

Short Sample Test Data III

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Recent wires which have been short sampled include Fermilab -11 cables, single strands of MCA wire Billet #239 and cabled wires made from these strands, a 36 strand square MCA cable, a French cable, a Brookhaven braid, a Furukawa solid, and solders.

A few comments about the following tables.  $J_c$  is current density in superconductor only.  $I_{eff}$  is current density in rectangular envelope including copper, superconductor, solder and any air pockets.

I. Equipment Change

There have been no procedural changes in recent short sample tests, but major equipment changes have been made. A Transrex 500-5 power supply, which give 5000 amp at maximum, is now used to supply current to the samples instead of using two H.P. 6463's in parallel. An automatic Helium level control was installed as well as additional temperature sensors, another liquid level probe, and a field detector. We are also now hooked into the Helium recovery system when it works.

## II. Fermilab 11 Strand Wire

Five samples of Fermilab 11 were tested. These are cables made of IGC 25 mil strands, and made into cables at the University of Wisconsin. Their results are shown in Table I. The samples are one without solder, two soldered ones, one keystoneed, and a broken one. The first sample had no solder, only 11 wires loosely twisted together. This sample showed lower quench currents than others as expected but same  $J_c$  at  $10^{-12} \Omega \text{cm}$  and less current shaving than the others. Two soldered samples were tested - one bifilar wound and the other hairpin and the results were practically identical. A sample was keystoneed, then tested, and gave the same results.

This wire shows an improvement over the Supercon 11 strand, but it is somewhat worse than MCA 11 strand. See Table I and Figure 1. The final sample had a broken strand, but there was about two inches overlap. The quench current was lowered by only 3~4%.

## III. Series of MCA Single Strands

We tested two series of single strand MCA samples. All the wires in a given series had the same treatment until the final drawing, but the heat treatments of the two series were different. The first consisted of #8 - #12, were .037", .030", .025", .020", and .015" in diameter and had the long heat treatment during drawing process at .114". The second consisted of #13 - #16, were

.030", .025", .020", and .015" in diameter, and had the long heat treatment at .078".

A plot of cross section vs current at 50 KG and at  $5 \times 10^{-13} \Omega \text{cm}$  gives a straight line for each series.  $I_{\text{eff}}$  is also indicated on the plot. The number with parenthesis is  $I_{\text{eff}}$  if each wire were enclosed in a square area and without is  $I_{\text{eff}}$  for the strand as is. The resistance of copper was about  $1.8 \sim 1.9 \times 10^{-6} \Omega \text{cm}$ . It looks like good wire. See Table II and Figures 2 and 3.

#### IV. MCA 7 Strand and 11 Strand Wires

Six 75 x 150 samples, made from previous MCA .037" strands were tested. They were an unsoldered, a soldered, two turksheaded and two keystoneed ones. The results are summarized in Table III and in Figure 4.

The final keystoneed form carried the same current as 7 times one strand. However, turksheaded samples before keystoneing carried from 400 to 600 amps more. This change in critical current values may be due to cold working of turksheading and keystoneing, or they may have come from different ends of a spool. A keystoneed sample was tested, resoldered, then tested again with no change in the critical current. A turksheaded sample had all measurements repeated and all results were the same.

The 11 strand 50 x 150 wire, made from 25 mil diameter strands, was tested using an unsoldered and a soldered sample. The results are shown in Table IV. The soldered one carries 60 amps more than 11 x current in a single strand. The unsoldered one carries 10% more. They may have come from different ends of a spool. We have not tested a keystoneed sample yet.

The design current at 50 KG for the seven strand wire is 3500 amps while the keystoneed samples tested had only 3270 amps. The 11 strand sample with a current of 2390 amps at 50 KG is about 60 amps over specification. Although the seven strand sample, after keystoneing at Fermilab, does not meet design, both MCA cables are probably the best wires tested so far.

#### V. Other Wires

The results of miscellaneous cables are listed in Table V. The square MCA cable (HI conductor) is 91 mils x 91 mils, has 36 strands with superconductor and a center strand which is all copper, and has Cu:S.C. ratio of 1.8:1.

$I_{\text{eff}}$  at 50 KG at  $10^{-12} \Omega \text{cm}$  is 50 kA/cm<sup>2</sup>. This MCA square cable seems good and might be worth looking into.

The French wire was received without any information at all. Six strands containing superconductor were twisted around a center all copper strand. Six of these small

cables were twisted together and shaped into a rectangle to form the final cable. No solder was used. Microscopic examination revealed 37,620 superconductor filament each approximately  $11\mu$  diameter. Therefore  $J_c$  is only an estimate. If the diameter is  $10\mu$  or  $12\mu$   $J_c$  would change by 15%. Although the sample has a high critical current, 4440 amps of 50 KG, the cross section is large and  $J_c$  and  $I_{eff}$  do not compare with other samples tested.

The result of the short sample test on the Furukawa solid wire Type D is a low critical current. This wire has 33,000  $7.3\mu$  filaments and CuNi sheaths. The cross sectional area of superconductor in the Furukawa is within 2% that of MCA 7 strand cable. However, the critical current,  $J_c$  and  $I_{eff}$  are all about half that of MCA 7 strand cable. The amount of current sharing is much greater than for MCA and Fermilab cables.

The final wire we have tested recently is a sample of Brookhaven braid, approximate dimensions of .8" x .030". We were told there were 186 strands each with 361 filaments  $12\mu$  in diameter. Microscopic examination revealed the filament diameter to be  $\sim 7\mu$ . This corresponded with calculations based on Cu:S.C. ratio of 1.25:1. Therefore  $J_c$  was calculated based on a filament diameter of  $7.1\mu$ . The critical current for the Brookhaven braid is higher than that of the MCA cables, but  $J_c$  is only  $3/4$  as much and due to braid structure  $I_{eff}$  is  $1/2$ .

VI. Superconductivity of Solders

In addition to testing the wires, we have run resistance measurements and short sample tests on Koester 50/50 and 60/40 solders to estimate their effect on the resistance measurement of superconducting wire.

For both types of solder the resistance goes to zero at approximately 6.5°K. The resistance curves are shown in Figure 6. The resistivity at different temperatures are shown below.

	Room Temp (300°K)	12°K	7.5°K	6.5°K	$P_{300}/P_1$
50/50 Solder	$14.1 \times 10^{-6}$	$2.6 \times 10^{-7}$	$2.3 \times 10^{-7}$	$2.9 \times 10^{-8}$	54
60/40 Solder	$14.2 \times 10^{-6}$	$5.3 \times 10^{-7}$	$4.9 \times 10^{-7}$	$4.8 \times 10^{-7}$	27

The resistivity of 60/40 solder at 12°K is about 14 times that of copper with resistivity ratio  $P_{300}/P_{12} = 50$ . If we assume there is 20% 60/40 solder in the cross section of wire, it will affect the resistivity ratio of copper by 4%.

The short sample test data is shown in Figure 5. At zero current 50/50 solder becomes superconducting below 0.6kG, while 60/40 solder below 0.5 kG. At zero field 50/50 solder has a current density of 10kA/cm<sup>2</sup>, while 60/40 has 9 kA/cm<sup>2</sup>. The resistivities of these solders are respectively about 2 and 4 x 10<sup>-7</sup>Ωcm above transition field. These resistivities were measured by short sample test method, increasing magnetic field beyond the transition field.

		at 50 KG					
		40KG	50KG	60KG	Resistivity at Quench	$J_c$ (KH/cm <sup>2</sup> )	$I_{eff}$ (KH/cm <sup>2</sup> )
Unsoldered (bifiliar) Jan 21	Quench		2030	1650		192	42
	$2 \times 10^{-12}$		-	-		-	-
	$10^{-12}$		2020	1630	$1.3 \times 10^{-12}$	191	41
	$5 \times 10^{-13}$		1920	1550		181	39
Soldered (bifiliar) Jan 21	Quench		2110	1700		199	43
	$2 \times 10^{-12}$		2040	1650	$5 \times 10^{-12}$	192	42
	$10^{-12}$		1970	1620		186	40
	$5 \times 10^{-13}$		1830	1540		173	37
Soldered (hairpin) Jan 22	Quench		2120	1710		200	43
	$2 \times 10^{-12}$		2050	1700	$5 \times 10^{-12}$	193	42
	$10^{-12}$		1930	1630		181	39.5
	$5 \times 10^{-13}$		1830	1550		173	37
Soldered (hairpin broken strand) Feb 7	Quench	2540	2060	1680		194	42
	$2 \times 10^{-12}$	2510	2040	1650	$3 \times 10^{-12}$	192	42
	$10^{-12}$	2320	1840	1530		174	37.6
	$5 \times 10^{-13}$	2040	1610	1370		152	33
Keystoned (hairpin) Feb 5	Quench	2630	2150	1740		203	44
	$2 \times 10^{-12}$	2620	2130	1720	$3 \times 10^{-12}$	201	44
	$10^{-12}$	2560	2000	1630		189	41
	$5 \times 10^{-13}$	2410	1850	1490		174	38
11 x IGC Value for Single Strand	Quench		2180	1740	$3 \times 10^{-11}$	206	45

TABLE I Fermilab 11 Strand Wire (made from IGC strands)

Billet #239	dia. (")	$\frac{P_{300}}{P_{12}}$		at 50 KG						
				30	40	50	60	$J_c$ (KA/cm <sup>2</sup> )	$I_{eff}$ (KA/cm <sup>2</sup> ) Strand	$I_{eff}$ (KA/cm <sup>7</sup> ) Square
#8	.037	71	Quench $5 \times 10^{-13}$	728	581	472	381	191	68	53
						462		187	67	53
#9	.030	71	Quench $5 \times 10^{-13}$	475	379	310	252	190	68	53
				463	374	303	246	186	66	52
#10	.025		Quench $5 \times 10^{-13}$		261	214	174	189	68	53
					258	212	170	187	67	53
#11	.020	62	Quench $5 \times 10^{-13}$	213	173	144	117	199	71	56
				202	163	133	107	184	66	52
#12	.015	54	Quench $5 \times 10^{-13}$	110	92	76	62	186	67	53
				110	92	75	60	184	66	52
#13	.030	87	Quench $5 \times 10^{-13}$	435	348	285	230	175	63	49
				433	341	279	226	171	61	48
#14	.025	68	Quench $5 \times 10^{-13}$	296	241	196	162	173	62	49
				296	241	192	160	170	61	48
#15	.020	62	Quench $5 \times 10^{-13}$	195	160	132	108	182	65	51
				191	157	127	104	175	63	49
#16	.015	112(?)	Quench $5 \times 10^{-13}$	118	97	81	67	199	71	56
				103	83	67	56	165	59	46
Billet #240	.037	73	Quench $5 \times 10^{-13}$	698	558	451	363	182	65	51

TABLE II Series of MCA Single Strands

		at 50 KG						
	$\frac{P_{300}}{P_{10}}$		40KG	50KG	60KG	P at Quench	$J_c$ (KA/cm <sup>2</sup> )	$I_{eff}$ (KA/cm <sup>2</sup> )
Unsoldered	50	Quench	4170	3440	2770		198	43
80 x 155		$2 \times 10^{-12}$	3860	2910	2340	$10^{-11}$	168	36
March 5		$10^{-12}$	3600	2550	2170		147	32
		$5 \times 10^{-13}$	<u>3370</u>	<u>2320</u>	1920		<u>134</u>	<u>29</u>
Soldered	52	Quench	4080	3390	2800		196	41
85 x 150		$2 \times 10^{-12}$	4080	3370	2780	$2 \times 10^{-12}$	194	41
March 5		$10^{-12}$	4010	3260	2720		188	40
		$5 \times 10^{-13}$	3860	<u>3120</u>	2640		<u>180</u>	<u>38</u>
Turksheaded I	51	Quench	4460	3760	3220		217	53
75 x 147		$2 \times 10^{-12}$	4460	3760	3190	$2 \times 10^{-12}$	217	53
March 5		$10^{-12}$	4370	3670	3120		212	52
		$5 \times 10^{-13}$	4290	<u>3570</u>	3020		<u>206</u>	<u>50</u>
Turksheaded II	48	Quench	4690	3970	3390		229	56
March 11		$2 \times 10^{-12}$	4670	3940	3370	$3 \times 10^{-12}$	228	55
		$10^{-12}$	4580	3860	3280		223	54
		$5 \times 10^{-13}$	4490	<u>3760</u>	3180		<u>217</u>	<u>53</u>
Keystoned I	46	Quench	4050	3390	2790		196	49
75 x 155		$2 \times 10^{-12}$	4030	3340	2750	$3 \times 10^{-12}$	193	48
63.6 x 155		$10^{-12}$	3930	3260	2660		188	47
Start of keystoneing		$5 \times 10^{-13}$	3800	<u>3180</u>	2580		<u>184</u>	<u>46</u>
March 7								
Keystoned II	44	Quench	4060	3390	2820		196	49
Start C-3-10		$2 \times 10^{-12}$	4060	3370	2780	$2 \times 10^{-12}$	194	49
Inner		$10^{-12}$	4010	3270	2720		189	47
		$5 \times 10^{-13}$	3860	<u>3140</u>	2640		<u>181</u>	<u>45</u>

TABLE III MCA 7 (37 mil strands Billet #239)

	$\frac{P_{300}}{P_{10}}$		40KG	50KG	60KG	P at Quench	$J_c$ (KA/cm <sup>7</sup> )	$I_{eff}$ (KA/cm <sup>2</sup> )
Unsoldered	45	Quench	3460	2960	2540		237	61
March 7		$2 \times 10^{-12}$	3370	2830	2420	$4 \times 10^{-12}$	227	59
50 x 149		$10^{-12}$	3260	2670	2340		215	56
$4.806 \times 10^{-2} \text{cm}^2$		$5 \times 10^{-13}$	3060	2480	2240		199	52
Soldered	46	Quench	2920	2450	2050		197	52
March 12		$2 \times 10^{-12}$		2450	2050	$2 \times 10^{-12}$	197	52
49 x 148		$10^{-12}$	2910	2390	1990		192	51
$4.679 \times 10^{-2} \text{cm}^2$		$5 \times 10^{-13}$	2850	2290	1900		184	49

TABLE IV MCA 11 (25 mil strands)

	$\frac{P_{300}}{P_{10}}$		40KG	50KG	60KG	Resistivity at Quench	$J_c$ (KA/cm <sup>2</sup> )	$I_{eff}$ (KA/cm <sup>7</sup> )
French L Feb 5 .107 x .188	185	Quench		5210	4350		146	40
		$2 \times 10^{-12}$		4540	3680	$4 \times 10^{-11}$	127	35
		<u><math>10^{-12}</math></u>		<u>4440</u>	<u>3570</u>		<u>124</u>	<u>34</u>
Brookhaven Feb 6 .031 x .790	19	Quench	5020	4160	3270		155	25
		$2 \times 10^{-12}$	-	3950	3070	$10^{-11}$	147	25
		$10^{-12}$	-	3730	2920		139	24
		<u><math>5 \times 10^{-13}</math></u>	4720	<u>3420</u>	2670		<u>128</u>	<u>22</u>
MCA HI (Sq. Cable) Feb 7 .091 x .091	71	Quench	3530	3010	2520		205	57
		$2 \times 10^{-12}$	3530	2990	2510	$2 \times 10^{-12}$	203	56
		$10^{-12}$	3200	2630	2220		179	50
		<u><math>5 \times 10^{-13}</math></u>	2820	<u>2340</u>	2000		<u>159</u>	<u>44</u>
Furukawa Solid, Type D March 6 .074 x .147	52	Quench	2380	1990	1670		116	30
		$2 \times 10^{-12}$	1930	1660	1350	$5 \times 10^{-11}$	97	25
		<u><math>10^{-12}</math></u>	1830	<u>1610</u>	1300		<u>94</u>	<u>24</u>

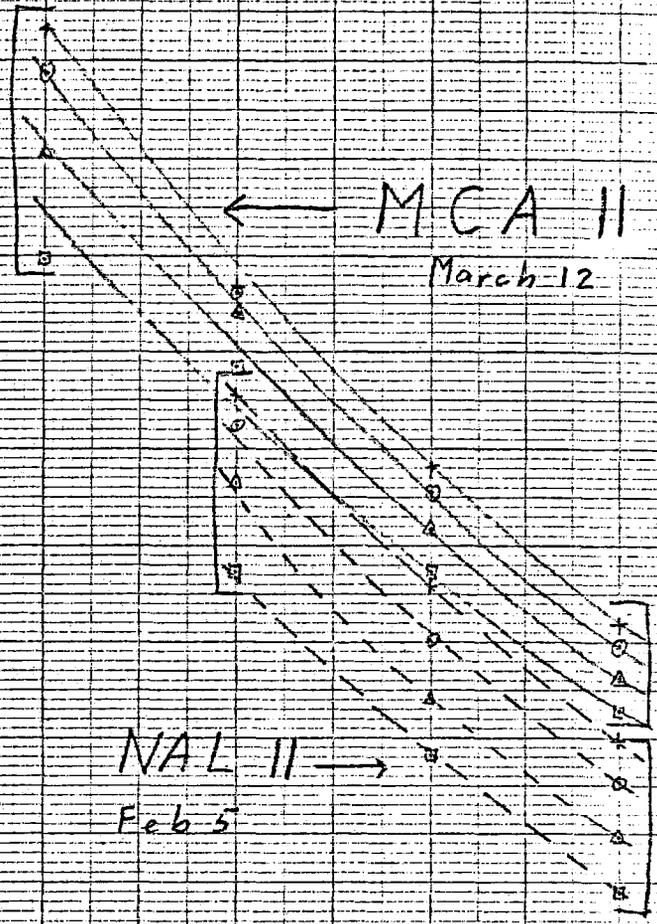
TABLE V MISCELLANEOUS WIRES

Current  
In sample  
(Amps)

3000

2000

1000



Quench  
 ○  $10^{-12}$   $\mu$ cm  
 △  $5 \times 10^{-13}$   $\mu$ cm  
 □  $2 \times 10^{-13}$   $\mu$ cm

Fig. 1

10

20

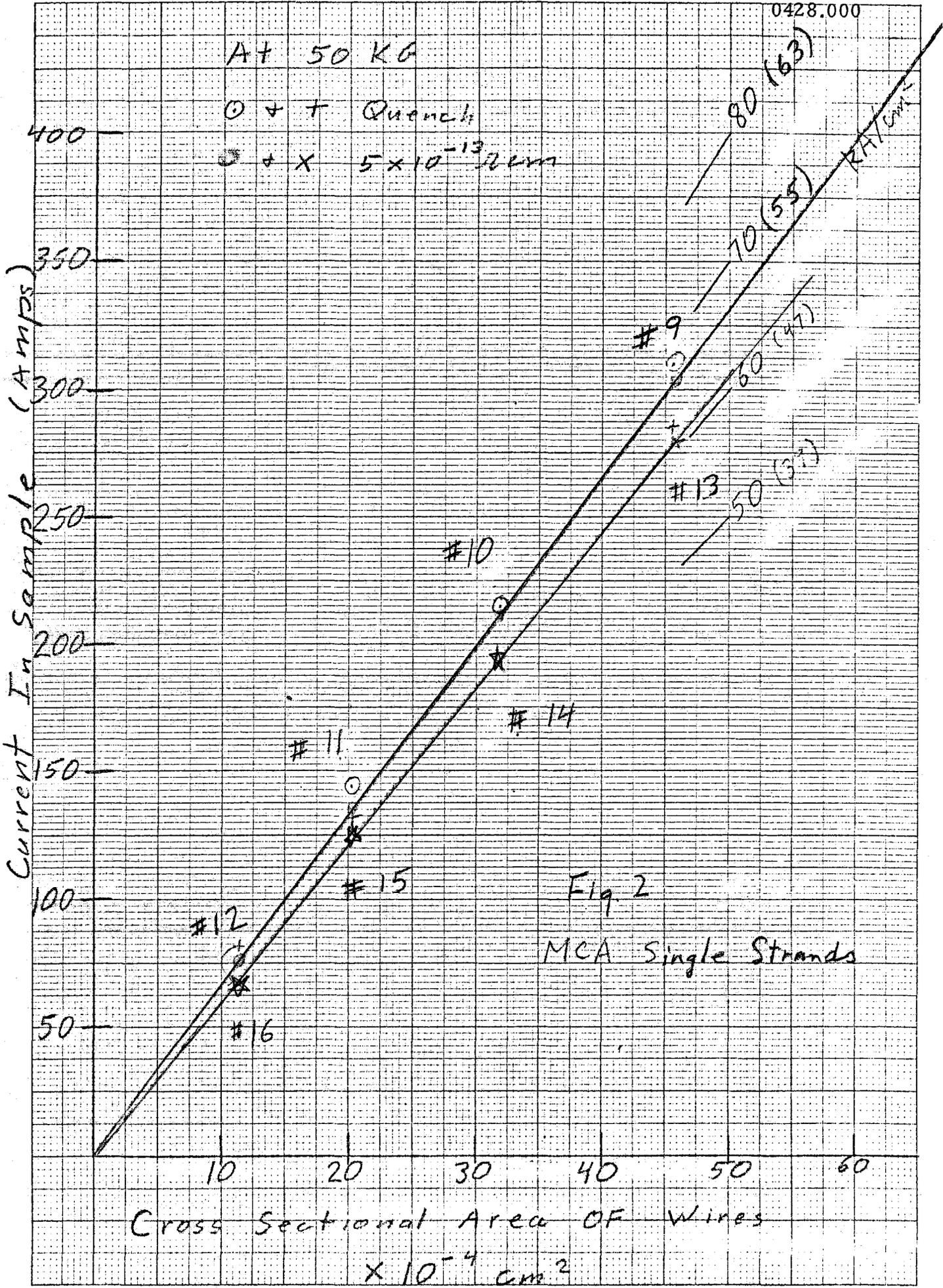
30

40

50

60

Field of Magnet (KG)



# MCA

Current  
In Sample  
(Amps)

single strand #10

.025"

Feb 17, 1975

used for 11 strand MCA

300

200

100

- + Quench
- △  $5 \times 10^{-13} \Omega \text{ cm}$
- $2 \times 10^{-13} \Omega \text{ cm}$
- $10^{-13} \Omega \text{ cm}$

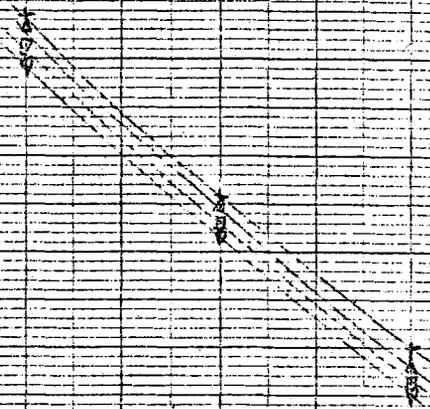


Fig. 3

10

20

30

40

50

60

Field of Magnet (kG)

Current  
In  
Sample  
(Amps)

4000

3000

2000

1000

MCA  
7 strand

Not  
Keystoned

March II

Keystoned

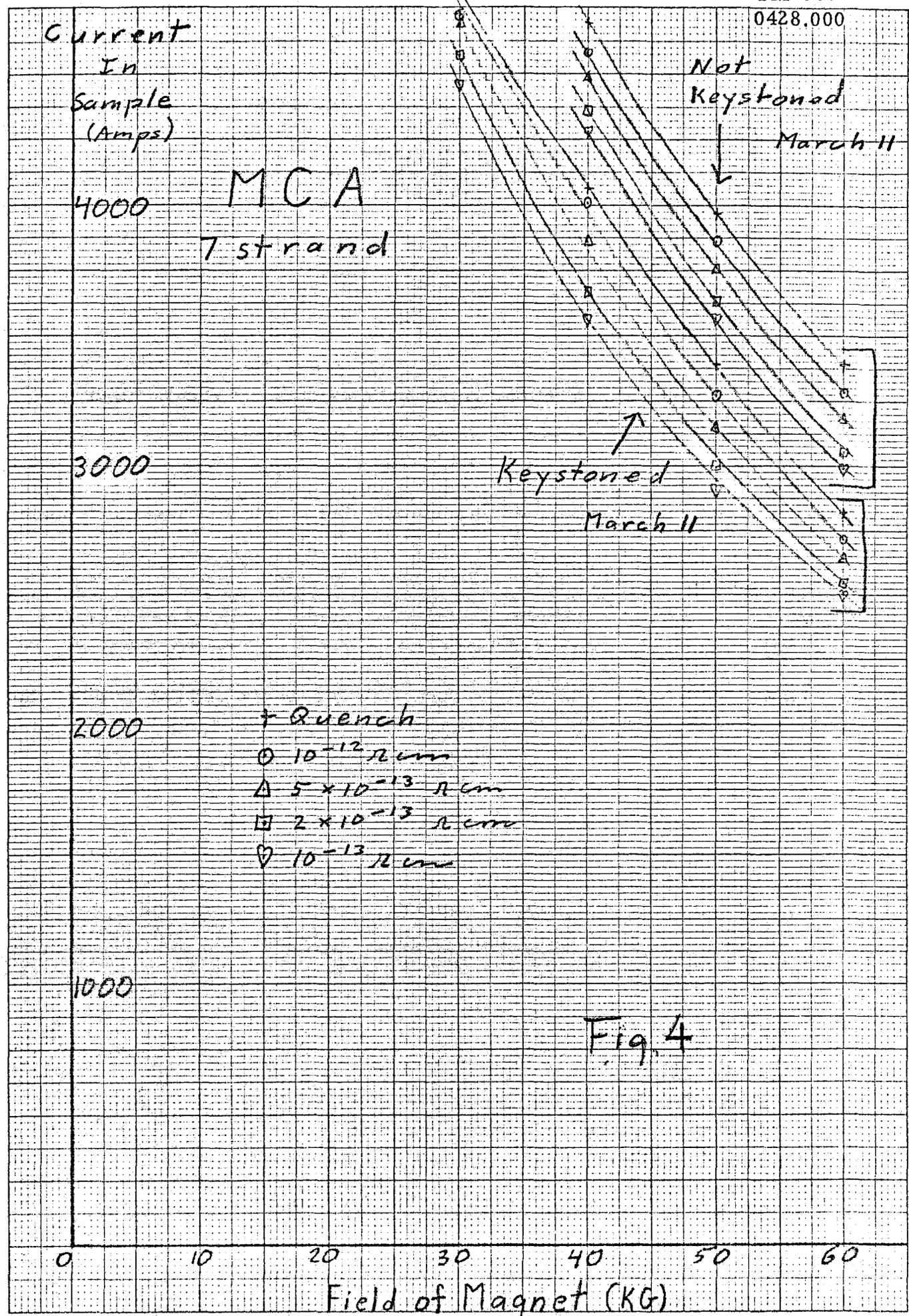
March II

- + Quench
- $10^{-12} \Omega \text{cm}$
- △  $5 \times 10^{-13} \Omega \text{cm}$
- $2 \times 10^{-13} \Omega \text{cm}$
- ▽  $10^{-13} \Omega \text{cm}$

Fig. 4

0 10 20 30 40 50 60

Field of Magnet (KG)



Amp

Fig 5

Critical Currents  
of Solders

150

100

50

$I_B$   
 $I_c$   
at  $10^{-11}$   
 $T_c$  Pb  
60/40 Solder  
(# 203)

50/50 Solder  
(# 202)

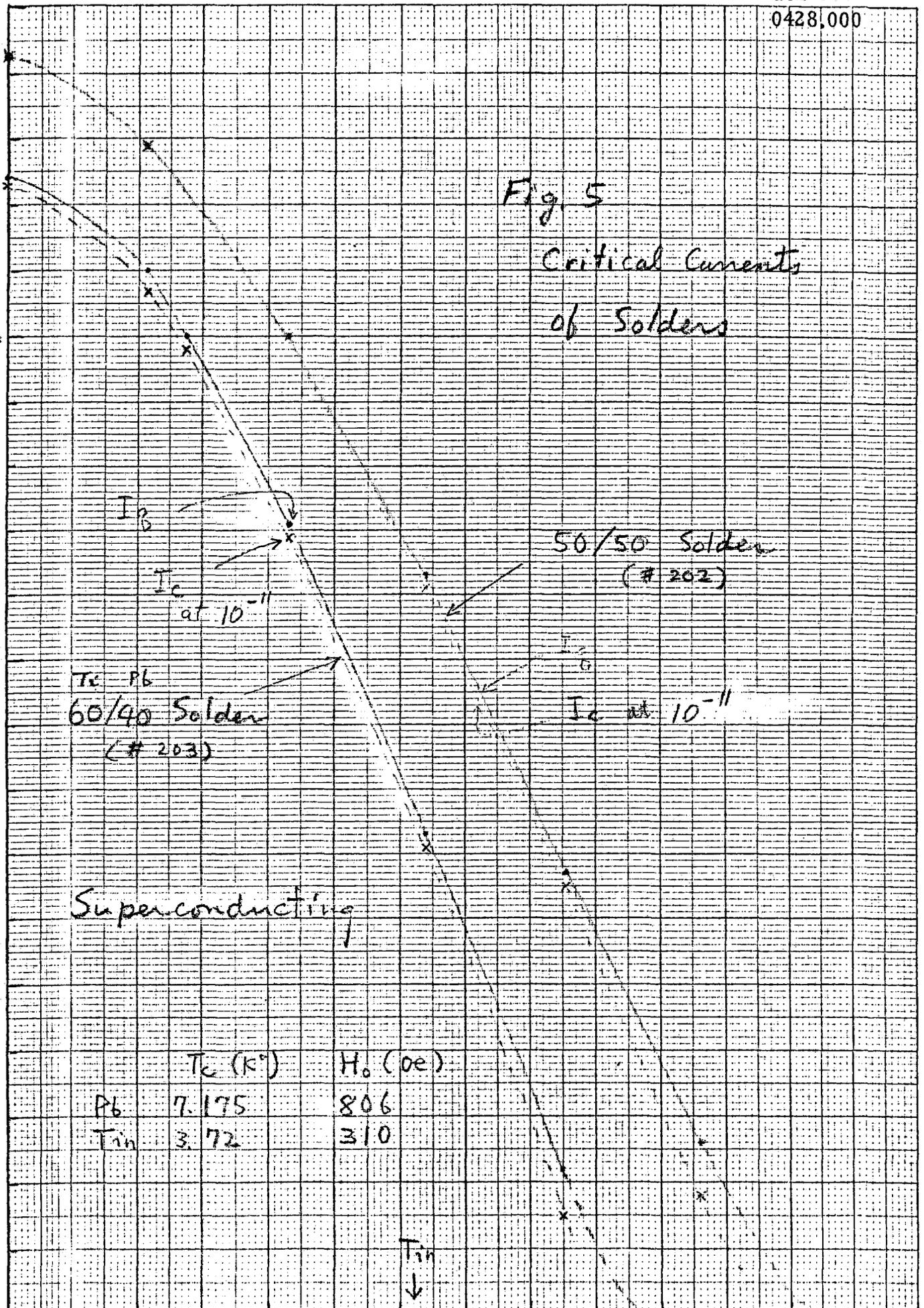
$I_B$   
 $I_c$  at  $10^{-11}$

Superconducting

	$T_c$ (K°)	$H_0$ (oe)
Pb	7.175	806
Tin	3.72	310

Tin  
↓

0 0.1 0.2 0.3 0.4 0.5 0.6 0.7k



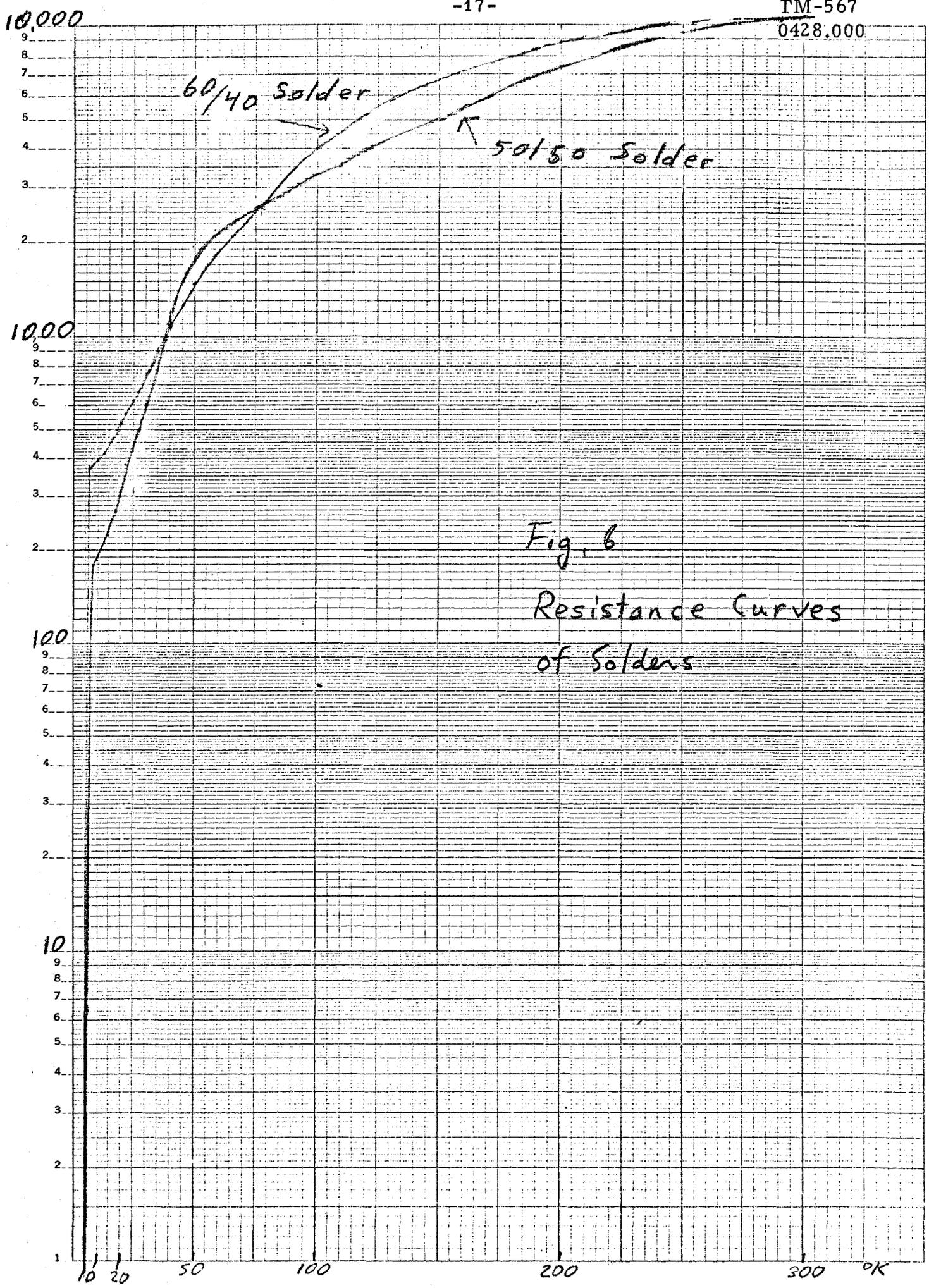


Fig. 6  
Resistance Curves  
of Solders