

Summary of DSA324 Quenches

DSA324 is the third Fermilab 50 mm short SSC dipole that was tested in Lab2. This magnet experienced four thermal cycles. Tests during the first and second cooldown included quench training at 4.3 K and 4.2 K, ramp rate dependence study of quench current at 4.3 K , ramping down from 6500 A at high rates (up to 400 A/S) , strain gage runs to 7350 A at 4.3 K and harmonics measurements as a function of current at the center of the magnet and as a function of position at 5000 A. Some additional tests performed during the second cooldown included quench training at 3.8 K , ramp rate dependence study of quench current at 4.2 K , AC loss measurements at different ramp rates , transfer function and periodic remnant field study using Rawson Lush Fieldmeter. The bore tube was evacuated except during magnetic measurement tests. The voltage tap in the upper outer coil was broken. All the strain gages were in working order when the cooldown to helium temperature started, later a shell gage was lost. The rest of the instrumentation was functional during the remainder of the test. For third cooldown the magnet ends were not preloaded and during the fourth thermal cycle the ends were preloaded to ~500 lb/bullet at ambient temperature.

Quench History (First Cooldown)

A summary of all quench files with quench locations is attached at the end of this report and the quench history is plotted in Figure 1. Figure 2 is a map of voltage tap locations used to determine the quench origins. The quench propagation velocity in straight sections of the coil was typically ≥ 80 m/s and ~ 33 m/s in ramp splices during a standard plateau quench. The first spontaneous quench occurred during a strain gage run ($I_q=7382$ A) at 4.3 K , located in non-ramp splice side straight section of the lower inner turn 19 about 3.3 ms (~ 29.6 cm ± 5 cm) from the lead tap.

The magnet achieved an average plateau current of ~ 7435 A on the second quench. The magnet was quenched five times at plateau current before going on to a strain gage run and then to ramp rate study. All standard plateau quenches (SPQ) were at a ramp rate of 16 A/s and 4.3 K. All SPQ's originated in the straight section of the lower inner pole turn. Four plateau quenches were on ramp-splice side and one was on the non ramp-splice side. However, the quench origin moved around in the straight section of the pole turn. The

quench location was about 40 to 60 cm \pm 5 cm from the lead tap (i.e. ramp splice tap). The quench velocity of these quenches was \sim 83 m/s. Figure 3 shows the voltages in three earliest segments for a typical plateau quench. Figure 4 shows the location of a typical plateau quench on the ramp splice and non-ramp splice side of the coil. Figure 5 shows the voltage growth in three earliest segments due to a typical quench on the side opposite the ramp-splice. The location of such quenches is \sim 25 cm \pm 5 cm from the lead tap.

4.2 K Quenches

The magnet did not show any training at 4.2 K and reached a current of 7690 A in first quench. All 4.2 K plateau quenches were in the same location (pole turn) as 4.3 K plateau quenches. Plateau quench was established by quenching the magnet twice with warm bore still evacuated and for the remaining 4.2 K quenches (in first thermal cycle) warm bore tube was at room temperature. There was no difference between evacuated and non-evacuated (bore tube) quenches. The magnet was ramped at a nominal ramp rate of 16 A/s and an average of \sim 7681 A quench current was achieved. All plateau quenches in turn 19 were about 4 -6 ms from the ramp splice and achieved a $V_q \approx$ 83 m/s. One 4.2 K quench in turn 18 was also on the ramp-splice side of the inner lower coil, \sim 4 ms (37 ± 5 cm) from the return end tap. The magnet temperature was not lowered any further during the first thermal cycle.

Quench History

During the second cooldown period the magnet did not show any training at 4.3 K. The plateau current was \sim 7485 A, \sim 50 A higher than plateau current for the first thermal cycle. The magnet was quenched several times at 4.2 K before and after the low temperature (3.8 K) studies. Plateau quench current at 4.2 K before and after 3.8 K quenches were \sim 7740 A (\sim 70 A higher than it was in the first thermal cycle \sim 7676 A) and \sim 7695 A respectively. The quench location was still the same (straight section of lower inner pole turn on the ramp splice side) at both temperatures. During 4.2 K quenching the only voltage tap in the lower outer coil was lost and a quench in the lower outer coil was detected. This quench originated approximately 13 ms from the ramp splice (nearest tap to the point of quench) in the lower outer coil. A strain gage run to $I_q - 50$ A = 7700 A was also taken at 4.2 K.

During third cooldown the plateau quench currents (I_q) , at all temperatures, were lower than I_q during the other three test cycles. The full range of quench currents is much higher for the third thermal cycle.

Low Temperature Studies

DSA324 temperature was lowered to 3.8 K during the second thermal cycle. It was quenched eight times at low temperature. First two quenches were in the upper and lower outer coils , then there were two quenches in the lower inner pole turn on the ramp-splice side (this is also the location for plateau quenches) before the magnet reached a plateau current of ~ 8175 A. These quenches were roughly 6 ms ($\sim 49 \pm 5$ cm) from the ramp-splice with a quench velocity $V_q \approx 87$ m/s. A strain gage run was also taken during low temperature studies.

During the third cooldown , the magnet did not have any end preload. It showed some training and plateaued at 8078 A , almost ~ 100 A below the previous thermal cycle plateau current. Whereas , during the fourth cooldown the end preload was ~ 500 pound / bullet. The plateau quench current in this test cycle was ~ 8118 A. The difference in quench currents can not be explained by fluctuations in temperatures. Table 2 shows the average temperature during each test cycle.

Ramp Rate Study

The ramp rate dependence of DSA324 was studied during the first two cooldowns. The magnet was quenched at a series of ramp rates ranging from the nominal rate of 16 A/s to 300 A/s. During the first cooldown high ramp rate quench study was done at 4.3 K. All high ramp rate quenches in first test cycle , from 25 - 300 A/s , were in the upper inner multiple turn rather than in one of the ramp splices. All of these quenches originated near the lead end tap of the upper inner coil in turn 13 (on the ramp splice side). Since the multiple turns are not very well instrumented so its rather difficult to pin point the exact location of the quenches. Figure 6 compares the ramp rate dependence of DSA324 with other 50 mm aperture magnets.

During the second cooldown the magnet was tested for ramp rate dependence at 4.3 K and 4.2 K. All high ramp rate quenches were still in upper inner coil multiple turn with the exception of 25 A/s quenches which now were ~ 3.2 ms from the lead tap on non ramp-splice side of the lower inner coil.

All the quenches during third test cycle were at 16 A/s except one at 100 A/s. The only 6 A/s quench in the fourth cooldown was at 7387 A and two quenches were at 25 A/s, and the rest were at 16 A/s. There was one 100 A/s quench in third thermal cycle.

As discussed in TS-SSC 90-26, the SSC dipole magnets should be able to ramp down at the initial ramp rate of -325 A/s. To show magnet's stability DSA324 was ramped down from 6500 A to 4000 A at high ramp rates of -100, -200, -300 and -400 A/s without quenching. At the end of this cycle the magnet was ramped at 16 A/s to quench. This, quench, during the first test cycle, was in the non ramp-splice side of the inner lower coil, ~3.2 ms (28.5 ± 5 cm, in first thermal cycle) from the lead tap .

Temperature Dependence

The quench performance of a magnet depends on temperature of helium bath in which the magnet is immersed. The relation between quench current for $dI/dt \leq 16$ A/s and the average of the three thermometers placed at top, middle and bottom of the magnet is shown in Figure 7. The solid dashed line in the figure is the critical current as predicted by Chris Quigg's program using Mike Green's parametrization of the critical surface. Table 2 shows the averages of plateau quench currents at 16 A/s at different temperatures (the average of three thermometers placed on the magnet skin). A plateau quench for this magnet is the one which originates in the pole turn of lower inner coil (turn 19) and is near the maximum current for a given temperature.

The cable used to wind the inner coils of DSA324 are from reel SSC 3S-00021. The short sample critical current (I_c) at 7 Tesla, 4.22 K for this cable is 10,079 A. A comparison of magnet performance and predicted quench current based on the short sample data is given in Table 1 and Table 2 shows the measured quench current at different temperatures during four cooldowns.

Table 1: Predicted critical current at different temperatures

<u>Temp (K)</u>	<u>Predicted I_{quench}</u>
4.35	7310 A
4.22	7470 A
3.80 K	7960 A

Table 2: Measured quench current at different temperatures during four test cycles.

<u>Thermal Cycle</u>	<u>Temperature</u>	<u>Measured I_{quench}</u>
1	4.35 K	7425 \pm 9 A
2	4.36 K	7486 \pm 5 A
3	4.29 K	7385 \pm 7 A
4	4.35 K	7425 \pm 3 A
1	4.17 K	7681 \pm 9 A
2	4.17 K	7695 \pm 11 A
3	4.19 K	7554 \pm 52 A
4	4.18 K	7651 \pm 8 A
2	3.81 K	7486 \pm 8 A
3	3.82 K	7385 \pm 16 A
4	3.82 K	7425 \pm 10 A

The error bars on the measured data are the standard deviation (of plateau currents) divided by the square root of the number of quenches for each temperature for each thermal cycle.

Distribution:

FNAL
 R. Bossert
 S. Delchamps
 S. Gourlay
 T. Jaffery
 W. Koska
 M. Lamm
 G. Pewitt
 J. Strait

SSCL
 A. Devred
 J. Jayakumar
 J. Tompkins
 R. Wetterskog
 Z. Wolf

DSA324 was cooled down four times and it experienced a total of 112 spontaneous quenches at 4.3 K, 4.2 K and 3.8 K. It is equipped with four SSC2 (12 inch long) type heater strip, one in each quadrant.

Quench File Summary DSA324

Q#	File	I-m	Idot	I-t	Idot	QDC	NIITS	t-Q	V-max	Coil	t(H)	V(H)	T(b)	T(m)	P	LL	Location			
4.35K Plateau Quenches:																				
First Thermal Cycle																				
1	0	1002.	0.	0.	0.	0.	0.	0.	0.	0.	-6.	UI	0.	0.000	0.	4.36	4.31	4.30	831.	
1	1	997.	0.	0.	0.	0.	0.	0.	0.	0.	-6.	UI	0.	0.000	0.	4.38	4.32	4.31	878.	
1	2	7382.	16.	0.	0.	0.	0.	0.	0.	0.	-27.	LI	0.	0.000	0.	4.40	4.34	4.33	880.	
2	2	7436.	16.	0.	0.	0.	0.	0.	0.	0.	-30.	LI	0.	0.000	0.	4.40	4.34	4.33	881.	
3	3	7421.	16.	0.	0.	0.	0.	0.	0.	0.	-26.	LI	0.	0.000	0.	4.36	4.30	4.29	867.	
4	4	7455.	16.	0.	0.	0.	0.	0.	0.	0.	-30.	LI	0.	0.000	0.	4.40	4.34	4.32	879.	
5	5	7436.	16.	0.	0.	0.	0.	0.	0.	0.	-13.	LI	0.	0.000	0.	4.39	4.34	4.33	851.	
6	6	7421.	16.	0.	0.	0.	0.	0.	0.	0.	-12.	LI	0.	0.000	0.	4.39	4.33	4.32	847.	
6	7	7421.	16.	0.	0.	0.	0.	0.	0.	0.	-29.	LI	0.	0.000	0.	4.39	4.33	4.32	881.	
4.35 K Ramp Rate Study:																				
7	7	8	7421.	26.	0.	0.	0.	0.	0.	0.	-23.	UI	0.	0.000	0.	4.33	4.28	4.28	809.	
8	8	9	7240.	50.	0.	0.	0.	0.	0.	0.	-24.	UI	0.	0.000	0.	4.40	4.33	4.31	856.	
9	9	10	7122.	75.	0.	0.	0.	0.	0.	0.	-25.	UI	0.	0.000	0.	4.39	4.33	4.32	851.	
10	10	11	6897.	100.	0.	0.	0.	0.	0.	0.	-15.	LI	0.	0.000	0.	4.39	4.34	4.33	853.	
11	11	12	6790.	125.	0.	0.	0.	0.	0.	0.	-12.	LI	0.	0.000	0.	4.39	4.34	4.33	853.	
12	12	13	6476.	200.	0.	0.	0.	0.	0.	0.	-20.	LI	0.	0.000	0.	4.46	4.34	4.33	857.	
13	13	14	6662.	150.	0.	0.	0.	0.	0.	0.	-18.	LI	0.	0.000	0.	4.39	4.34	4.33	901.	
14	14	15	6344.	250.	0.	0.	0.	0.	0.	0.	-19.	LI	0.	0.000	0.	4.36	4.31	4.30	826.	
15	15	16	6217.	300.	0.	0.	0.	0.	0.	0.	-16.	LI	0.	0.000	0.	4.40	4.33	4.32	864.	
16	16	17	7428.	16.	0.	0.	0.	0.	0.	0.	-12.	LI	0.	0.000	0.	4.39	4.33	4.32	853.	
4.2 K Plateau Quenches:																				
17	17	18	7690.	16.	0.	0.	0.	0.	0.	0.	-28.	LI	0.	0.000	0.	4.21	4.16	4.16	721.	
18	18	19	7681.	16.	0.	0.	0.	0.	0.	0.	-29.	LI	0.	0.000	0.	4.21	4.16	4.16	721.	
19	19	20	7686.	16.	0.	0.	0.	0.	0.	0.	-28.	LI	0.	0.000	0.	4.21	4.16	4.15	718.	
20	20	21	7676.	16.	0.	0.	0.	0.	0.	0.	-27.	LI	0.	0.000	0.	4.21	4.16	4.15	718.	
21	21	22	72.	0.	0.	0.	0.	0.	0.	-1.	LO	0.	0.000	0.	4.20	4.16	4.15	715.		
21	22	23	7656.	16.	0.	0.	0.	0.	0.	-28.	LI	0.	0.000	0.	4.20	4.16	4.15	715.		
22	22	24	7705.	16.	0.	0.	0.	0.	0.	-13.	LI	0.	0.000	0.	4.20	4.16	4.15	715.		
Second Thermal Cycle																				
25	25	1002.	0.	0.	0.	0.	0.	0.	0.	0.	-6.	UI	0.	0.000	0.	4.44	4.38	4.37	881.	
26	26	1438.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	4.41	4.35	4.34	859.	
27	27	797.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	4.40	4.34	4.34	851.	
28	28	7504.	16.	0.	0.	0.	0.	0.	0.	0.	-15.	LI	0.	0.000	0.	4.42	4.35	4.34	871.	
29	29	7490.	16.	0.	0.	0.	0.	0.	0.	-009.	-31.	LI	0.	0.000	0.	4.41	4.35	4.33	859.	
30	30	7470.	16.	0.	0.	0.	0.	0.	0.	-11.	-29.	LI	0.	0.000	0.	4.40	4.33	4.31	862.	
31	31	7480.	16.	0.	0.	0.	0.	0.	0.	-13.	-31.	LI	0.	0.000	0.	4.40	4.34	4.33	852.	
32	32	7480.	16.	0.	0.	0.	0.	0.	0.	-13.	-31.	LI	0.	0.000	0.	4.41	4.34	4.33	858.	
4.35K Ramp Rate Study:																				
28	28	33	7480.	26.	0.	0.	0.	0.	0.	0.	-11.	-28.	LI	0.	0.000	0.	4.38	4.31	4.30	852.
29	29	34	7245.	50.	0.	0.	0.	0.	0.	0.	-007.	-24.	LI	0.	0.000	0.	4.40	4.34	4.32	855.
30	30	35	7157.	75.	0.	0.	0.	0.	0.	0.	-008.	-25.	LI	0.	0.000	0.	4.39	4.34	4.33	847.
31	31	36	6985.	100.	0.	0.	0.	0.	0.	0.	-14.	-30.	LI	0.	0.000	0.	4.41	4.35	4.34	867.
32	32	37	6775.	150.	0.	0.	0.	0.	0.	0.	-17.	-32.	LI	0.	0.000	0.	4.40	4.34	4.33	850.
33	33	38	6525.	200.	0.	0.	0.	0.	0.	0.	-17.	-31.	LI	0.	0.000	0.	4.41	4.35	4.33	853.
34	34	39	6295.	300.	0.	0.	0.	0.	0.	0.	-16.	-31.	LI	0.	0.000	0.	4.39	4.34	4.33	845.
4.2 K Plateau Quenches:																				
35	35	36	35.	7157.	75.	0.	0.	0.	0.	0.	-008.	-25.	LI	0.	0.000	0.	4.39	4.34	4.33	847.
36	36	37	37.	6775.	150.	0.	0.	0.	0.	0.	-14.	-30.	LI	0.	0.000	0.	4.41	4.35	4.34	867.
37	37	38	38.	6525.	200.	0.	0.	0.	0.	0.	-17.	-32.	LI	0.	0.000	0.	4.40	4.34	4.33	850.
38	38	39	39.	6295.	300.	0.	0.	0.	0.	0.	-17.	-31.	LI	0.	0.000	0.	4.41	4.35	4.33	853.
39	39	40.	40.	30.	30.	0.	0.	0.	0.	0.	-16.	-31.	LI	0.	0.000	0.	4.39	4.34	4.33	845.
4.2 K Ramp Rate Study:																				
40	40	41	41.	35.	7157.	75.	0.	0.	0.	0.	-008.	-25.	LI	0.	0.000	0.	4.39	4.34	4.33	847.
41	41	42	42.	35.	6775.	150.	0.	0.	0.	0.	-14.	-30.	LI	0.	0.000	0.	4.41	4.35	4.34	867.
42	42	43	43.	35.	6525.	200.	0.	0.	0.	0.	-17.	-32.	LI	0.	0.000	0.	4.40	4.34	4.33	850.
43	43	44	44.	35.	6295.	300.	0.	0.	0.	0.	-17.	-31.	LI	0.	0.000	0.	4.41	4.35	4.33	853.
44	44	45	45.	35.	30.	30.	0.	0.	0.	0.	-16.	-31.	LI	0.	0.000	0.	4.39	4.34	4.33	845.
First spontaneous quench from lead tap																				
45	45	46	46.	35.	7157.	75.	0.	0.	0.	0.	-008.	-25.	LI	0.	0.000	0.	4.39	4.34	4.33	847.
46	46	47	47.	35.	6775.	150.	0.	0.	0.	0.	-14.	-30.	LI	0.	0.000	0.	4.41	4.35	4.34	867.
47	47	48	48.	35.	6525.	200.	0.	0.	0.	0.	-17.	-32.	LI	0.	0.000	0.	4.40	4.34	4.33	850.
48	48	49	49.	35.	6295.	300.	0.	0.	0.	0.	-17.	-31.	LI	0.	0.000	0.	4.41	4.35	4.33	853.
49	49	50	50.	35.	30.	30.	0.	0.	0.	0.	-16.	-31.	LI	0.	0.000	0.	4.39	4.34	4.33	845.
First spontaneous quench from ramp splice																				
50	50	51	51.	35.	7157.	75.	0.	0.	0.	0.	-008.	-25.	LI	0.	0.000	0.	4.39	4.34	4.33	847.
51	51	52	52.	35.	6775.	150.	0.	0.	0.	0.	-14.	-30.	LI	0.	0.000	0.	4.41	4.35	4.34	867.
52	52	53	53.	35.	6525.	200.	0.	0.	0.	0.	-17.	-32.	LI	0.	0.000	0.	4.40	4.34	4.33	850.
53	53	54	54.	35.	6295.	300.	0.	0.	0.	0.	-17.	-31.	LI	0.	0.000	0.	4.41	4.35</td		

93	7010.	0.	0.	0.0	0.0	Cu L	0.0	0.0000	0.	UI 0.0000	0.	4.21 4.16 4.15	721.	73.	Trip
94	6932.	0.	0.	0.0	0.0	Cu L	0.0	0.0000	0.	LI 0.0000	0.	4.21 4.16 4.15	722.	76.	Trip
3.8 K quench studies:															
75	95	7754.	16.	0.	0.	U-L	0.0	-0.015	-24.	UI 0.0000	0.	3.84 3.80	3.80	98.	95. UI MULTI TURN
76	96	7725.	16.	0.	0.	U-L	0.0	-0.016	-36.	UI 0.0000	0.	3.84 3.79	3.79	495.	92. OL
77	97	7867.	16.	0.	0.	U-L	0.0	-0.021	-38.	UI 0.0000	0.	3.84 3.80	3.80	495.	96. OU
78	98	7637.	16.	0.	0.	U-L	0.0	-0.015	-24.	UI 0.0000	0.	3.86 3.82	3.80	505.	92. IU MULTI TURN
79	99	7984.	16.	0.	0.	U-L	0.0	-0.014	-39.	UI 0.0000	0.	3.84 3.80	3.80	496.	70. DU
80	100	8063.	16.	0.	0.	U-L	0.0	-0.008	-28.	LI 0.0000	0.	3.85 3.81	3.80	503.	81. IL19SR 7 ms from Lead tap
81	101	8102.	16.	0.	0.	U-L	0.0	-0.005	-27.	LI 0.0000	0.	3.84 3.79	3.79	494.	95. IL19SR 7 ms from Lead tap
82	102	8023.	16.	0.	0.	U-L	0.0	-0.010	-24.	LI 0.0000	0.	3.85 3.81	3.80	500.	89. IL16SL 4 ms from Lead tap 415 (non pole turn quench)
83	103	8107.	16.	0.	0.	U-L	0.0	-0.005	-26.	LI 0.0000	0.	3.84 3.80	3.80	498.	86. IL19SR 6 ms from Lead tap
84	104	8097.	16.	0.	0.	U-L	0.0	-0.006	-26.	LI 0.0000	0.	3.85 3.81	3.80	504.	92. IL19SR 6 ms from Lead tap
Heater Studies:															
105	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.200	-12.	UI 0.0000	0.	4.26 4.22	4.21	761.	79.
106	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.170	-12.	UI 0.0000	0.	4.25 4.20	4.20	753.	79.
107	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.150	-12.	UI 0.0000	0.	4.28 4.21	4.21	761.	79.
108	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.145	-12.	UI 0.0000	0.	4.27 4.22	4.21	765.	78.
109	1993.	0.	0.	0.0	0.0	U-L	0.0	-0.025	-30.	UI 0.0000	0.	4.27 4.22	4.22	761.	79.
110	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.020	-30.	UI 0.0000	0.	4.26 4.21	4.20	757.	80.
111	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.0000	0.	4.27 4.22	4.22	768.	79.
112	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.010	-30.	UI 0.0000	0.	4.30 4.23	4.22	780.	78.
113	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.0000	0.	4.29 4.23	4.22	842.	81.
114	-2.	0.	0.	0.0	0.0	V-dI	0.0	0.000	0.	LO 0.0000	0.	4.26 4.21	4.20	755.	78.
115	-2.	0.	0.	0.0	0.0	V-dI	0.0	0.000	0.	LO 0.0000	0.	4.26 4.21	4.20	758.	78.
116	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.185	-12.	UI 0.0000	0.	4.27 4.21	4.20	772.	79.
117	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.170	-12.	UI 0.0000	0.	4.28 4.22	4.21	799.	78.
118	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.155	-12.	UI 0.0000	0.	4.27 4.22	4.21	783.	81.
119	1991.	0.	0.	0.0	0.0	U-L	0.0	-0.155	-12.	UI 0.0000	0.	4.24 4.20	4.19	740.	81.
120	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.0000	0.	4.26 4.20	4.19	769.	78.
121	5002.	0.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.0000	0.	4.33 4.22	4.20	808.	78.
122	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.0000	0.	4.20 4.15	4.15	718.	83.
123	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.095	-30.	UI 0.0000	0.	4.20 4.15	4.15	717.	79.
124	4993.	0.	0.	0.0	0.0	U-L	0.0	-0.075	-30.	UI 0.0000	0.	4.20 4.15	4.15	717.	79.
85	125	7480.	16.	0.	0.	U-L	0.0	-0.010	-27.	LI 0.0000	0.	4.22 4.18	4.17	730.	80.
Fourth Cooldown															
126	992.	0.	0.	0.0	0.0	V-dI	0.0	-6.	UI 0.0000	0.	4.39 4.27	4.26	857.	8.	
127	987.	0.	0.	0.0	0.0	V-dI	0.0	-6.	UI 0.0000	0.	4.38 4.29	4.28	855.	12.	
86	128	7431.	16.	0.	0.	U-L	0.0	-0.015	-32.	LI 0.0000	0.	4.38 4.31	4.31	848.	78.
87	129	7421.	16.	0.	0.	U-L	0.0	-0.013	-30.	LI 0.0000	0.	4.41 4.36	4.35	878.	78.
88	130	7426.	16.	0.	0.	U-L	0.0	-0.012	-30.	LI 0.0000	0.	4.39 4.34	4.33	856.	78.
89	131	7426.	16.	0.	0.	U-L	0.0	-0.013	-30.	LI 0.0000	0.	4.39 4.33	4.32	854.	68.
90	132	7690.	16.	0.	0.	U-L	0.0	-0.008	-28.	LI 0.0000	0.	4.21 4.16	4.16	720.	83.
91	133	7676.	16.	0.	0.	U-L	0.0	-0.008	-28.	LI 0.0000	0.	4.21 4.16	4.16	720.	83.
92	134	7661.	16.	0.	0.	U-L	0.0	-0.011	-28.	LI 0.0000	0.	4.21 4.16	4.16	720.	83.
93	135	7387.	6.	0.	0.	U-L	0.0	-0.009	-30.	LI 0.0000	0.	4.21 4.16	4.16	720.	83.
94	136	7627.	16.	0.	0.	U-L	0.0	-0.013	-28.	LI 0.0000	0.	4.18 4.17****	4.17	734.	75.
95	137	7637.	16.	0.	0.	U-L	0.0	-0.007	-27.	LI 0.0000	0.	4.18 4.16	4.11	720.	73.
96	138	7612.	16.	0.	0.	U-L	0.0	-0.013	-28.	LI 0.0000	0.	4.21 4.19	4.71	750.	79.
97	139	7602.	16.	0.	0.	U-L	0.0	-0.010	-26.	LI 0.0000	0.	4.18 4.15	4.58	717.	77.
98	140	7642.	16.	0.	0.	U-L	0.0	-0.008	-28.	LI 0.0000	0.	4.23 4.22****	4.22	768.	77.
99	141	7661.	16.	0.	0.	U-L	0.0	-0.008	-28.	LI 0.0000	0.	4.17 4.17	4.17	724.	76.
3.8 K quench studies:															
100	142	8102.	16.	0.	0.	U-L	0.	-0.007	-26.	LI 0.0000	0.	3.81 3.80****	4.97.	75.	
101	143	8116.	16.	0.	0.	U-L	0.	-0.007	-26.	LI 0.0000	0.	3.82 3.81****	503.	76.	
102	144	8121.	16.	0.	0.	U-L	0.	-0.007	-26.	LI 0.0000	0.	3.83 3.82-2.81	507.	75.	
103	145	8116.	16.	0.	0.	U-L	0.	-0.007	-26.	LI 0.0000	0.	3.82 3.81****	503.	77.	

104	148	8136.	16.	0.0	0.0	U-L	0.0	-0.008	-28.	LI 0.000	0. 3.81 3.80*****	498.	70.	IL19SR 5 ms from Lead tap
147	4136.	16.	0.0	0.0	Cu L	0.0	0.000	0.	UI 0.000	0.*****	726.	86.	Trip-lost thermometers (*)	

4.2 K quenches:

105	148	7827.	25.	0.0	0.0	U-L	0.0	-0.006	-22.	UI 0.000	0.*****	713.	86.	IL19SR 3.5 ms from Lead tap
106	149	7871.	16.	0.0	0.0	U-L	0.0	-0.014	-29.	LI 0.000	0. 4.21 4.16 4.16	719.	85.	IL19SR 3.5 ms from Lead tap

Heater Studies

150	1977.	0.	0.0	0.0	U-L	0.0	-0.150	-12.	UI 0.000	0. 4.21 4.16 4.16	717.	85.	
151	4983.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.000	0. 4.21 4.16 4.16	720.	81.	
152	1977.	0.	0.0	0.0	U-L	0.0	-0.180	-12.	UI 0.000	0. 4.21 4.16 4.16	717.	82.	
153	1962.	0.	0.0	0.0	U-L	0.0	-0.160	-12.	UI 0.000	0. 4.22 4.17 4.16	727.	77.	
154	4988.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.000	0. 4.22 4.17 4.16	727.	77.	
155	1986.	0.	0.0	0.0	U-L	0.0	-0.165	-12.	UI 0.000	0. 4.21 4.16 4.16	719.	83.	
156	4978.	0.	0.0	0.0	U-L	0.0	-0.020	-30.	UI 0.000	0. 4.21 4.16 4.16	718.	83.	
157	1987.	0.	0.0	0.0	U-L	0.0	-0.170	-12.	UI 0.000	0. 4.21 4.16 4.16	717.	77.	
158	4973.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.000	0. 4.21 4.16 4.16	718.	78.	
159	1981.	0.	0.0	0.0	U-L	0.0	-0.165	-12.	UI 0.000	0. 4.21 4.16 4.16	718.	79.	
160	4978.	0.	0.0	0.0	U-L	0.0	-0.015	-30.	UI 0.000	0. 4.21 4.16 4.16	718.	79.	
161	1981.	0.	0.0	0.0	U-L	0.0	-0.160	-12.	UI 0.000	0. 4.21 4.16 4.16	718.	79.	
162	4978.	0.	0.0	0.0	U-L	0.0	-0.020	-30.	UI 0.000	0. 4.21 4.16 4.16	718.	79.	
163	1981.	0.	0.0	0.0	U-L	0.0	-0.160	-12.	UI 0.000	0. 4.21 4.16 4.16	718.	79.	
164	4988.	0.	0.0	0.0	U-L	0.0	-0.020	-30.	UI 0.000	0. 4.21 4.16 4.16	718.	79.	

4.2 K quenches:

107	165	7878.	16.	0.0	0.0	U-L	0.0	-0.010	-27.	LI 0.000	0. 4.21 4.16 4.16	720.	73.	IL19SR 10 ms(10 ms) from Lead tap
108	166	7848.	26.	0.0	0.0	U-L	0.0	-0.005	-26.	LI 0.000	0. 4.20 4.15 4.15	717.	74.	IL19SR 2 ms from Lead tap
109	167	7818.	16.	0.0	0.0	U-L	0.0	-0.155	28.	UI 0.000	0. 4.34 4.23 4.21	897.	79.	OU
110	168	7846.	16.	0.0	0.0	U-L	0.0	-0.008	26.	UI 0.000	0. 4.21 4.17 4.16	718.	90.	Multiturn
111	169	7837.	16.	0.0	0.0	U-L	0.0	-0.013	19.	LI 0.000	0. 4.22 4.17 4.17	728.	73.	IL19SR 4 ms from Lead tap
112	170	7886.	16.	0.0	0.0	U-L	0.0	-0.008	18.	LI 0.000	0. 4.21 4.16 4.15	720.	76.	IL19SR 4 ms from Lead tap

170 7886. 16. 0.0 0.0 U-L 0.0 -0.008 18. LI 0.000 0. 4.21 4.16 4.15 720. 76.

----- QSUMARY V83.13 -----

FORMAT:

Q#	File	I-m	Idot	I-t	Idot	QDC	MIITS	t-Q	V-max	Coil	t(H)	V(H)	T(t)	T(m)	T(b)	P	LL	Location
A5,	15,	F8.0,F5.0,F5.1,F5.1,	A5,F5.1,	F8.0,	A4,	F6.3,F5.0,F5.2,F5.2,F5.0,F5.0,2X,A30												

NOTATION KEY

Q# Quench number or Spot heater number (e.g. s4 is spot heater 4)
File Quench file number

I-m Main coil current at quench

Idot Main coil di/dt at quench

I-t Trim coil current at quench

Idot Trim coil di/dt at quench

Name of quench detection circuit which tripped:

1) U-L Upper - Lower Coil

2) V-dI Magnet - Idot

3) SC L SC Pwr Leads - Idot

4) Vtot Magnet

5) Trim Trim Coil

6) Cu L Cu Pwr Leads - IR

7) GndI Ground Fault Monitor

8) Thru Through Bus - Idot

MIITS Integral of (I**2)dt from t-Q to "infinity"

t-Q Time first voltage appears in V(Upper) - V(Lower) (relative to quench detection time)

y-max Maximum voltage across any quarter coil

Coil	coil corresponding to V-max
$t(H)$	Protection heater firing time (relative to quench detection time); -999 if heater did not fire
$V(H)$	Protection heater firing voltage; -999. if heater did not fire
$T(t)$	Temperature at top of magnet
$T(m)$	Temperature at middle of magnet
$T(b)$	Temperature at bottom of magnet
P	Dewar pressure (Torr)
LL	Liquid level (%)
Location	Quench or spot heater location

DSA324 QUENCH HISTORY

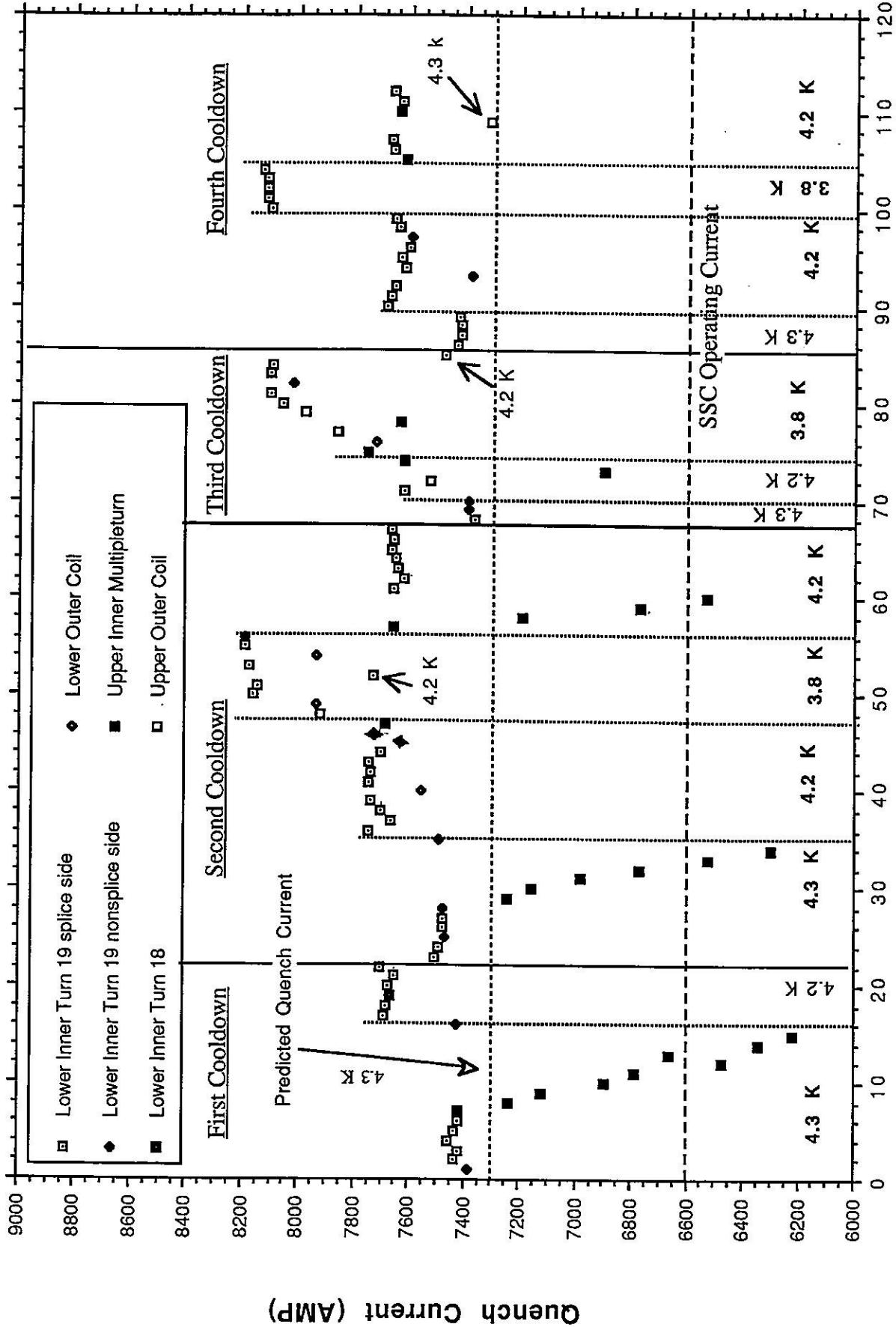
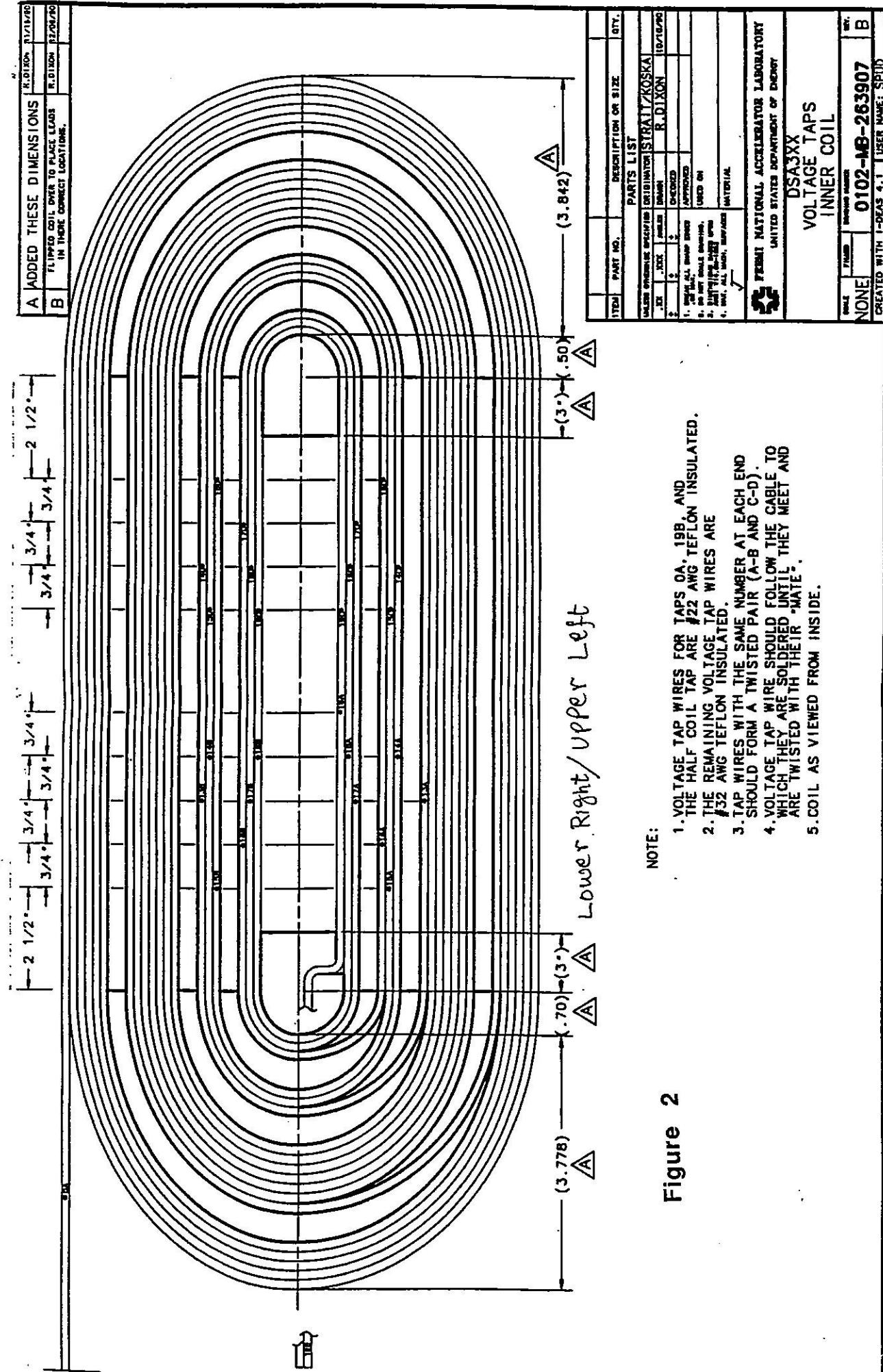


Figure 1

Lower Left / Upper Right



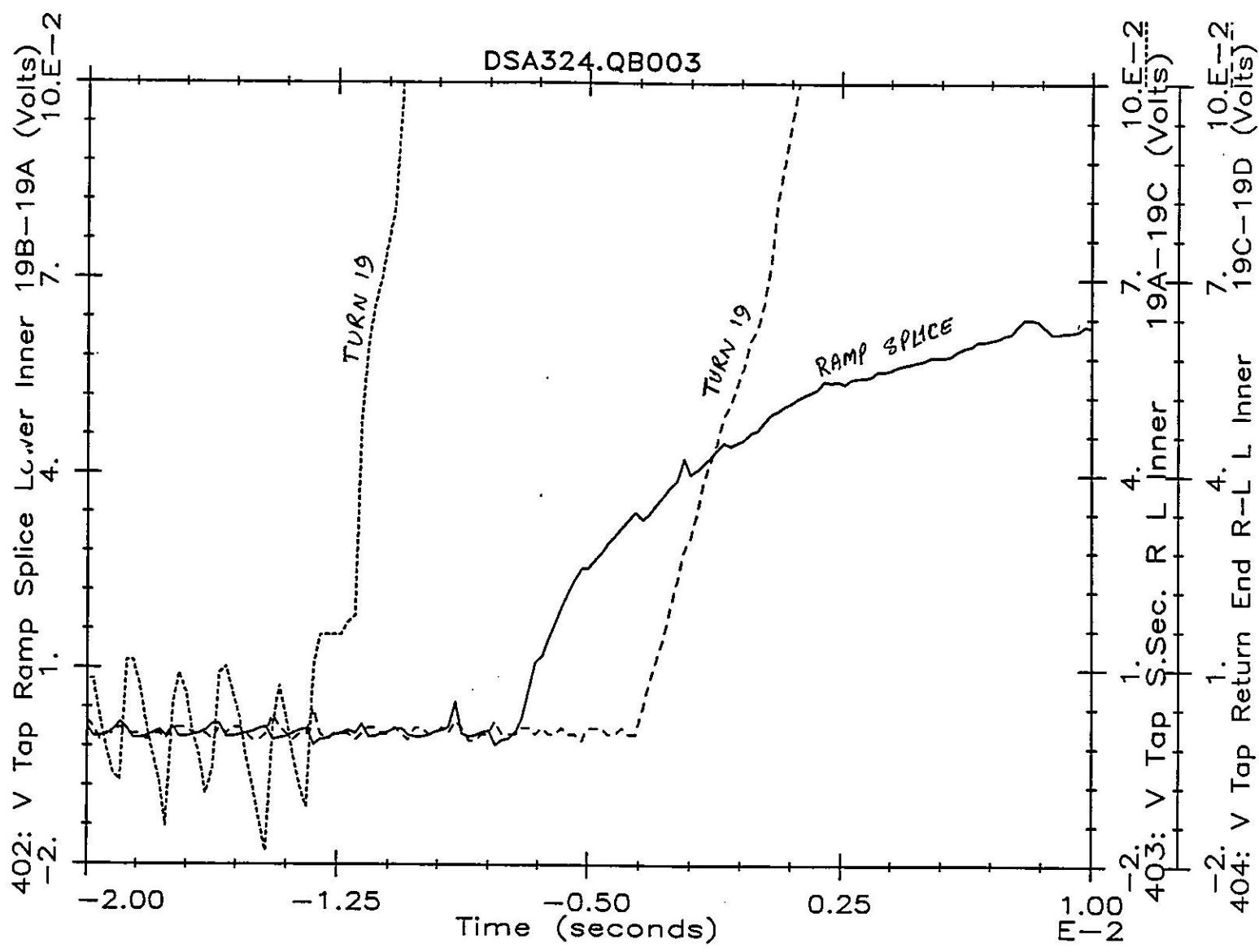
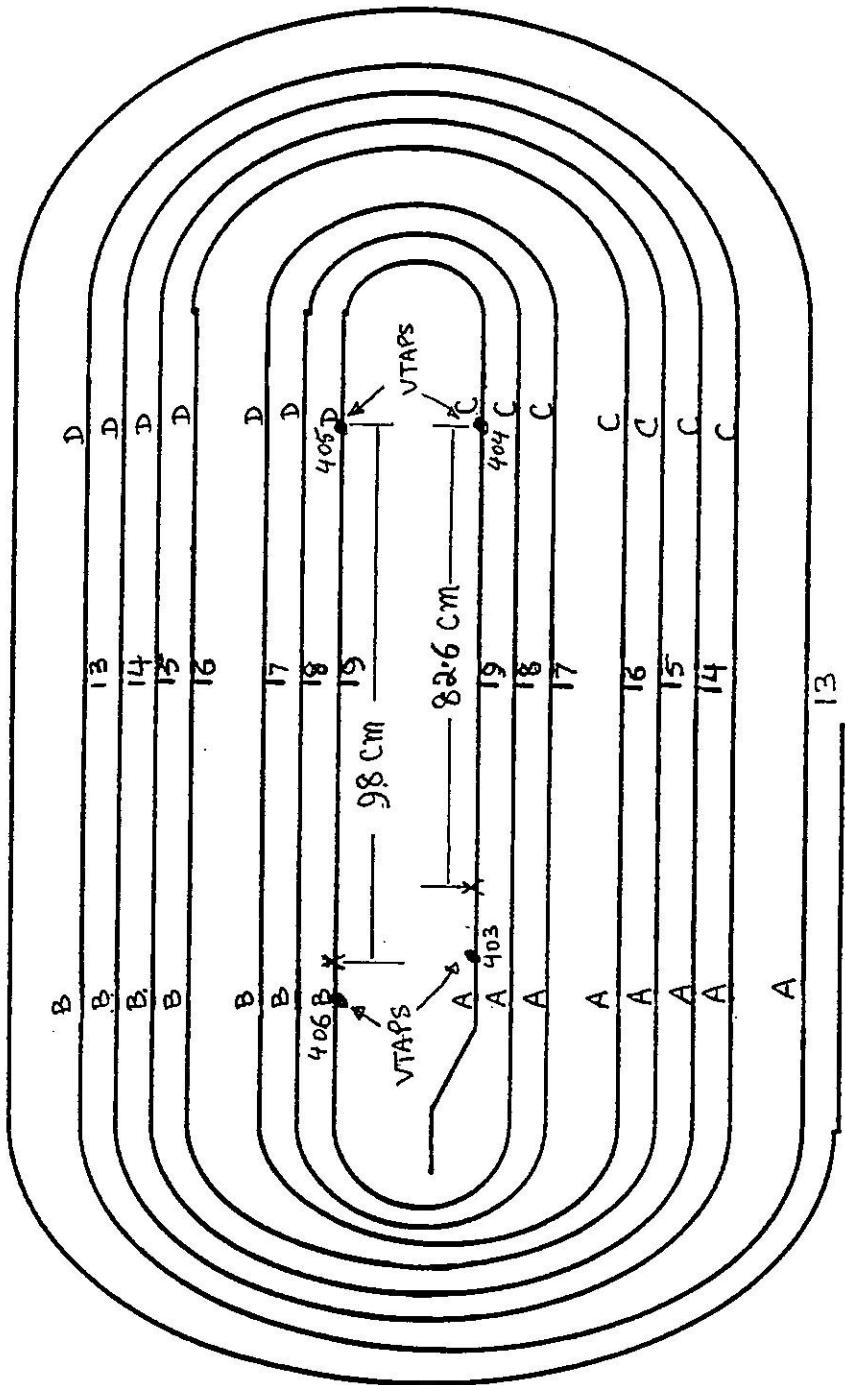


Figure 3

LOWER LEFT / UPPER RIGHT



LOWER RIGHT / UPPER LEFT

Figure 4

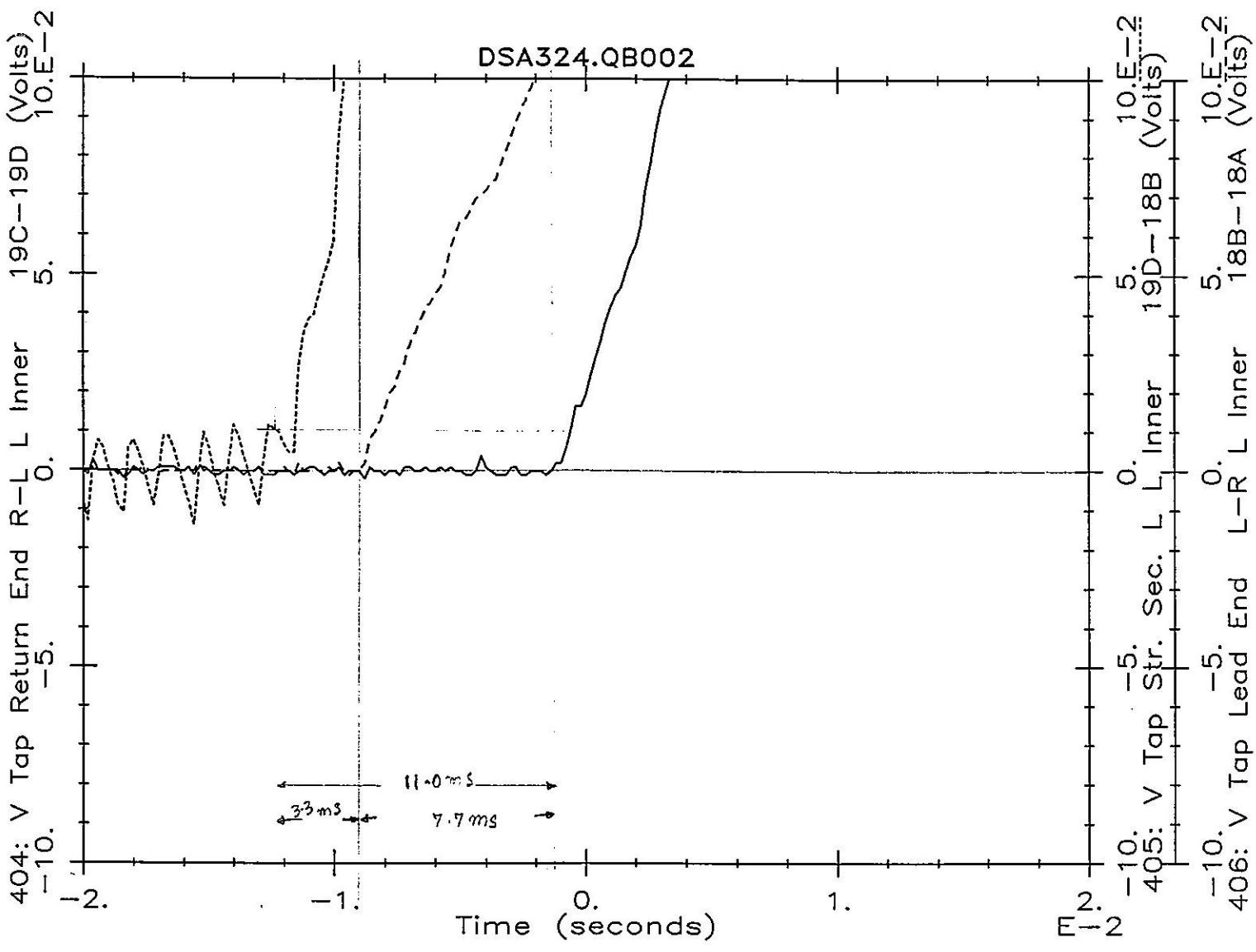


Figure 5

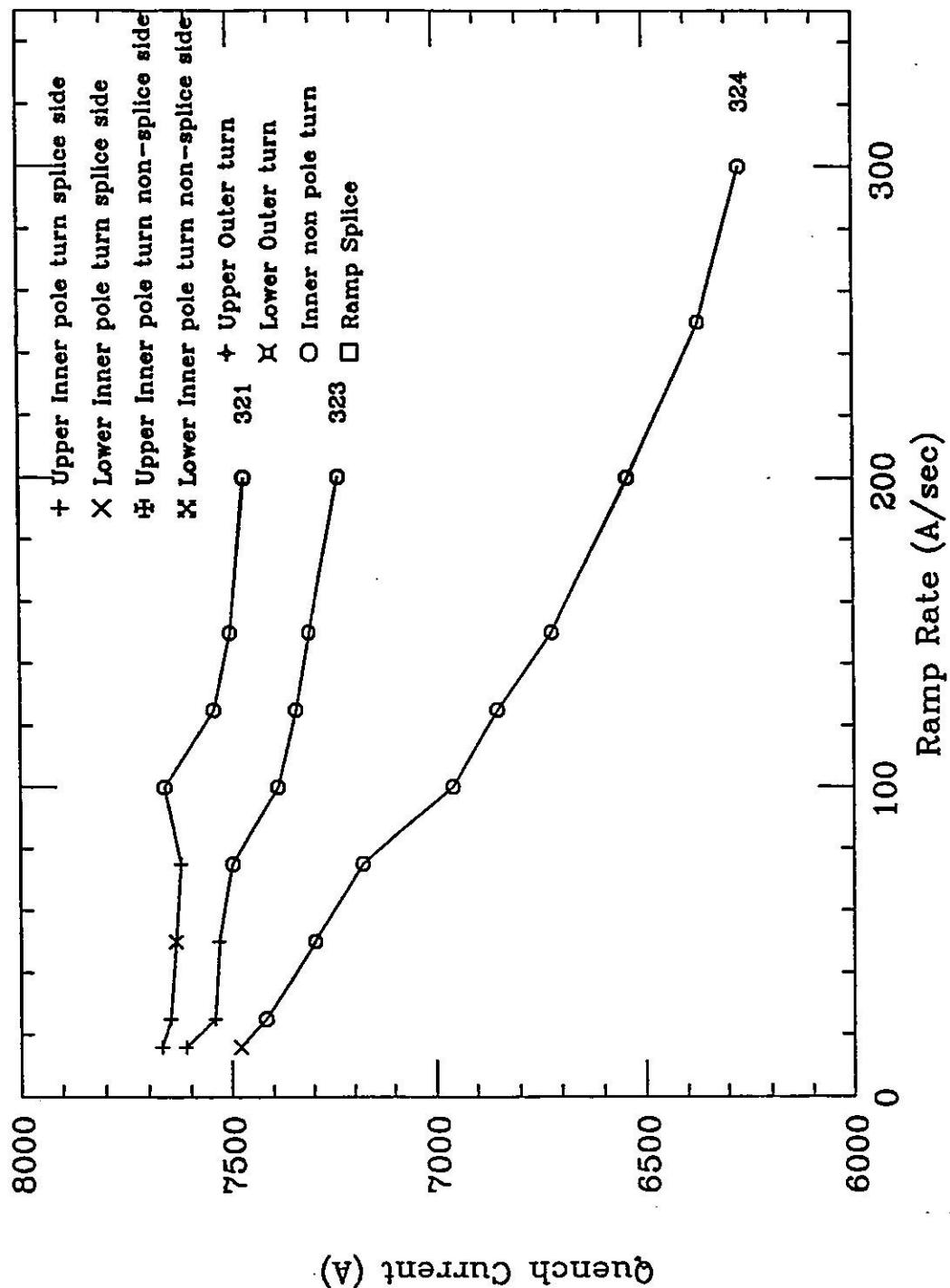
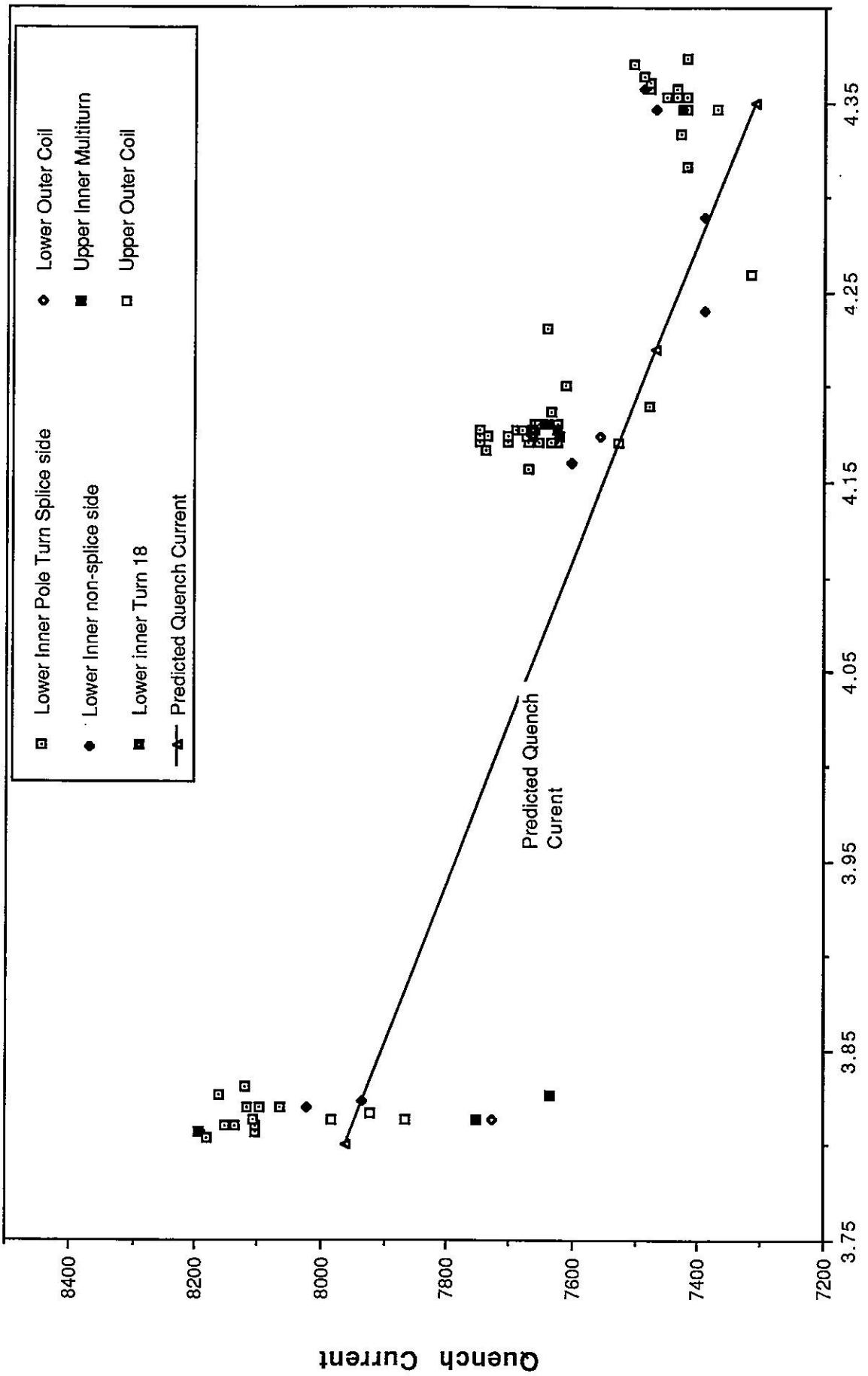


Figure 6

DSA324 Quench Current vs Temperature



Temperature (K)

Figure 7