

Some Notes on Sparse Correctors

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Look at having sparse corrector layout:

- Better packing fraction
- Shorter cable runs to correctors
- Fewer interfaces to power, cryo system

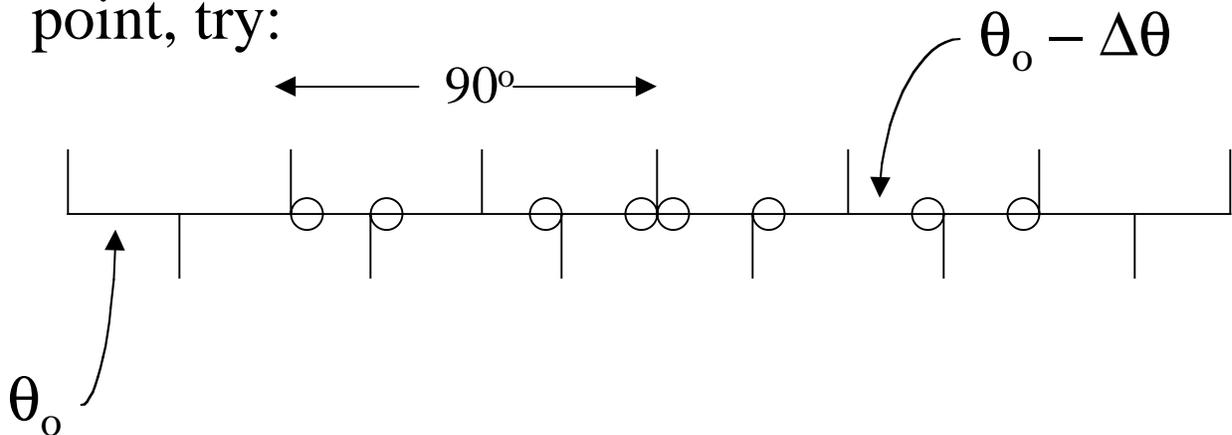
For now, study steering, tune, and chromaticity corrections ...

Issues:

- Corrector strengths
- Lattice perturbations
- Allowable orbit distortions
- Dynamic Aperture (sextupoles)

Correction Region

Near each access
point, try:

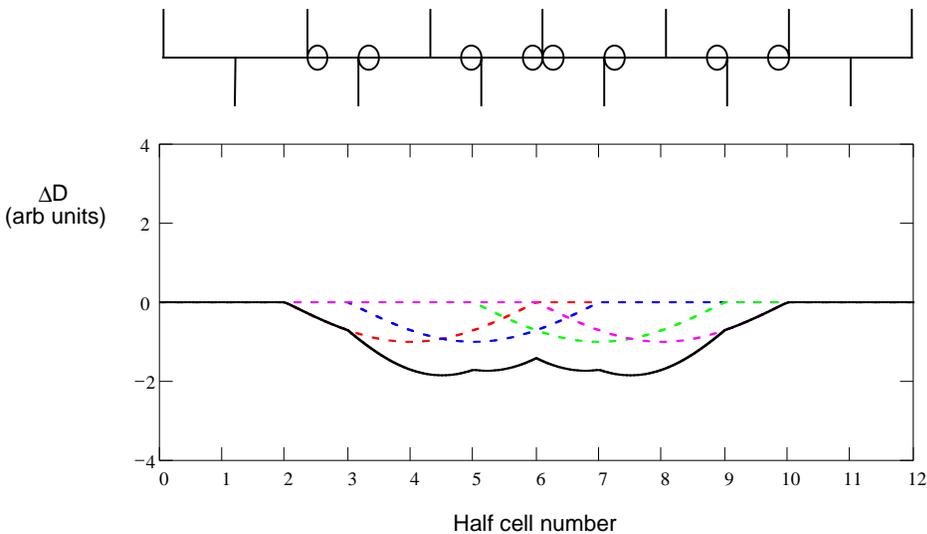


○ = “short” or
“missing” magnet

As a numerical example,
take SSC numbers:

- $L_{\text{sec}} \approx 4 \text{ km}$
- $L = 90 \text{ m}, \mu = 90^\circ$
 - $D_{\text{max}} = (243 \text{ m})\theta_0$
 - $D_{\text{min}} = (116 \text{ m})\theta_0$
- Take $\Delta\theta/\theta_0 = 1/5$
(1/5 dipoles per half cell)
 \Rightarrow *Then....*

Disturbance of Dispersion Function:



| <u>Location</u> | <u>$\Delta D/D_0$</u> |
|-----------------|----------------------------------|
|-----------------|----------------------------------|

| | |
|---|---|
| 2 | 0 |
|---|---|

| | |
|---|-----|
| 3 | -16 |
|---|-----|

| | |
|---|------|
| 5 | -25% |
|---|------|

| | |
|---|------|
| 6 | -15% |
|---|------|

| | |
|---|------|
| 7 | -25% |
|---|------|

| | |
|---|------|
| 9 | -16% |
|---|------|

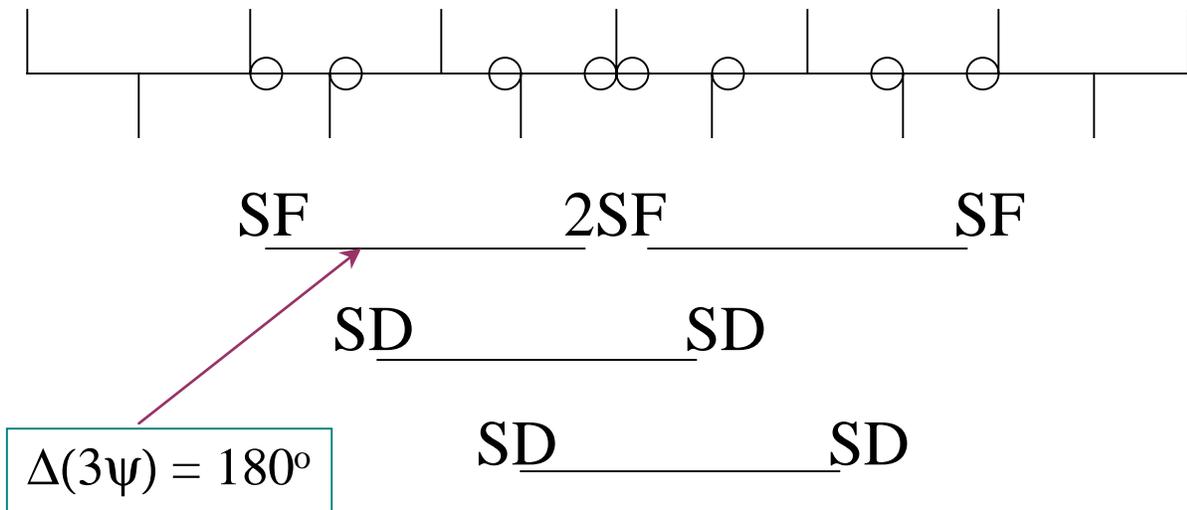
| | |
|----|---|
| 10 | 0 |
|----|---|

$$\Delta\theta/\theta_0 = 1/5$$

(in SSC, 15 m)

So, chromaticity correctors will need to be stronger by appropriate amounts...

Chromaticity Correction



In one “sector” (SSC),

≈ 44 half-cells

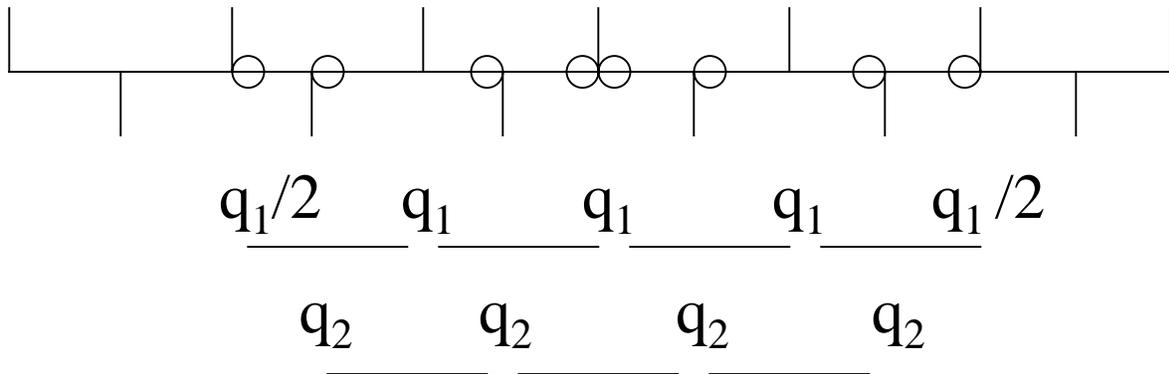
$\Rightarrow 22 \beta_{\max}$ locations

\therefore need $(22/4)*1.15 = 6X$ stronger F sextupoles,
and $(22/4)*1.25 = 7X$ stronger D sextupoles

SSC Specs: F sext: 0.15 T-m (≈ 0.6 m)
(@1 cm) D sext: 0.25 T-m (≈ 1 m)

Need about 6-7 m at D locations

Tune Adjustment



adjust strength of q @ β_1 , disturbs β downstream ...

$$\frac{\Delta\beta}{\beta}(s) = -(q\beta_1)\sin(2\psi_0) + \frac{1}{2}(q\beta_1)^2(1 - \cos(2\psi_0))$$

\therefore with 90° cells, $\Delta\beta/\beta$ remains \approx local

estimate: $\Delta v \approx (1/4\pi)(\beta/F)N\delta$

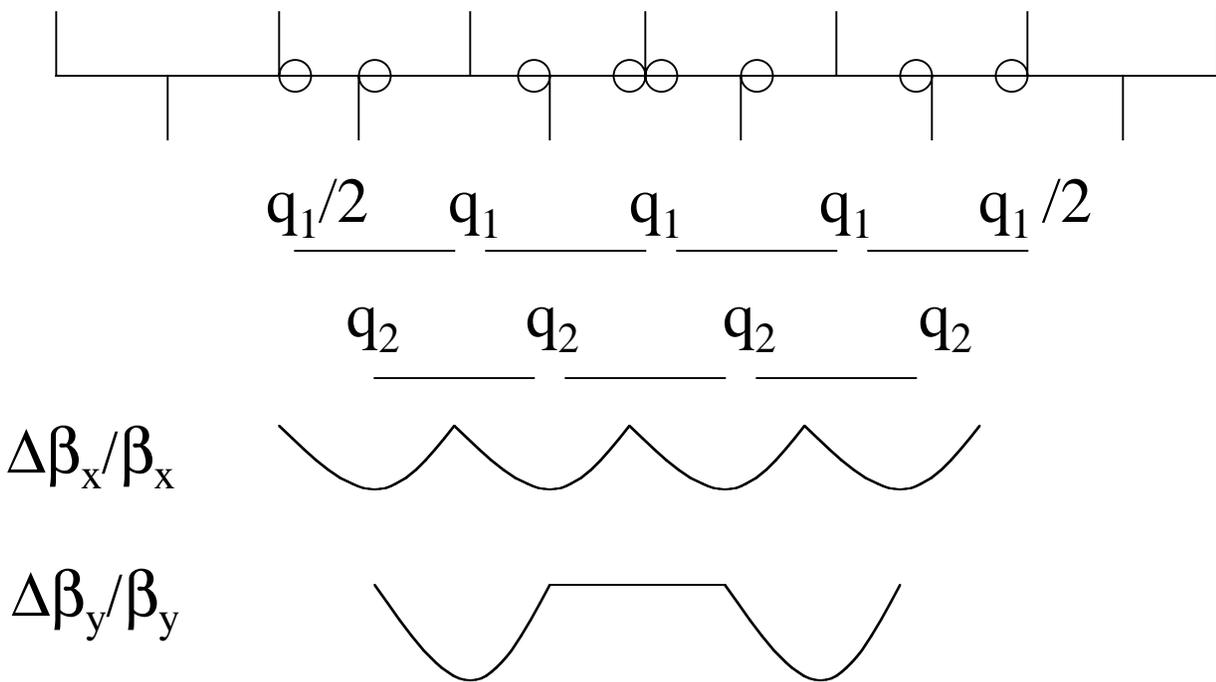
$$2 \approx (1/4\pi)(350\text{m}/64\text{m})(20*4)\delta$$

% of $(1/F)$

$$\Rightarrow \delta = 0.06$$

\therefore local $(\Delta\beta/\beta)_{\text{max}} \approx -(0.06/2)(350/64) = 15\%$

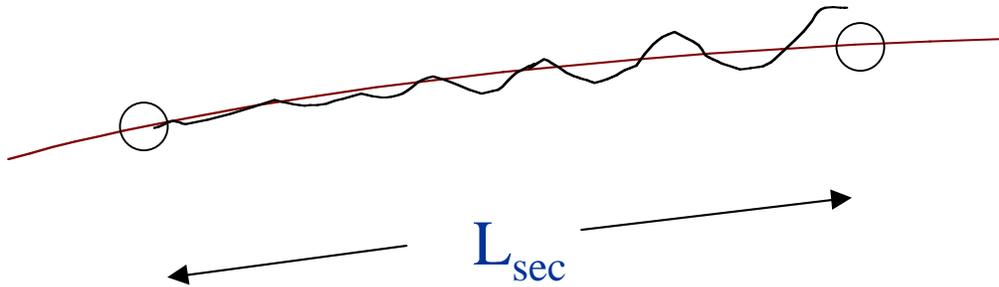
Tune Adjustment (cont'd)



$\therefore (\Delta\beta_y/\beta_y)_{\max} \approx 30\%$, with these
maxima located at the F quads

- in reality, F/D corrections *interlaced*,
 \therefore perturbations are coupled
- effects dispersion function
- above, used $\Delta\nu = 2$ units; may not be this large
- note: at SSC, tune quads had $\delta = 0.06$ (design)

Steering



for quad displacement d , $\Delta\theta = d/F$
 so, at n -th quad,

$$\Delta x_n = \sum_i \theta_i \sqrt{\beta_i \beta_n} \sin \psi_{i \rightarrow n}$$

$$\langle \Delta x_n^2 \rangle = \theta_{rms}^2 \beta_n \langle \beta \sin^2 \psi_{i \rightarrow n} \rangle n$$

$$\Rightarrow \Delta x_n^{rms} = \theta_{rms} \sqrt{\langle \beta \rangle \beta_n} \sqrt{n/2}$$

So:

$$\Delta x_n^{rms} = \frac{2d_{rms}}{L} \sin \frac{\mu}{2} \sqrt{\langle \beta \rangle \beta_n} \sqrt{n/2}$$

Steering (cont'd)

note: $\beta \propto L$, so Δx_n^{rms} independent of L

BUT,

if $n = L_{\text{sec}} / L$, where L_{sec} is predetermined,

$$\text{then } \Delta x_n^{\text{rms}} \propto 1/L^{1/2}$$

note also: d_{rms} is likely a function of L
(quads further apart, harder to align)

SSC-type numbers:

$$\begin{aligned}\Delta x_n^{\text{rms}} &= \frac{2\left(\frac{1}{4} \text{ mm}\right) \frac{\sqrt{2}}{2}}{90 \text{ m}} \sqrt{(200 \text{ m})(350 \text{ m})} \sqrt{40/2} \\ &= 4.6 \text{ mm}\end{aligned}$$

\therefore could expect $\Delta x_{\text{max}} \approx 15 \text{ mm}$

Steering (cont'd)

$$\begin{aligned}\text{rms corrector strength} &\approx \Delta x^{\text{rms}}/\beta_{\text{max}} \\ &\approx (4.6 \text{ mm})/(350 \text{ m}) \\ &\approx 13 \mu\text{rad}\end{aligned}$$

$$\therefore \text{max strength} \approx 40 \mu\text{rad}$$

For SSC numbers,

$$\begin{aligned}\Rightarrow B*L &= (10/3)(20,000)(40 \cdot 10^{-6}) \text{ T-m} \\ &= 2.7 \text{ T-m}\end{aligned}$$

(3 T over 1 m, say)

note: if “steer” @ each quad location,
would have...

$$\begin{aligned}\Delta\theta^{\text{rms}} &\approx d_{\text{rms}}/F \approx (0.25 \text{ mm})/(64 \text{ m}) \\ &\approx 4 \mu\text{rad}\end{aligned}$$

$$\therefore \theta_{\text{max}} \approx 12 \mu\text{rad}, B*L \approx 1\text{T-m}$$

(for local correction)

Next Steps...

- Shorten / Optimize module
 - * change half-cell length?
 - * abandon FODO?
 - * ???
- Practical range of tune adjustment
 - * beta-beat
 - * effect on chromaticity correction
- Range of steering corrections
 - * use of various steering algorithms
 - * tolerable residual orbits
- Dynamic Aperture with sparse chromaticity correction
- Effect on phases *between* modules