29 39 27.2	17.87	8.4	435	13 38 37.29	29 34 52.7	17.21	11.4
376	13 29 47.12	29 37 50.1	17.90	8.2	436	13 38 37.44	29 32 16.5	17.47	10.0
377	13 29 54.06	29 38 10.3	17.24	11.2	437	13 38 43.77	29 32 39.0	17.61	9.4
378	13 29 57.55	29 28 49.6	17.80	8.4	438	13 38 44.17	29 33 42.6	17.30:	10.8
379	13 30 0.77	29 28 49.0	17.81	8.4	439	13 38 44.78	29 39 52.1	17.81	8.4
380	13 30 2.25	29 33 30.3	17.59	9.6	440	13 38 45.68	29 34 47.0	17.18	11.6
381	13 30 2.77	29 35 44.6	17.96	8.0	441	13 38 46.88	29 31 54.0	17.98	7.6
382	13 30 24.70	29 34 19.6	17.99	8.0	442	13 38 49.82	29 31 37.4	16.93	12.6
383	13 30 32.10	29 36 7.7	17.21	11.6	443	13 38 55.16	29 38 49.5	16.22:	17.8
384	13 31 16.33	29 36 24.9	16.78:	13.2	444	13 38 55.21	29 38 41.3	16.34:	14.0
385	13 31 55.24	29 32 32.7	16.97	12.8	445	13 39 20.70	29 31 0.2	17.25	14.4
386	13 32 20.46	29 32 29.7	17.83	8.4	446	13 40 7.36	29 36 53.8	16.97	12.6
387	13 32 32.73	29 31 57.2	17.60	9.2	447	13 40 19.11	29 34 31.9	15.57	23.0
388	13 32 39.38	29 36 5.9	17.71	9.0	448	13 40 24.61	29 34 33.2	17.97	8.0
389	13 32 45.06	29 31 3.7	17.36	10.6	449	13 40 32.34	29 35 1.9	16.60	14.8
390	13 33 0.54	29 35 55.4	15.79	21.6	450	13 40 38.95	29 34 35.5	17.95	8.2

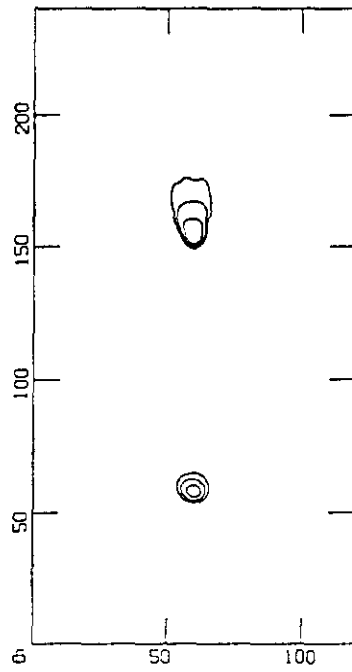
<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
451	13 40 41.20	29 38 14.1	15.99	18.6	511	13 51 23.94	29 37 42.1	17.74	9.0
452	13 41 7.48	29 32 22.8	16.14	18.8	512	13 51 25.90	29 39 4.0	17.80	8.6
453	13 41 14.60	29 39 50.1	16.70:	12.4	513	13 51 56.31	29 35 10.4	17.19	11.6
454	13 41 14.88	29 40 2.4	16.84:	12.0	514	13 52 50.81	29 33 20.0	17.86:	8.0
455	13 42 11.80	29 31 59.4	17.98	7.6	515	13 52 56.80	29 38 10.5	17.54	8.8
456	13 42 16.31	29 38 47.8	17.87	8.4	516	13 53 20.57	29 38 48.7	17.51	10.0
457	13 42 25.85	29 37 16.4	17.74	8.8	517	13 54 15.08	29 38 34.2	17.72	8.4
458	13 42 32.83	29 28 43.9	16.72:	14.0	518	13 54 46.62	29 38 56.4	17.70	8.8
459	13 43 24.79	29 30 40.8	17.85	8.2	519	13 55 21.92	29 32 34.2	17.82	8.4
460	13 43 26.11	29 30 12.4	15.91	20.6	520	13 55 23.25	29 31 52.6	17.96	8.0
461	13 43 49.44	29 35 35.3	17.83	8.2	521	13 55 26.85	29 36 38.1	16.19:	17.4
462	13 44 5.98	29 33 53.8	17.15	11.2	522	13 56 20.99	29 37 52.5	16.52	15.4
463	13 44 21.47	29 32 44.4	16.83	12.8	523	13 56 21.13	29 35 51.8	17.79	8.0
464	13 44 25.56	29 36 53.8	14.97	34.6	524	13 56 28.99	29 32 57.0	16.13	18.8
465	13 44 33.15	29 28 44.3	17.67	8.6	525	13 56 33.65	29 33 9.0	17.70	9.0
466	13 44 45.76	29 34 22.2	17.91	8.2	526	13 56 58.32	29 28 59.0	17.32	10.6
467	13 44 47.75	29 40 7.0	17.35	10.2	527	13 57 3.66	29 30 2.3	15.85:	17.2
468	13 45 19.89	29 30 38.0	17.46	9.8	528	13 57 30.76	29 30 50.9	17.37	10.4
469	13 45 43.88	29 35 59.0	17.89	8.2	529	13 57 41.05	29 28 23.2	17.37	10.0
470	13 46 2.76	29 35 13.3	17.95	8.0	530	13 58 5.32	29 33 48.4	14.95	31.4
471	13 46 10.35	29 33 25.3	17.72	9.0	531	13 58 6.64	29 35 30.0	17.61	9.4
472	13 46 36.77	29 36 59.4	16.67	14.8	532	13 58 27.39	29 30 14.2	17.62	9.0
473	13 46 59.22	29 37 16.5	17.65:	9.2	533	13 58 59.65	29 38 54.4	15.15	31.4
474	13 47 7.36	29 35 25.0	17.57:	9.2	534	13 59 14.65	29 36 1.8	17.95	8.0
475	13 47 7.67	29 32 46.2	16.72	14.2	535	13 59 14.80	29 28 29.0	17.31:	10.4
476	13 47 35.19	29 34 40.7	17.87	8.4	536	13 59 27.51	29 35 0.7	17.76	9.0
477	13 47 50.95	29 39 7.6	16.32:	16.6	537	13 59 33.65	29 38 48.5	17.15	11.6
478	13 47 52.58	29 28 57.7	16.50	15.2	538	14 0 1.96	29 34 20.6	17.48	9.4
479	13 48 0.69	29 29 28.7	16.73:	13.6	539	14 0 15.57	29 36 32.8	15.14	23.0
480	13 48 9.32	29 31 4.8	17.33	10.6	540	14 0 21.32	29 29 13.5	17.65	9.0
481	13 48 11.76	29 31 21.0	16.41	16.0	541	14 0 35.43	29 36 41.1	16.82	13.0
482	13 48 15.69	29 29 47.5	17.21	11.0	542	14 0 53.70	29 33 21.8	17.42:	10.2
483	13 48 18.15	29 37 9.5	14.46	40.4	543	14 0 54.98	29 33 26.8	17.40:	10.0
484	13 48 19.60	29 32 9.9	16.94:	13.0	544	14 1 1.03	29 28 24.0	17.13	11.2
485	13 48 22.11	29 38 56.8	16.59	14.8	545	14 1 12.32	29 31 0.4	17.60	9.2
486	13 48 44.87	29 31 46.5	17.14	11.2	546	14 1 29.28	29 35 4.5	15.32	34.6
487	13 48 50.79	29 34 56.3	17.86	8.4	547	14 1 30.62	29 36 4.3	15.25	30.2
488	13 48 54.06	29 34 27.3	15.96	19.8	548	14 1 33.72	29 35 24.5	16.69	14.4
489	13 49 7.45	29 36 37.6	17.28	10.8	549	14 1 36.85	29 37 29.3	16.73	14.2
490	13 49 14.30	29 38 9.7	17.28	11.0	550	14 1 49.19	29 34 38.3	15.71	27.4
491	13 49 15.92	29 39 47.8	16.37:	15.6	551	14 1 54.42	29 31 23.5	17.51	9.6
492	13 49 17.09	29 39 47.3	17.20:	10.8	552	14 2 38.60	29 32 59.4	17.03	11.6
493	13 49 21.79	29 31 43.4	17.95	7.8	553	14 2 58.75	29 39 20.8	15.01	34.6
494	13 49 24.95	29 30 50.1	17.25	11.0	554	14 3 1.08	29 39 45.7	15.04	18.8
495	13 49 26.65	29 34 40.6	14.41	21.6	555	14 3 2.98	29 35 25.5	15.74	23.0
496	13 49 27.64	29 33 2.9	17.42	10.0	556	14 3 15.74	29 35 40.2	17.27:	10.8
497	13 49 31.52	29 38 50.0	17.17	11.0	557	14 3 21.71	29 38 57.3	16.26	17.8
498	13 49 32.61	29 30 39.3	17.78	8.4	558	14 3 32.52	29 38 34.3	16.15	18.8
499	13 49 40.86	29 33 32.9	13.83:	21.6	559	14 4 1.49	29 39 26.6	16.95	13.0
500	13 50 4.23	29 37 45.8	17.91	8.2	560	14 4 9.02	29 38 37.6	15.65:	26.0
501	13 50 11.40	29 31 44.8	17.67	8.8	561	14 4 9.24	29 38 28.2	15.61:	26.0
502	13 50 12.56	29 31 7.3	17.68	9.0	562	14 4 29.34	29 35 14.9	16.08:	19.0
503	13 50 13.34	29 31 39.2	16.86	13.4	563	14 4 29.56	29 29 50.8	17.60	8.8
504	13 50 17.61	29 36 30.8	17.97	5.8	564	14 4 45.40	29 32 1.9	17.73	8.6
505	13 50 19.93	29 34 54.3	17.68	9.2	565	14 5 7.74	29 31 6.2	17.94:	7.6
506	13 50 31.97	29 39 31.7	17.60	9.4	566	14 5 19.31	29 38 24.8	16.49:	15.4
507	13 50 44.13	29 38 49.3	17.03	12.4	567	14 5 22.23	29 31 26.2	16.61	14.6
508	13 50 53.89	29 37 0.9	17.39	10.4	568	14 5 30.03	29 29 59.3	16.74:	13.2
509	13 50 56.12	29 38 21.4	17.85	8.4	569	14 5 33.81	29 35 43.9	16.80	14.0
510	13 51 10.89	29 31 20.9	17.18	11.0	570	14 5 41.97	29 31 6.2	17.66:	8.8

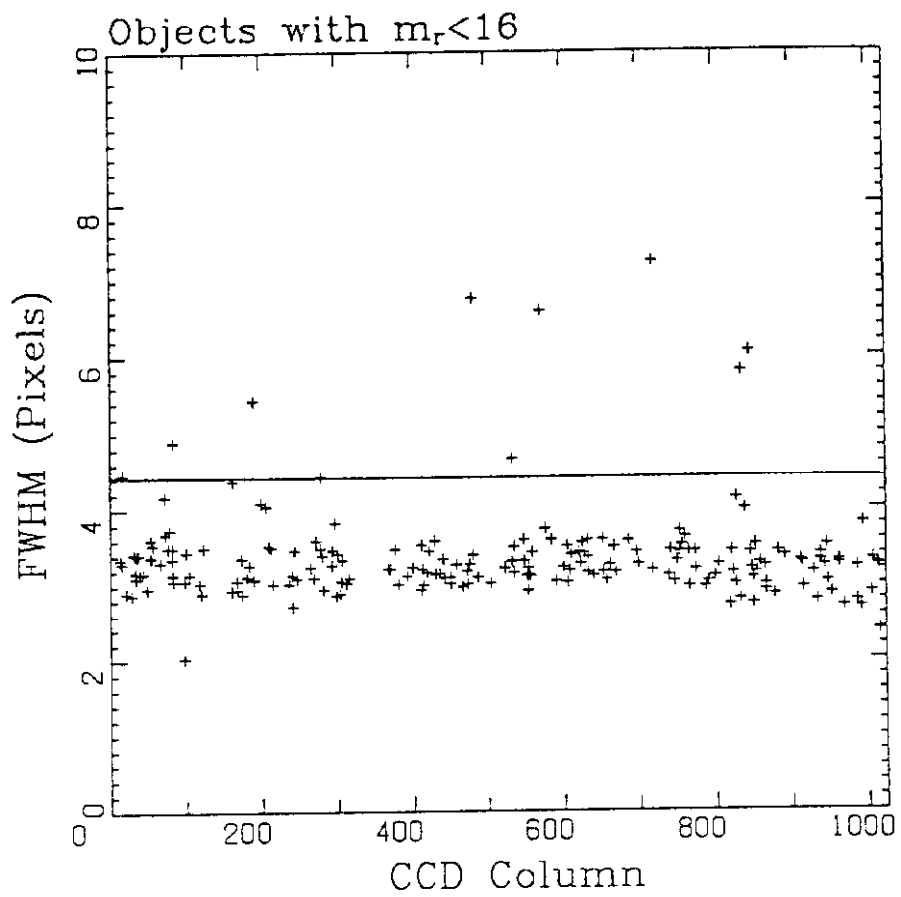
<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
571	14 6 1.03	29 29 15.9	17.66	8.8	631	14 17 52.10	29 33 49.2	17.53:	9.8
572	14 6 56.07	29 34 53.5	17.86	8.4	632	14 20 37.76	29 31 52.1	17.79	8.4
573	14 7 14.89	29 31 47.0	17.75	8.8	633	14 20 38.17	29 38 39.5	17.36	10.6
574	14 7 17.91	29 28 56.1	17.79:	7.8	634	14 20 40.58	29 35 37.8	16.41	16.2
575	14 7 30.10	29 27 35.8	17.43	10.0	635	14 21 35.80	29 33 21.2	17.83	8.4
576	14 7 40.24	29 31 42.5	17.47	10.0	636	14 21 43.61	29 27 57.0	16.20	17.2
577	14 7 40.71	29 38 53.7	17.82	8.4	637	14 21 52.89	29 34 7.7	16.28	17.2
578	14 7 40.94	29 35 6.1	17.52	9.8	638	14 22 27.29	29 30 5.2	16.33	17.0
579	14 7 41.57	29 31 14.4	17.10	11.6	639	14 22 39.60	29 34 13.7	15.37	31.8
580	14 7 44.41	29 32 50.9	17.51	9.6	640	14 22 45.19	29 38 14.9	17.39	10.4
581	14 8 0.04	29 36 20.3	16.96	13.2	641	14 22 48.21	29 30 59.7	17.67:	9.0
582	14 8 8.92	29 32 5.5	16.72	14.2	642	14 22 48.52	29 34 4.6	17.19	11.6
583	14 8 29.85	29 38 30.2	17.41	10.0	643	14 22 48.54	29 30 31.1	15.22	26.0
584	14 8 41.74	29 39 38.4	17.86	8.4	644	14 22 53.71	29 36 5.1	17.29	11.0
585	14 8 45.78	29 28 49.8	16.85:	12.8	645	14 23 2.09	29 31 54.4	16.69	14.4
586	14 8 47.56	29 29 20.3	17.41	9.6	646	14 23 3.80	29 36 0.9	15.64	24.6
587	14 8 47.56	29 34 44.9	17.10	11.8	647	14 23 23.32	29 35 25.8	17.66	9.2
588	14 8 53.24	29 36 23.1	17.21	11.6	648	14 23 30.23	29 33 51.1	17.18:	11.0
589	14 8 57.00	29 30 34.7	15.03	37.4	649	14 25 8.10	29 35 36.9	17.06	12.2
590	14 9 2.67	29 32 1.2	17.38:	10.0	650	14 25 15.31	29 27 17.0	17.30	10.4
591	14 9 20.94	29 38 20.0	16.78	13.6	651	14 25 17.78	29 38 15.8	16.60:	14.6
592	14 9 21.86	29 36 39.4	16.86	13.2	652	14 25 28.64	29 37 2.9	17.53	10.0
593	14 9 39.31	29 39 2.6	17.84	8.6	653	14 25 35.84	29 36 34.5	17.12	12.0
594	14 9 43.24	29 28 5.2	17.87	7.8	654	14 25 49.29	29 38 50.5	16.18:	18.4
595	14 10 0.32	29 33 21.1	17.88	7.8	655	14 26 6.80	29 32 21.2	17.47:	10.0
596	14 10 31.82	29 36 48.5	17.43	10.4	656	14 26 8.12	29 32 2.3	15.58	26.0
597	14 10 38.99	29 28 16.2	17.29	10.4	657	14 26 9.38	29 34 53.4	15.67:	19.6
598	14 11 14.00	29 29 5.2	17.36	11.6	658	14 26 55.82	29 27 25.0	16.67	14.0
599	14 11 14.07	29 30 36.6	16.39	16.8	659	14 27 42.71	29 33 23.4	17.73	8.6
600	14 11 31.00	29 36 28.7	17.16	11.6	660	14 27 48.51	29 31 17.0	15.98	19.6
601	14 11 37.17	29 37 20.2	16.32	16.6	661	14 28 43.61	29 37 34.7	17.98	8.0
602	14 11 40.70	29 35 32.6	17.92	8.2	662	14 28 43.64	29 37 36.4	17.76	8.8
603	14 12 14.58	29 35 1.0	17.39	10.4	663	14 28 46.17	29 34 3.0	17.79	8.4
604	14 13 12.24	29 37 2.9	16.16	18.2	664	14 28 50.58	29 28 44.3	17.94	7.6
605	14 13 13.37	29 34 25.5	17.88	8.2	665	14 29 26.09	29 30 41.5	17.31	10.6
606	14 13 20.53	29 34 28.9	17.72	9.0	666	14 29 43.91	29 36 26.9	16.46	16.6
607	14 13 21.69	29 34 11.9	17.31	10.6	667	14 29 53.31	29 29 24.2	17.90	8.0
608	14 13 22.25	29 34 41.9	17.93	8.2	668	14 30 51.32	29 33 59.9	17.78	8.8
609	14 13 24.08	29 34 5.4	16.14	18.2	669	14 31 6.65	29 27 1.0	16.41	16.2
610	14 13 36.07	29 30 42.2	17.17	11.4	670	14 31 28.39	29 36 2.4	17.50	10.0
611	14 13 39.17	29 39 18.3	17.25	11.2	671	14 31 36.65	29 27 5.4	17.75	8.4
612	14 13 45.36	29 37 31.2	16.82	14.0	672	14 31 46.18	29 38 54.6	16.84	13.6
613	14 13 51.42	29 39 9.7	15.94:	19.2	673	14 31 59.62	29 35 56.9	15.79:	19.2
614	14 13 57.19	29 34 4.0	17.59	9.6	674	14 32 6.60	29 26 49.8	16.23	17.6
615	14 14 14.07	29 35 51.1	17.89	8.4	675	14 32 11.95	29 33 13.8	17.09	12.0
616	14 14 32.55	29 31 20.6	17.61	9.4	676	14 32 24.26	29 37 47.1	15.03	34.6
617	14 14 39.65	29 36 39.9	17.02	12.6	677	14 32 49.99	29 33 29.7	17.82	8.0
618	14 14 42.63	29 30 0.5	15.60	30.2	678	14 32 59.25	29 28 46.8	17.13	11.6
619	14 14 42.81	29 31 11.6	17.29	11.0	679	14 33 8.63	29 33 12.6	17.86	8.2
620	14 14 45.49	29 37 31.7	17.26	11.0	680	14 35 3.27	29 29 36.0	16.24:	17.2
621	14 15 3.27	29 30 17.8	17.59	9.0	681	14 35 4.37	29 29 11.4	17.08:	11.6
622	14 15 21.62	29 34 28.8	17.40	10.4	682	14 35 21.14	29 34 57.5	16.37:	16.2
623	14 15 21.96	29 35 21.3	17.88	8.0	683	14 35 22.25	29 35 27.1	16.43:	15.6
624	14 15 41.78	29 27 27.0	15.33	26.0	684	14 35 43.22	29 35 44.7	16.01:	17.4
625	14 15 58.05	29 37 54.3	17.22	11.6	685	14 35 44.61	29 35 46.8	15.65:	19.8
626	14 16 42.60	29 29 37.7	17.56	8.4	686	14 36 33.66	29 29 24.7	17.98	7.6
627	14 16 47.29	29 32 0.3	16.95	13.0	687	14 36 44.65	29 34 13.7	17.78	9.0
628	14 16 53.17	29 32 14.1	16.12	18.4	688	14 37 11.69	29 36 52.6	16.75:	14.2
629	14 17 24.86	29 38 14.4	17.32	11.0	689	14 37 12.79	29 32 22.7	17.33	10.2
630	14 17 46.58	29 35 43.7	17.42	10.4	690	14 37 40.61	29 34 41.4	17.65	9.0

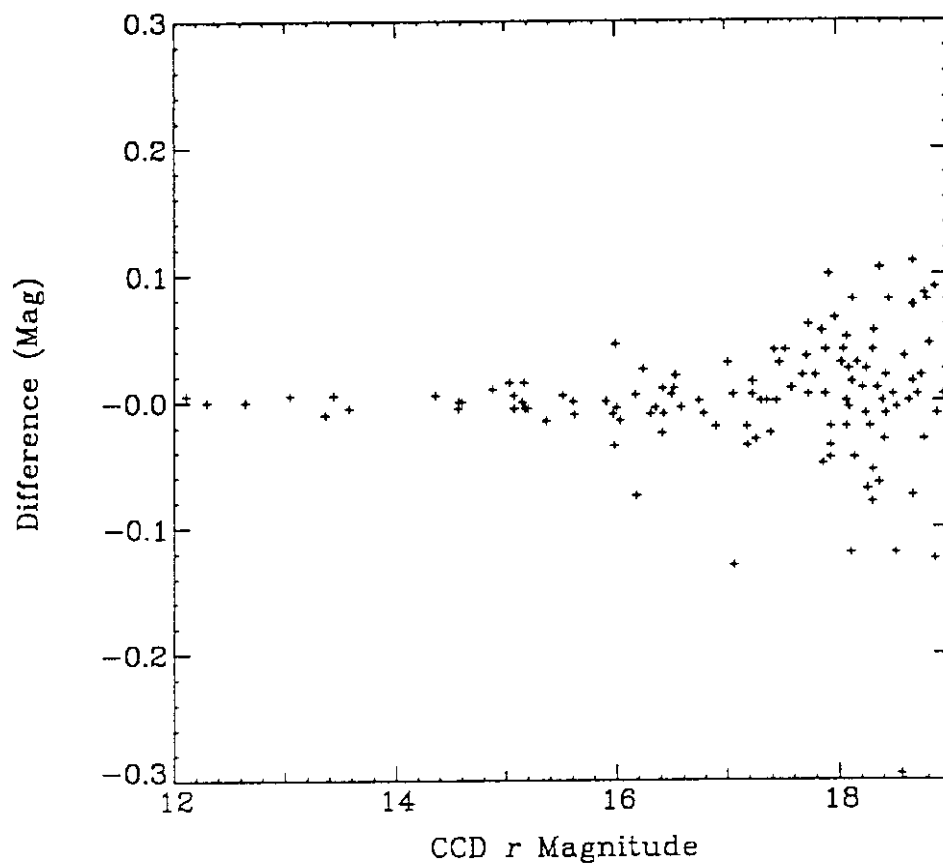
<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
691	14 37 48.06	29 36 34.0	17.02	12.4	751	14 53 35.49	29 32 24.6	16.50	15.8
692	14 37 52.30	29 29 58.2	17.75	8.4	752	14 53 43.99	29 34 19.8	16.04:	18.0
693	14 38 2.83	29 33 10.6	16.89	13.2	753	14 53 51.85	29 33 15.4	17.82	8.4
694	14 38 4.14	29 32 5.7	17.65	9.2	754	14 53 58.21	29 32 32.3	17.94:	8.0
695	14 38 29.39	29 37 28.5	15.75	37.4	755	14 54 16.92	29 35 18.7	17.45	10.4
696	14 38 59.99	29 32 37.8	17.22	11.2	756	14 54 22.91	29 35 37.6	15.64	33.2
697	14 39 11.66	29 33 51.9	16.76	13.6	757	14 55 29.28	29 26 40.8	16.51	15.2
698	14 39 15.95	29 35 33.1	17.93	8.0	758	14 56 1.81	29 30 29.0	17.45	9.6
699	14 39 27.78	29 28 48.3	16.00	19.0	759	14 56 51.64	29 27 23.7	17.04	12.0
700	14 39 47.49	29 30 35.3	16.61	14.4	760	14 56 52.63	29 26 49.2	17.08:	10.2
701	14 40 10.04	29 28 43.5	17.78	8.0	761	14 57 2.69	29 32 46.0	17.90	8.2
702	14 40 19.81	29 38 11.8	16.42:	15.6	762	14 57 4.31	29 33 55.5	17.68	8.8
703	14 40 30.45	29 33 27.8	15.45	24.6	763	14 57 8.61	29 32 13.4	17.97	8.0
704	14 40 38.04	29 36 56.7	17.89	8.4	764	14 57 16.07	29 26 59.3	17.09	12.0
705	14 41 47.22	29 30 49.5	17.64:	9.0	765	14 57 29.64	29 26 43.4	16.90	12.6
706	14 41 47.96	29 31 51.9	17.90:	7.8	766	14 57 41.40	29 27 33.4	17.26	10.8
707	14 41 48.63	29 31 56.9	17.29:	9.6	767	14 57 45.88	29 30 43.4	17.26	10.8
708	14 41 50.91	29 28 25.5	16.22:	15.8	768	14 58 25.36	29 36 28.8	16.63	15.2
709	14 41 56.73	29 32 32.0	17.93	7.8	769	14 58 37.81	29 34 48.6	17.08	12.0
710	14 42 23.71	29 34 54.5	17.53	9.8	770	14 58 37.95	29 36 38.7	17.32	11.0
711	14 42 49.21	29 29 57.5	17.57	9.4	771	14 58 41.02	29 31 0.4	17.83	8.2
712	14 42 53.29	29 32 22.3	16.02:	18.2	772	14 58 43.18	29 34 32.8	17.69:	9.2
713	14 43 3.57	29 38 6.4	16.29	16.8	773	14 58 44.03	29 28 16.8	17.71	8.6
714	14 43 10.52	29 31 21.6	17.32	10.8	774	14 58 45.06	29 26 31.4	16.77	13.2
715	14 43 18.72	29 34 55.0	16.13	18.0	775	14 58 53.38	29 34 26.5	17.36:	10.6
716	14 43 50.46	29 31 51.4	17.47	9.8	776	15 0 20.97	29 29 32.5	17.99	7.4
717	14 43 50.67	29 27 13.7	17.40	10.2	777	15 1 40.82	29 29 32.7	15.44	31.8
718	14 44 19.98	29 29 27.6	17.73	8.8	778	15 1 52.53	29 34 44.3	17.96	8.0
719	14 44 29.31	29 34 22.4	17.75	8.8	779	15 1 55.52	29 34 20.1	17.41	9.8
720	14 44 39.56	29 37 46.7	17.13	11.6	780	15 1 56.32	29 28 29.3	17.54	8.8
721	14 44 48.44	29 30 19.1	17.90:	8.0	781	15 2 8.69	29 26 1.6	17.48	9.6
722	14 44 58.40	29 32 50.5	17.03:	12.6	782	15 2 11.73	29 32 42.1	17.76	8.6
723	14 44 58.56	29 32 30.2	17.68:	9.0	783	15 2 14.03	29 26 58.8	16.75	13.4
724	14 45 21.07	29 35 40.6	17.73	9.0	784	15 2 22.99	29 33 47.2	17.55	9.8
725	14 45 46.08	29 31 51.5	16.43:	15.0	785	15 2 23.74	29 27 53.6	17.72	8.4
726	14 45 49.01	29 35 34.3	17.64	9.4	786	15 2 39.25	29 31 37.5	16.56	15.2
727	14 45 52.36	29 32 45.5	17.31	10.6	787	15 2 42.62	29 30 48.9	16.39:	15.2
728	14 46 7.89	29 37 20.1	17.86	8.4	788	15 2 59.98	29 28 20.0	17.55	9.2
729	14 46 50.21	29 33 34.0	17.47:	9.8	789	15 3 6.24	29 27 47.3	17.35	10.4
730	14 46 59.41	29 29 38.0	17.45	10.0	790	15 3 26.17	29 34 21.6	17.49	10.0
731	14 47 28.67	29 32 6.7	17.86:	8.0	791	15 3 27.18	29 27 33.4	15.54	26.0
732	14 47 39.87	29 35 43.8	17.95	8.0	792	15 3 52.99	29 26 51.2	16.51:	15.6
733	14 47 40.24	29 30 43.2	17.55	9.6	793	15 4 4.33	29 36 52.2	15.89	18.2
734	14 47 42.54	29 32 42.1	17.94	8.0	794	15 4 11.01	29 34 47.8	17.30	10.4
735	14 48 23.18	29 32 22.7	14.36	18.8	795	15 4 31.04	29 29 30.3	16.73:	14.0
736	14 50 2.46	29 36 22.9	15.89	15.8	796	15 4 34.95	29 27 53.9	17.56	9.0
737	14 50 14.97	29 31 4.1	17.00:	12.4	797	15 4 41.19	29 33 53.0	16.94	13.0
738	14 51 15.56	29 36 35.8	17.97	8.0	798	15 5 11.75	29 32 9.2	17.20	11.4
739	14 51 27.47	29 36 17.6	17.59:	9.6	799	15 5 16.08	29 28 30.7	17.81	8.4
740	14 51 28.50	29 34 35.4	17.30	10.8	800	15 6 6.59	29 27 19.0	17.47	9.6
741	14 51 33.16	29 26 49.7	17.31:	10.6	801	15 6 8.08	29 26 36.1	17.37	10.0
742	14 51 54.30	29 28 57.6	16.69:	15.8	802	15 6 22.76	29 34 1.8	17.36	10.6
743	14 51 56.30	29 29 19.4	17.62	9.2	803	15 6 25.97	29 37 27.4	17.09	12.0
744	14 51 57.72	29 35 27.1	17.75	8.6	804	15 6 27.51	29 28 51.7	16.43	16.0
745	14 52 2.71	29 27 59.7	17.40	10.0	805	15 6 34.29	29 30 16.7	17.68	9.0
746	14 52 24.98	29 34 58.0	17.25:	11.2	806	15 6 39.16	29 37 17.1	17.42	10.0
747	14 52 34.99	29 33 28.4	17.84	8.4	807	15 6 40.83	29 26 38.1	17.99	7.6
748	14 52 38.25	29 33 9.1	17.41	10.4	808	15 6 42.03	29 36 20.2	17.91	8.2
749	14 53 20.39	29 34 56.1	17.71	9.0	809	15 6 43.40	29 35 47.3	17.91	8.2
750	14 53 33.62	29 37 35.0	16.39:	16.2	810	15 6 45.00	29 31 18.3	17.85	8.4

<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
811	15 7 1.30	29 28 16.5	17.85	8.0	871	15 19 24.68	29 31 28.4	17.71	9.0
812	15 7 8.28	29 33 41.5	17.21	11.2	872	15 19 27.75	29 29 55.2	16.23:	17.0
813	15 7 12.10	29 36 50.7	17.42:	10.4	873	15 19 32.32	29 34 58.0	17.82	8.6
814	15 7 15.27	29 26 34.6	17.98	7.6	874	15 19 34.65	29 34 46.7	17.37	10.6
815	15 7 35.37	29 35 28.1	17.81	8.0	875	15 19 36.67	29 25 51.5	17.58:	9.2
816	15 7 35.40	29 35 29.2	17.81	8.6	876	15 19 40.26	29 28 33.6	17.53	9.6
817	15 7 35.52	29 36 9.9	15.64	28.8	877	15 19 42.80	29 28 18.4	17.61	9.2
818	15 8 0.28	29 28 7.1	17.28	10.6	878	15 20 2.89	29 27 2.2	17.16	11.2
819	15 8 9.50	29 29 44.4	17.85	8.4	879	15 20 12.34	29 35 58.5	17.83:	8.4
820	15 8 11.95	29 33 45.9	16.74	13.8	880	15 20 12.62	29 32 27.4	17.80	8.2
821	15 8 26.35	29 29 58.1	17.63	9.2	881	15 20 15.40	29 29 43.0	17.76	8.6
822	15 8 29.56	29 33 29.9	16.55	15.6	882	15 20 38.55	29 28 55.4	17.89	8.0
823	15 8 33.38	29 36 45.9	16.71	14.2	883	15 20 41.93	29 25 50.4	17.39	10.2
824	15 8 44.24	29 36 22.7	17.23	11.4	884	15 20 44.87	29 36 19.1	17.43	10.0
825	15 9 22.51	29 32 0.2	16.76	14.2	885	15 20 54.83	29 28 24.4	16.09	19.0
826	15 10 0.63	29 31 55.1	17.43	10.2	886	15 21 5.55	29 26 56.9	17.94	7.8
827	15 10 0.72	29 30 26.9	17.70	9.0	887	15 21 6.49	29 26 47.4	17.63	9.0
828	15 10 30.43	29 27 33.3	17.34	10.4	888	15 21 11.18	29 35 30.5	17.90	8.2
829	15 10 35.41	29 26 59.7	16.71	14.2	889	15 21 11.52	29 25 39.3	17.75	8.0
830	15 10 40.40	29 27 12.8	17.30	10.6	890	15 21 43.73	29 27 12.4	16.80	13.2
831	15 10 44.76	29 33 13.1	17.57	9.6	891	15 21 45.22	29 33 44.6	17.78	8.6
832	15 10 46.54	29 29 48.3	17.25	11.0	892	15 22 3.87	29 35 31.1	17.27	11.0
833	15 11 41.63	29 31 12.1	17.99	8.0	893	15 22 28.99	29 26 59.4	17.55	9.2
834	15 11 43.18	29 31 1.4	17.51	9.6	894	15 22 36.47	29 30 10.6	17.87	8.0
835	15 12 10.41	29 32 44.4	17.31	10.8	895	15 22 39.16	29 35 50.5	17.67	9.2
836	15 12 14.97	29 37 0.9	17.90	8.4	896	15 22 39.34	29 26 4.6	17.68	8.8
837	15 13 36.13	29 32 55.5	17.16	11.0	897	15 22 45.73	29 30 31.2	17.27	10.8
838	15 14 1.87	29 27 41.7	17.76	5.8	898	15 22 49.23	29 34 42.7	17.57	9.6
839	15 14 9.92	29 35 47.2	17.13	12.0	899	15 22 53.40	29 31 57.8	16.21	17.8
840	15 14 16.89	29 35 8.6	16.59	14.8	900	15 23 1.65	29 24 55.7	17.88	8.0
841	15 14 20.74	29 29 31.4	16.03:	20.4	901	15 23 18.06	29 35 58.4	16.24	17.8
842	15 14 36.36	29 29 2.1	16.19:	17.8	902	15 24 3.93	29 35 26.2	16.79	13.6
843	15 14 39.81	29 29 59.5	16.65	14.2	903	15 24 5.78	29 26 25.1	17.23	11.0
844	15 14 44.33	29 35 24.5	16.41:	16.6	904	15 24 7.49	29 36 17.8	17.10	11.8
845	15 14 46.77	29 36 3.2	17.13	5.8	905	15 24 16.53	29 26 44.0	16.92	12.6
846	15 14 46.89	29 36 13.3	15.41	26.0	906	15 24 23.11	29 32 53.7	16.47	16.0
847	15 14 48.27	29 36 20.2	17.01	12.6	907	15 24 30.72	29 30 49.0	16.14	30.2
848	15 14 49.11	29 32 51.1	17.63	9.4	908	15 24 37.70	29 33 45.8	15.05:	34.6
849	15 15 5.98	29 31 19.2	17.38	10.6	909	15 25 4.34	29 33 23.5	17.77	8.4
850	15 15 12.79	29 34 42.5	16.27	44.8	910	15 25 10.77	29 30 9.3	16.69	20.8
851	15 15 56.15	29 25 46.0	17.20	11.0	911	15 25 14.72	29 34 39.7	17.97	7.6
852	15 16 11.07	29 34 5.1	17.98	8.0	912	15 25 30.45	29 27 31.2	17.49	10.6
853	15 16 11.85	29 33 55.3	17.42	10.4	913	15 25 35.19	29 25 49.5	17.97	8.4
854	15 16 11.90	29 33 30.5	17.54	9.8	914	15 25 36.29	29 28 56.8	17.69	9.0
855	15 17 9.81	29 31 10.3	16.08:	17.6	915	15 25 42.53	29 27 25.8	17.62	9.2
856	15 17 15.22	29 32 54.1	16.84	13.4	916	15 25 44.93	29 35 32.6	17.90	8.4
857	15 17 19.80	29 32 3.8	17.07	11.4	917	15 25 52.49	29 30 39.1	15.45	31.8
858	15 17 40.43	29 29 42.3	17.88	8.2	918	15 26 0.77	29 32 7.2	17.54	9.8
859	15 17 58.69	29 31 20.8	17.33	10.8	919	15 26 2.54	29 31 54.4	17.00	12.6
860	15 18 14.66	29 29 17.8	16.80	13.8	920	15 26 5.81	29 24 40.2	16.42	15.0
861	15 18 24.72	29 34 26.1	17.78	8.8	921	15 26 21.95	29 26 15.2	16.26	17.6
862	15 18 39.15	29 25 40.3	17.43:	8.2	922	15 26 41.72	29 25 27.4	17.38	10.2
863	15 18 43.47	29 29 13.8	17.62	9.4	923	15 26 43.76	29 35 7.6	17.63	9.6
864	15 18 54.94	29 32 26.1	16.82	13.6	924	15 26 45.60	29 32 17.5	17.83	8.6
865	15 18 59.03	29 28 34.1	16.34	16.8	925	15 27 7.57	29 30 55.9	17.84	8.4
866	15 19 0.43	29 36 8.1	15.24	37.4	926	15 27 17.15	29 30 35.8	17.29	11.0
867	15 19 8.18	29 35 34.5	17.60	9.6	927	15 27 46.32	29 25 47.1	17.55	9.4
868	15 19 17.78	29 25 59.7	17.74	8.4	928	15 27 46.87	29 35 16.6	16.72	13.8
869	15 19 19.22	29 26 31.1	17.97	7.6	929	15 28 54.09	29 36 15.1	16.86	13.6
870	15 19 23.95	29 27 29.4	15.94	19.4	930	15 28 59.87	29 30 51.8	17.42	9.8

<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")	<i>ID</i>	<i>R.A.</i> ₍₁₉₅₀₎	<i>Decl.</i> ₍₁₉₅₀₎	<i>Mag.</i>	<i>Rad.</i> (")
931	15 29 2.93	29 31 46.8	17.91	8.2	993	16 22 29.33	29 31 19.7	17.18	11.6
932	15 29 27.67	29 29 54.5	15.87	20.8	994	16 23 14.73	29 30 30.0	17.76	8.8
933	15 29 30.82	29 29 23.8	17.19	11.6	995	16 23 25.31	29 31 4.2	15.63	17.4
934	15 29 42.78	29 29 34.0	16.55	15.0	996	16 23 35.92	29 23 44.6	17.52:	9.6
935	15 29 54.22	29 31 5.1	17.89	8.2	997	16 23 38.34	29 28 52.7	17.93	8.0
936	15 29 55.40	29 31 49.1	17.01	12.6	998	16 23 50.03	29 26 20.2	17.93	8.0
937	15 30 8.51	29 27 33.2	17.79	8.4	999	16 24 31.54	29 22 20.2	17.61	9.0
938	15 30 15.92	29 32 59.2	16.71	14.2	1000	16 24 53.01	29 29 50.0	17.33	10.6
939	15 30 22.59	29 28 10.1	17.55	9.2	1001	16 25 11.84	29 30 3.0	17.45:	9.6
940	15 30 26.90	29 30 39.6	17.36	10.6	1002	16 25 19.26	29 29 57.2	17.38	10.2
941	15 30 30.65	29 29 10.5	13.37:	13.2	1003	16 25 30.40	29 30 24.4	17.85	8.4
942	15 30 32.03	29 29 5.2	16.55:	13.6	1004	16 26 51.40	29 29 41.3	16.37	16.6
943	15 30 38.22	29 34 41.5	16.50	16.0	1005	16 27 13.10	29 32 13.9	17.13:	11.8
944	15 31 17.51	29 35 27.3	15.48	27.4	1006	16 27 14.12	29 30 50.5	17.98	8.0
945	15 31 22.81	29 24 39.5	17.72	8.4	1007	16 27 19.75	29 32 29.8	17.46:	14.4
946	15 31 25.06	29 26 12.6	17.75	8.4	1008	16 27 38.25	29 29 53.6	17.46	10.0
947	15 31 39.23	29 32 27.0	17.06	12.0	1009	16 27 51.49	29 30 29.9	17.72	9.0
948	15 31 40.80	29 30 29.3	16.28	17.6	1010	16 28 50.69	29 30 23.1	15.00	28.8
949	15 31 41.05	29 31 45.9	16.44:	15.6	1011	16 28 59.37	29 26 44.5	17.16	11.6
950	15 31 41.43	29 34 48.4	16.27	17.8	1012	16 32 3.00	29 33 13.2	16.29	17.4
951	15 31 49.81	29 25 38.2	17.58	9.2	1013	16 32 15.27	29 32 27.8	17.35	10.4
952	15 32 9.15	29 29 23.1	17.48	9.8	1014	16 32 43.81	29 24 41.9	17.86	8.0
953	15 32 18.16	29 34 31.7	17.04:	12.0	1015	16 32 53.05	29 32 55.6	16.83	13.2
954	15 32 30.11	29 33 52.0	17.54	9.6	1016	16 33 12.86	29 23 56.1	17.63	9.0
955	15 32 32.52	29 28 39.7	17.09:	11.4	1017	16 33 21.44	29 32 10.1	17.93	8.0
956	15 32 35.18	29 32 11.3	17.90	8.2	1018	16 33 54.89	29 32 28.4	16.49	15.8
957	15 32 35.22	29 31 25.0	17.93	8.0	1019	16 34 14.49	29 29 31.0	17.28	11.0
958	15 32 36.70	29 30 16.5	17.67	9.0	1020	16 34 15.45	29 22 2.9	16.37	16.8
959	15 32 41.33	29 28 59.5	16.46	15.2	1021	16 34 25.83	29 26 13.2	15.48	33.2
960	15 32 42.57	29 30 3.5	17.35	10.0	1022	16 34 27.49	29 26 10.3	15.83	21.2
961	15 32 43.46	29 27 12.6	17.33	10.2	1023	16 34 27.65	29 25 44.3	15.96:	17.8
962	15 34 12.35	29 25 16.4	16.61	14.6	1024	16 34 32.25	29 31 37.9	17.35:	10.6
963	15 34 23.72	29 29 37.0	17.51	10.0	1025	16 34 32.80	29 31 27.1	16.32	15.2
964	15 35 1.01	29 30 15.1	15.45:	36.0	1026	16 34 33.71	29 24 1.6	17.87	7.8
965	15 35 2.29	29 30 0.6	15.13:	30.2	1027	16 34 33.75	29 31 49.3	17.06	12.2
966	15 35 17.31	29 33 47.0	17.80	8.6	1028	16 34 34.40	29 25 34.6	17.97	7.8
967	15 35 36.54	29 24 44.0	16.83	13.4	1029	16 34 45.33	29 29 13.1	16.05:	13.2
968	15 36 4.93	29 29 18.7	17.80	8.6	1030	16 35 3.02	29 30 42.5	17.37	10.6
969	15 36 32.55	29 34 42.5	17.83	8.4	1031	16 35 3.60	29 29 15.3	16.23	17.8
970	15 36 40.53	29 34 31.0	15.49	41.8	1032	16 35 41.26	29 32 22.3	17.37	10.6
971	15 36 47.41	29 35 6.0	15.55	30.2	1033	16 35 41.56	29 22 25.3	17.58:	9.2
972	15 36 56.64	29 33 57.8	16.27	17.8	1034	16 35 42.73	29 28 17.8	16.36	16.8
973	15 39 12.88	29 31 38.8	17.16	11.6	1035	16 36 6.84	29 23 55.2	16.80	13.6
974	15 39 53.25	29 24 18.0	16.22	17.2	1036	16 36 10.33	29 24 0.1	16.71:	13.6
975	15 41 40.65	29 26 35.5	15.15:	20.8	1037	16 36 11.28	29 24 18.9	17.13:	11.2
976	15 41 42.46	29 35 8.8	15.16	28.8	1038	16 36 13.71	29 24 5.9	17.56	9.6
977	15 42 2.52	29 32 35.0	17.72	8.8	1039	16 36 45.96	29 28 4.4	17.35	10.8
978	15 42 45.00	29 25 22.0	15.05	27.4	1040	16 36 47.23	29 25 19.5	17.47	9.8
979	16 15 41.36	29 28 40.4	17.61	9.4	1041	16 37 23.16	29 27 55.0	17.00	12.4
980	16 15 47.46	29 28 57.7	17.69	9.0	1042	16 37 24.20	29 30 5.4	17.35	10.8
981	16 16 24.65	29 27 56.2	17.25	10.6	1043	16 37 39.74	29 26 7.3	16.59	15.2
982	16 16 44.42	29 33 34.4	17.98	8.0	1044	16 39 11.55	29 32 15.7	17.38	10.6
983	16 16 47.93	29 22 42.6	17.92	7.8	1045	16 39 17.18	29 28 41.5	17.63	9.4
984	16 17 11.83	29 30 16.7	17.69	9.0	1046	16 39 40.89	29 26 10.8	17.68	9.0
985	16 17 42.33	29 29 45.9	17.91	8.2	1047	16 40 38.74	29 31 37.8	17.97	8.0
986	16 17 47.44	29 30 20.8	17.49:	9.8	1048	16 41 1.42	29 27 40.9	16.91	13.2
987	16 19 32.80	29 29 4.8	16.97:	12.2	1049	16 41 26.15	29 23 47.2	17.60	9.2
988	16 19 35.03	29 24 1.6	17.10	11.6	1050	16 41 29.76	29 24 24.8	17.56	9.0
989	16 19 56.67	29 29 3.5	16.57	15.0	1051	16 42 9.43	29 31 18.5	17.68	9.2
990	16 20 19.11	29 29 56.6	17.25	11.2	1052	16 42 11.88	29 23 29.0	17.81	8.4
991	16 20 45.33	29 31 20.8	17.83	8.4	1053	16 42 12.57	29 22 11.3	16.85	12.6
992	16 21 53.85	29 32 19.4	15.76:	20.2	1054	16 42 20.10	29 30 35.9	17.02	12.6







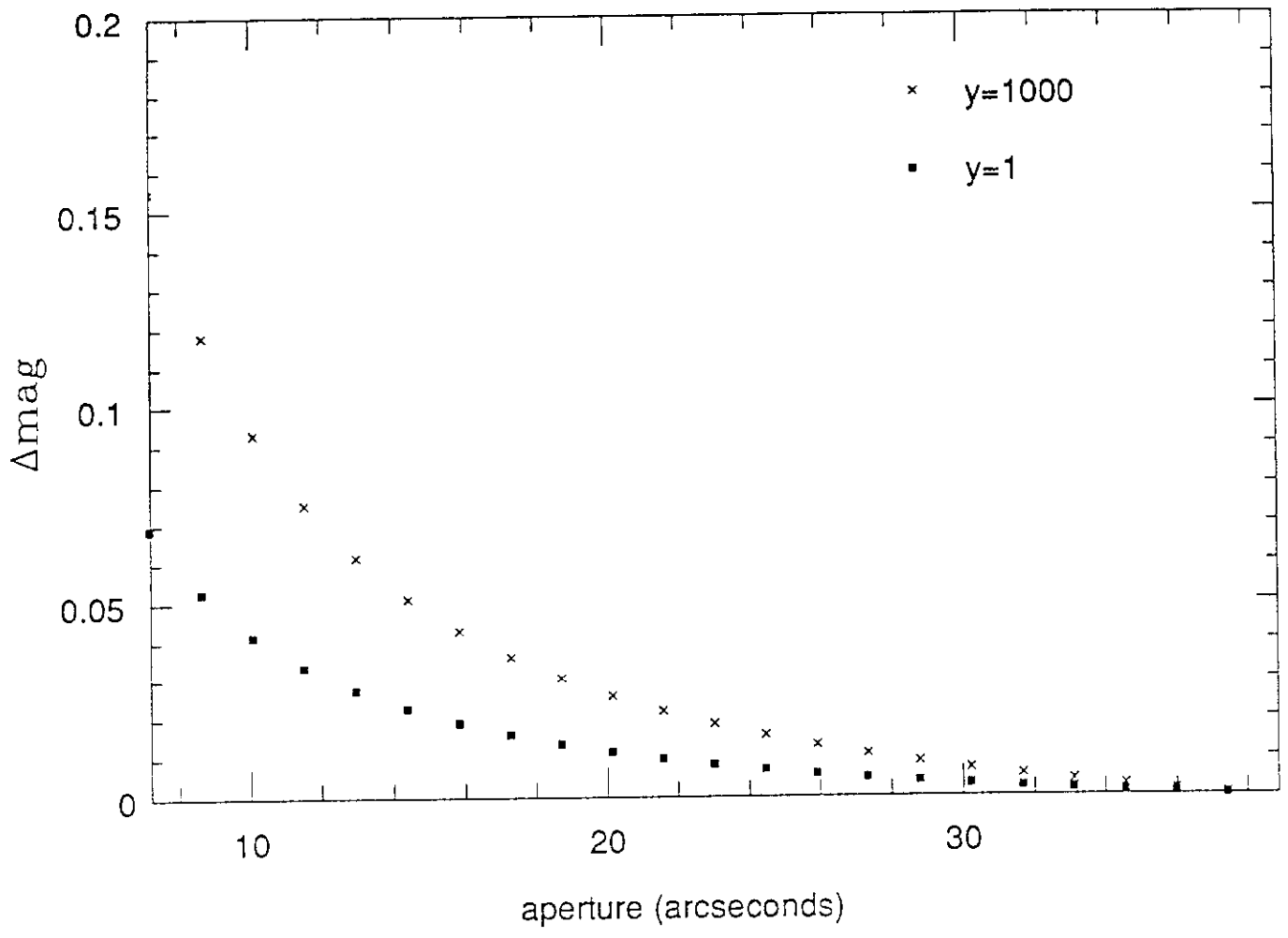


Figure 5

