

TS-SSC 91-257  
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## Summary of DSA326 Quenches

DSA326 is the fourth Fermilab 50 mm aperture short SSC dipole magnet. This magnet experienced three thermal cycles during which it was quenched (spontaneous quenches) a total of 54 times. Tests during the first cooldown included quench training at temperatures of 4.3 K and 4.2 K. During the second and third cooldown the magnet was quenched at temperatures of 4.3 K, 4.2 K and 3.8 K. The first and second cooldown tests also included ramping down of magnet from 6500 A at high rates (up to 400 A/S), strain gage runs to >7300 A at 4.3 K and harmonics measurements as a function of current at the center of the magnet and as a function of position at 5000 A. Some additional tests performed during the second cooldown included ramp rate dependence study of quench current at 4.3 K. Heater induced quench studies were done during the first thermal cycle. Throughout the magnet test the bore tube was evacuated except during magnetic measurement tests. The zero current end preload during the first two cooldowns was on the order of 250 lbs./bullet and it was increased to 4000 lbs./bullet (at ambient temperature) for the third cycle of tests. There was no obvious change in quench performance due to the increased end preload. The measured magnet temperatures used in this report are the average of three thermometers used on the magnet and the temperature fluctuation is within .05K unless otherwise. This report is a chronological summary of test results followed by a comparison of magnet performance and predicted quench currents at different temperatures.

### Quench History (First Cooldown)

A summary of all the quench files with quench locations is attached at the end of this report and the quench history is plotted in Figure 1. Figure 2 is a map of voltage tap locations used to determine the quench origins. The quench propagation velocity in straight sections of the coil was typically  $\geq 80$  m/s and  $\sim 33$  m/s in ramp splices during a standard plateau quench. The first spontaneous quench occurred during a strain gage run ( $I_q=7343$  A) at 4.3 K, located in ramp splice side straight section of the upper inner turn 19 about 3.3 ms ( $26 \text{ cm} \pm 5 \text{ cm}$ ) from the ramp-splice voltage tap.

The second quench was in the pole turn at a current of  $\sim 7362$  A. The magnet achieved an average plateau current of  $\sim 7386$  A during the first cooldown. The magnet was quenched four times (4.3K) at plateau current before going on to a strain gage run and then to quench study at 4.2K. All standard plateau quenches (SPQ) were at a ramp rate of 16 A/s and 4.3 K. All quenches originated in the straight section of the upper inner pole turn. Four quenches were on ramp-splice side and one was on the non ramp-splice side of the coil. The quench location was about  $38 \pm 5$  cm from the lead tap (i.e. ramp splice tap ). The quench velocity of these quenches was  $\sim 83$  m/s. Figure 3 shows the voltages in three earliest segments for a typical quench. Figure 4 shows the location of a typical quench on the ramp splice and non-ramp splice side of the coil. Figure 5 shows the voltage growth in three earliest segments due to a typical quench on the side opposite the ramp-splice. The location of such quenches is  $\sim 33\text{cm} \pm 2$  cm from the lead tap . The quench currents have a standard deviation of  $\sim 28$  A and the full range of quench currents is almost 70 A. See Table 1 for details.

#### 4.2 K Quenches

The magnet did not show any training at 4.2 K and reached a current of 7671 A in the first quench. All 4.2 K quenches were in turn 19 of upper inner coil in the same location (pole turn) as 4.3 K quenches. Three quenches were in the straight section of the non ramp splice side of the coil and one was in the ramp splice side of the coil. The magnet was ramped at a nominal ramp rate of 16 A/s and an average quench current of  $\sim 7666$  A was achieved. All quenches in turn 19 were about 4 -5ms from the lead voltage tap and had a  $V_q \approx 83$  m/s. One quench on ramp splice side of the magnet was  $\sim 7$  ms ( $58 \pm 5$  cm ) from the ramp splice voltage tap. The quench currents have a standard deviation of  $\sim 14$  A and the full range of quench currents is 25 A. See Table 1 for details. The magnet temperature was not lowered any further during the first thermal cycle.

#### Quench History (Second Cooldown)

During the second cooldown period there are some indications of magnet training at some points at both 4.3 K and 4.2 K. The quench current at each temperature was some what erratic and the large spread in quench currents at 16 A/s cannot be explained by temperature fluctuations. The location of all the 16 A/s quenches, at 4.3 K and 4.2 K, was similar to the quenches in the first test cycle. The full range of quench currents is much higher for the second test cycle which is not fully understood. There is no evident low ramp rate plateau during the second cycle of cold tests. BNL magnet DSA309 also showed an erratic quench plateau until a ramp rate of 2 A/s was tried.

### 4.3K Quenches

During second cooldown the magnet was quenched 19 times at 4.3K. Ramp rate studies was also done during the second cooldown. All 16 A/s quenches were in the upper inner pole turn. The first spontaneous quench occurred during a strain gage ramp (16 A/s, 4.35K) at 7465 A. The second quench was at a lower current of 7333 A (4.29K), which can not be explained with temperature fluctuations, still in the pole turn of the upper inner coil. The magnet quenched twice close to ~7460 A and once at 7441 A. The quench current on five quenches was similar to first cooldown quenches at about 7400 A and the remaining two quenches of 16 A/s were close to 7420 A. The wide range of quench currents at 16 A/s is quite evident during the second cooldown.

### 4.2 K Quenches

It was then quenched 10 times at 4.2K. Once again all 16 A/s quenches occurred in upper inner coil either on the ramp splice or non ramp splice side of the coil. The temperature fluctuation from quench to quench was ~.06K. The first quench was at 7460 A similar to quenches in first test cycle. Following three quenches were near 7500 A and the fifth quench was at a much higher current of 7661 A. The seventh quench was (7568 A) almost 100 A lower than the previous two quenches. The magnet quenched four times close to 7660 A and once at 7612 A. As mentioned above the magnet had a wide range of quench currents at 16 A/s. The magnet temperature was then lowered to 3.8 K.

### Ramp Rate Studies

Ramp rate dependence of DSA326 was studied during the second cooldown at 4.3K. The magnet was quenched at a series of ramp rates ranging from the nominal rate of 16 A/s to 300 A/s. The only 6 A/s quench in the second cooldown was at 7421 A in the upper inner pole turn. All high ramp rate quenches in second test cycle, from 25 - 300 A/s, were in the upper inner multiple turn rather than in one of the ramp splices. All of these quenches originated near the lead end tap of the upper inner coil in turn 13 (on the ramp splice side of the coil). Since the multiple turns are not very well instrumented, it's rather difficult to pin point the exact location of these quenches. Figure 6 compares the ramp rate dependence of DSA326 with other 50 mm aperture magnets. All the quenches during third test cycle were at 16 A/s.

## Quench History (Third Cooldown)

The magnet was recooled the third time. It was then quenched six times at 4.3K. The location of all 16 A/s quenches was similar to the quenches in previous two coolodowns, i.e; pole turn of upper inner coil. The temperature fluctuation from quench to quench was  $\sim 0.05$ K. At 4.3K the quench currents have a standard deviation of  $\sim 22$  and the full range of quench currents is almost 54 A at 16 A/s. The only quench at 4.2K during third cooldown was at 7656 A. The magnet temperature was then lowered to 3.8 K.

## Low Temperature Studies

DSA326 temperature was lowered to 3.8 K during the second and third cooldowns. During the second test cycle it was quenched five times at 3.8K. All the quenches were in the upper inner pole turn. The first quench was at 7930 A about 2 ms ( $\sim 17$  cm) from the ramp splice voltage tap. Then the magnet was quenched four times and it reached a plateau current of  $\sim 8126$  A. These quenches were  $\sim 4$  ms from the ramp splice voltage tap in the straight section of the upper inner coil turn 19, with a quench velocity  $V_q \approx 83$  m/s. A strain gage run was also taken during low temperature studies. At lower temperature the plateau quench currents had a standard deviation of 7 A and the spread in plateau quench currents was also very small (15 A).

During the third cooldown the magnet was quenched three times at 3.8K and it exhibited no retraining. All quenches were standard plateau quenches. It reached an average quench current of 8105 A with a standard deviation of  $\sim 14$  A. Table 1 shows this and the average temperature during each test cycle.

As discussed in TS-SSC 90-26, the SSC dipole magnets should be able to ramp down at the initial ramp rate of  $-325$  A/s. To show magnet's stability DSA326 was ramped down from 6500 A to 4000 A at high ramp rates of  $-100$ ,  $-200$ ,  $-300$  and  $-400$  A/s without quenching. At the end of this cycle the magnet was ramped at 16 A/s to quench. This test was performed during the first and second test cycles.

During the first two cooldowns the zero current end preload, at ambient temperature, was  $\sim 1.11$  kN ( $\sim 250$  lbs.) per bullet ( $\sim 30$  in-lb torque/bullet). For third cooldown, the magnet end preload was increased to  $\sim 18$  kN ( $\sim 4000$  lbs.) per bullet and the lead end screws were also torqued to  $\sim 37$  ft-lb/screw. There is no evident difference in quench currents due to increased end preload.

## Temperature Dependence

The quench performance of a magnet depends on temperature of helium bath in which the magnet is immersed. The relation between quench current for  $dI/dt \leq 16$  A/s and the average of the three thermometers placed at top, middle and bottom of the magnet is shown in Figure 7. The solid line in the figure is the critical current as predicted by Chris Quigg's program using Mike Green's parametrization of the critical surface. Table 1 shows the averages of quench currents at 16 A/s at different temperatures (the average of three thermometers placed on the magnet skin). A plateau quench for this magnet is the one which originates in the pole turn of upper inner coil (turn 19) and is near the maximum current for a given temperature.

The cable used to wind the inner coils of DSA326 are from reel SSC 3S-00021. The short sample critical current ( $I_c$ ) at 7 Tesla, 4.22 K for this cable is 10,079 A. A comparison of magnet performance and predicted quench current based on the short sample data is given in Table 2 and Table 1 shows the measured quench current at different temperatures during three cooldowns. The  $I_q$  for first four quenches, at 4.2K during the second cooldown, was close to 7500 A, and the rest six quenches were at much higher currents. There are two average quench currents for second cooldown at 4.2 K. Quenches 2 thru 4 have been bunched together and quenches 5 thru 10 have been grouped together in table 1.

**Table 1:** Measured quench current at different temperatures during four test cycles.

<u>Test Cycle #</u>	<u>Temperature</u>	<u>Measured <math>I_{quench}</math></u>	<u>Full Range of current</u>
1	4.34 K	7386 $\pm$ 11A	
3	4.36 K	7404 $\pm$ 9 A	
1	4.17 K	7666 $\pm$ 9 A	
2	4.22 K	7518 A	34 A (for quench 2 thru quench 4, test cycle #2)
2	4.19 K	7642 A	108 A (for quench 5 thru quench 10, test cycle #2)
3	4.18 K	7656 A	
2	3.80 K	8126 $\pm$ 4 A	
3	3.82 K	8105 $\pm$ 9A	

**Table 2:** Predicted critical current at different temperatures

<u>Temp (K)</u>	<u>Predicted I<sub>quench</sub></u>
4.35	7310 A
4.22	7470 A
3.80 K	7960 A

The error bars on the measured data are the standard deviation (of quench currents) divided by the square root of the number of quenches for each temperature for each thermal cycle.

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Quench File Summary  
DSA326

Q#	File	I-m	Idot	I-t	Idot	V-dI	QDC	MIITs	t-Q	V-max	Coil	t(H)	V(H)	T(t)	T(m)	T(b)	P	LL	Location
First Cooldown:																			
0		-75.	0.	0.0	0.0	V-dI	0.0	0.0000	0.	U0	0.0000	0.	0.0000	0.000	0.000	0.000	0.	0.	manual trip to check s.c.
1		-85.	0.	0.0	0.0	Vtot	0.0	-0.002	7.	U0	0.0000	0.	4.23	4.18	4.18	744.	73.	73.	manual trip to check s.c.
2		-3674.	0.	0.0	0.0	Cu L	0.0	0.0000	0.	U0	0.0000	0.	4.23	4.18	4.18	743.	73.	73.	manual trip to check s.c.
3		-3865.	0.	0.0	0.0	Cu L	0.0	0.0000	0.	U0	0.0000	0.	4.23	4.18	4.18	743.	73.	73.	manual trip to check s.c.
4		-4114.	0.	0.0	0.0	Cu L	0.0	0.0000	0.	U0	0.0000	0.	4.23	4.18	4.18	743.	73.	73.	manual trip to check s.c.
5		1002.	0.	0.0	0.0	V-dI	0.0	0.0000	-6.	UI	0.0000	0.	4.23	4.18	4.18	743.	72.	72.	manual trip to check s.c.
6		1991.	0.	0.0	0.0	U-L	0.0	0.0000	-11.	UI	0.0000	0.	4.35	4.30	4.30	834.	75.	75.	manual trip to check s.c.
7		1002.	0.	0.0	0.0	V-dI	0.0	0.0000	-6.	UI	0.0000	0.	4.36	4.32	4.31	845.	72.	72.	manual trip to check s.c.
8		997.	0.	0.0	0.0	Vtot	0.0	-0.003	-6.	UI	0.0000	0.	4.40	4.35	4.35	874.	85.	85.	manual trip to check s.c.
-----4.3 K QUENCHES-----																			
9		7343.	16.	0.0	0.0	U-L	0.0	-0.017	-25.	UI	0.0000	0.	4.39	4.34	4.33	867.	74.	74.	IU19SR 3.5 ms from Ramp Splice
10		7362.	16.	0.0	0.0	U-L	0.0	-0.014	-23.	UI	0.0000	0.	4.35	4.30	4.29	853.	65.	65.	IU19SR 3.5 ms from Ramp Splice
11		7397.	16.	0.0	0.0	U-L	0.0	-0.011	-25.	UI	0.0000	0.	4.40	4.35	4.34	871.	69.	69.	IU19SR 3.5 ms from Ramp Splice
12		7392.	16.	0.0	0.0	U-L	0.0	-0.015	-25.	UI	0.0000	0.	4.38	4.33	4.32	867.	66.	66.	IU19SR 3.5 ms from Ramp Spl
13		7416.	16.	0.0	0.0	U-L	0.0	-0.010	-25.	UI	0.0000	0.	4.35	4.30	4.29	866.	66.	66.	IU19SR 2.5 ms from Ramp Spl
14		7406.	16.	0.0	0.0	U-L	0.0	-0.009	-24.	UI	0.0000	0.	4.37	4.32	4.31	878.	67.	67.	IU19SL 4 ms from LE
-----4.2 KStudies-----																			
15		1007.	0.	0.0	0.0	Vtot	0.0	0.0000	-6.	UI	0.0000	0.	4.20	4.15	4.15	724.	76.	76.	Manual Trip to check system
16		7671.	16.	0.0	0.0	U-L	0.0	-0.006	-24.	UI	0.0000	0.	4.20	4.15	4.15	724.	76.	76.	IU19SL ~4 ms from LE
17		7671.	16.	0.0	0.0	U-L	0.0	-0.012	-24.	UI	0.0000	0.	4.20	4.15	4.15	724.	59.	59.	IU19SR ~7 ms from Ramp Spl
18		7676.	16.	0.0	0.0	U-L	0.0	-0.008	-24.	UI	0.0000	0.	4.20	4.15	4.15	724.	59.	59.	IU19SL ~4.8 ms from LE
-----Heater tests-----																			
19		-6.	0.	0.0	0.0	V-dI	0.0	0.0000	0.	U0	0.0000	0.	4.20	4.15	4.15	724.	84.	84.	
20		-2.	0.	0.0	0.0	V-dI	0.0	0.0000	0.	U0	0.0000	0.	4.20	4.15	4.15	724.	84.	84.	
21		-2.	0.	0.0	0.0	V-dI	0.0	0.0000	0.	U0	0.0000	0.	4.20	4.15	4.15	723.	75.	75.	
22		-2.	0.	0.0	0.0	U-L	0.0	0.0000	0.	U0	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
23		1991.	0.	0.0	0.0	V-dI	0.0	-0.325	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
24		1991.	0.	0.0	0.0	V-dI	0.0	-0.341	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	73.	73.	
25		2025.	0.	0.0	0.0	V-dI	0.0	-0.285	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	73.	73.	
26		1986.	0.	0.0	0.0	V-dI	0.0	-0.535	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	73.	73.	
27		1986.	0.	0.0	0.0	V-dI	0.0	-0.492	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
28		1986.	0.	0.0	0.0	V-dI	0.0	-0.352	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
29		1991.	0.	0.0	0.0	V-dI	0.0	-0.347	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
30		1986.	0.	0.0	0.0	V-dI	0.0	-0.346	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
31		1991.	0.	0.0	0.0	V-dI	0.0	-0.352	-12.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
32		4978.	0.	0.0	0.0	V-dI	0.0	-0.028	-30.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
33		4978.	0.	0.0	0.0	V-dI	0.0	-0.012	-30.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
34		4978.	0.	0.0	0.0	V-dI	0.0	-0.035	-30.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
35		4978.	0.	0.0	0.0	V-dI	0.0	-0.032	-30.	UI	0.0000	0.	4.20	4.15	4.15	723.	74.	74.	
36		62.	100.	0.0	0.0	Vtot	0.0	-0.002	7.	U0	0.0000	0.	4.26	4.22	4.21	771.	48.	48.	
37		1986.	0.	0.0	0.0	V-dI	0.0	-0.554	-12.	UI	0.0000	0.	4.20	4.16	4.15	724.	74.	74.	
38		1986.	0.	0.0	0.0	V-dI	0.0	-0.554	-12.	UI	0.0000	0.	4.20	4.16	4.15	724.	74.	74.	
39		1986.	0.	0.0	0.0	V-dI	0.0	-0.503	-12.	UI	0.0000	0.	4.20	4.16	4.15	724.	74.	74.	
40		1986.	0.	0.0	0.0	V-dI	0.0	-0.515	-12.	UI	0.0000	0.	4.20	4.16	4.15	724.	74.	74.	
41		1986.	0.	0.0	0.0	V-dI	0.0	-0.518	-12.	UI	0.0000	0.	4.20	4.16	4.15	724.	74.	74.	
42		4973.	0.	0.0	0.0	V-dI	0.0	-0.050	-30.	UI	0.0000	0.	4.20	4.16	4.15	724.	74.	74.	
43		4978.	0.	0.0	0.0	V-dI	0.0	-0.045	-30.	UI	0.0000	0.	4.21	4.17	4.16	730.	75.	75.	
44		4968.	0.	0.0	0.0	V-dI	0.0	-0.051	-30.	UI	0.0000	0.	4.21	4.17	4.16	730.	75.	75.	
45		4978.	0.	0.0	0.0	V-dI	0.0	-0.049	-30.	UI	0.0000	0.	4.21	4.17	4.16	730.	75.	75.	
46		4978.	0.	0.0	0.0	V-dI	0.0	-0.050	-30.	UI	0.0000	0.	4.21	4.17	4.16	730.	75.	75.	
47		4978.	0.	0.0	0.0	V-dI	0.0	-0.049	-30.	UI	0.0000	0.	4.21	4.17	4.16	730.	75.	75.	
48		-2.	0.	0.0	0.0	V-dI	0.0	0.0000	1.	L0	0.0000	0.	0.00	0.00	0.00	0.	0.	0.	
49		1986.	0.	0.0	0.0	V-dI	0.0	0.0000	-12.	UI	0.0000	0.	4.21	4.17	4.16	730.	75.	75.	



-----3.8 K QUENCHES-----

40	104	7930.	16.	0.0	0.0	U-L	0.0	-013	-23.	UI 0.000	0.	3.84	3.80	3.80	497.	92.	IU19SR	~2 ms from Ramp Spl
41	105	8121.	16.	0.0	0.0	U-L	0.0	-005	-22.	UI 0.000	0.	3.83	3.79	3.80	496.	82.	IU19SR	~4 ms from Ramp Spl
42	106	8136.	16.	0.0	0.0	U-L	0.0	-005	-22.	UI 0.000	0.	3.82	3.78	3.78	492.	70.	IU19SR	~3.5 ms from Ramp Spl
43	107	8121.	16.	0.0	0.0	U-L	0.0	-007	-22.	UI 0.000	0.	3.85	3.81	3.80	505.	70.	IU19SR	~4 ms from Ramp Spl
44	108	8126.	16.	0.0	0.0	U-L	0.0	-005	-23.	UI 0.000	0.	3.79	3.75	3.76	479.	70.	IU19SR	~4 ms from Ramp Spl

Third Cooldown:

-----4.3 K QUENCHES-----

109	1002.	0.	0.0	0.0	V-dI	0.0	0.000	-6.	UI 0.000	0.	4.39	4.34	4.34	858.	76.	manual	trip to check safety ckts	
110	1002.	0.	0.0	0.0	V-dI	0.0	0.000	-6.	UI 0.000	0.	4.37	4.32	4.32	844.	74.	manual	trip to check safety ckts	
45	111	7441.	16.	0.0	0.0	U-L	0.0	-012	-32.	UI 0.000	0.	4.42	4.36	4.36	878.	74.	IU19SR	~4 ms from Ramp Spl
46	112	7387.	16.	0.0	0.0	U-L	0.0	-010	-27.	UI 0.000	0.	4.41	4.36	4.36	877.	58.	IU19SL	~3.5 ms from LE tap
47	113	7421.	16.	0.0	0.0	U-L	0.0	-010	-25.	UI 0.000	0.	4.40	4.34	4.34	861.	76.	IU19SR	~5.2 ms from Ramp Spl
48	114	7392.	16.	0.0	0.0	U-L	0.0	-012	-26.	UI 0.000	0.	4.40	4.35	4.34	871.	79.	IU19SR	~6 ms from Ramp Spl
49	115	7397.	16.	0.0	0.0	U-L	0.0	-010	-27.	UI 0.000	0.	4.37	4.32	4.31	847.	67.	IU19SR	~5.5 ms from Ramp Spl
50	116	7387.	16.	0.0	0.0	U-L	0.0	-011	-27.	UI 0.000	0.	4.39	4.33	4.32	855.	70.	IU19SR	~5.5 ms from Ramp Spl
51	117	7656.	16.	0.0	0.0	U-L	0.0	-010	-24.	UI 0.000	0.	4.21	4.16	4.16	726.	73.	IU19SR	~2.5 ms from Ramp Spl

-----3.8 K Studies-----

52	118	8092.	16.	0.0	0.0	U-L	0.0	-005	-22.	UI 0.000	0.	3.84	3.80	3.80	499.	87.	IU19SR	~4.2 ms from Ramp Spl
53	119	8121.	16.	0.0	0.0	U-L	0.0	-006	-22.	UI 0.000	0.	3.85	3.81	3.81	505.	88.	IU19SR	~4.5 ms from Ramp Spl
54	120	8102.	16.	0.0	0.0	U-L	0.0	-005	-22.	UI 0.000	0.	3.84	3.81	3.80	503.	81.	IU19SR	~3.5 ms from Ramp Spl
121	5355.	0.	0.0	0.0	Cu L	0.0	-001	0.	LI 0.000	0.	3.84	3.80	3.79	503.	94.			

FORMAT:

Q# File I-m Idot I-t Idot QDC MIITS t-q V-max Coil t(H) V(H) T(t) T(m) T(b) P LL Location  
 A5, I5, F8.0,F5.0,F5.1,F5.1, A5,F5.1, F6.3, F6.0, A4, F6.3,F5.0,F5.2,F5.2,F5.2,F5.0,F5.0,2X,A30

NOTATION KEY

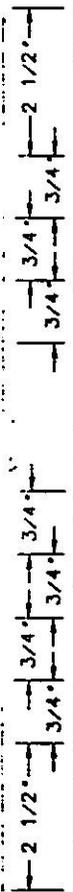
Quench number or Spot heater number (e.g. s4 is spot heater 4)

- Q# File Quench file number
- I-m Main coil current at quench
- Idot Main coil di/dt at quench
- I-t Trim coil current at quench
- Idot Trim coil di/dt at quench
- QDC Name of quench detection circuit which tripped:
  - 1) U-L Upper - Lower Coil
  - 2) V-dI Magnet - Idot
  - 3) SC L SC Pwr Leads - Idot
  - 4) Vtot Magnet
  - 5) Trim Trim Coil
  - 6) Cu L Cu Pwr Leads - IR
  - 7) GndI Ground Fault Monitor
  - 8) Thru Through Bus - Idot

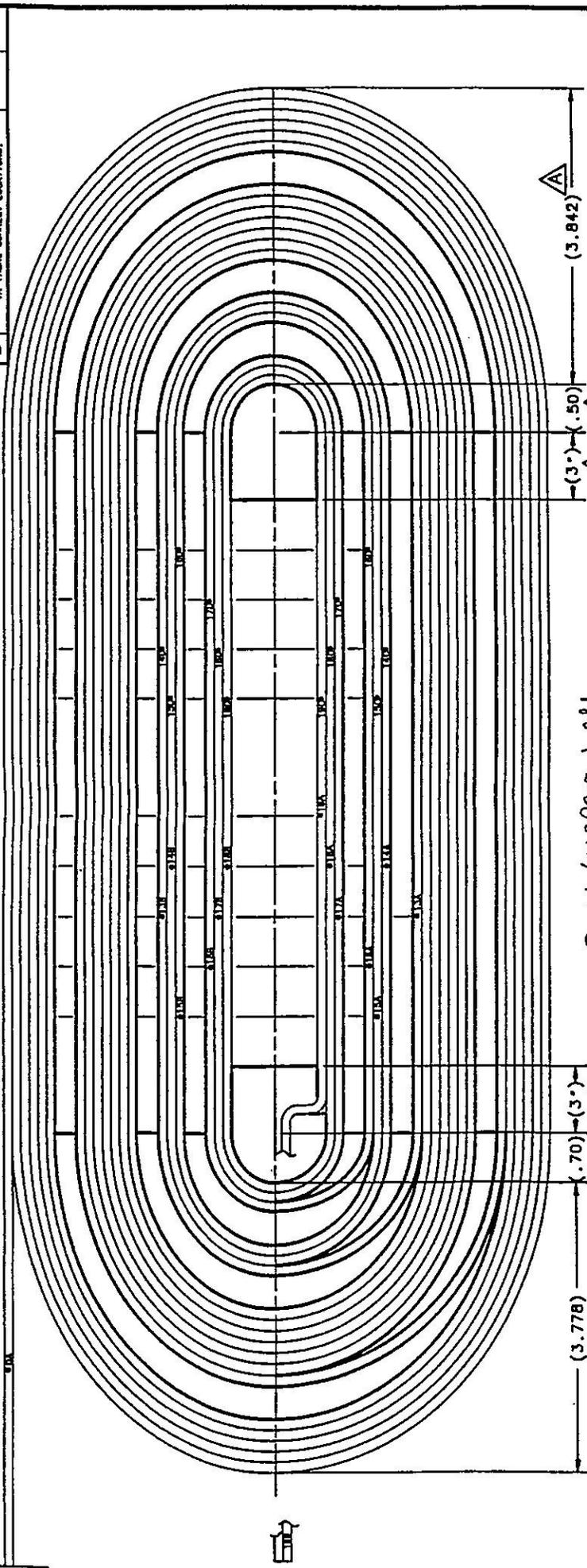
- MIITS Integral of (I\*\*2)dt from t-q to "infinity"
- t-q Time first voltage appears in V(Upper) - V(Lower) (relative to quench detection time)
- V-max Maximum voltage across any quarter coil
- Coil Coil corresponding to V-max
- t(H) Protection heater firing time (relative to quench detection time); -999 if heater did not fire
- V(H) Protection heater firing voltage; -999. if heater did not fire
- T(t) Temperature at top of magnet
- T(m) Temperature at middle of magnet
- T(b) Temperature at bottom of magnet
- P Dewar pressure (Torr)
- LL Liquid level (%)
- Location Quench or spot heater location



Lower Left / Upper Right



A	ADDED THESE DIMENSIONS	R. DIXON	11/11/90
B	FLIPPED COIL OVER TO PLACE LEADS IN THEIR CORRECT LOCATIONS.	R. DIXON	12/01/90



Lower Right / Upper Left

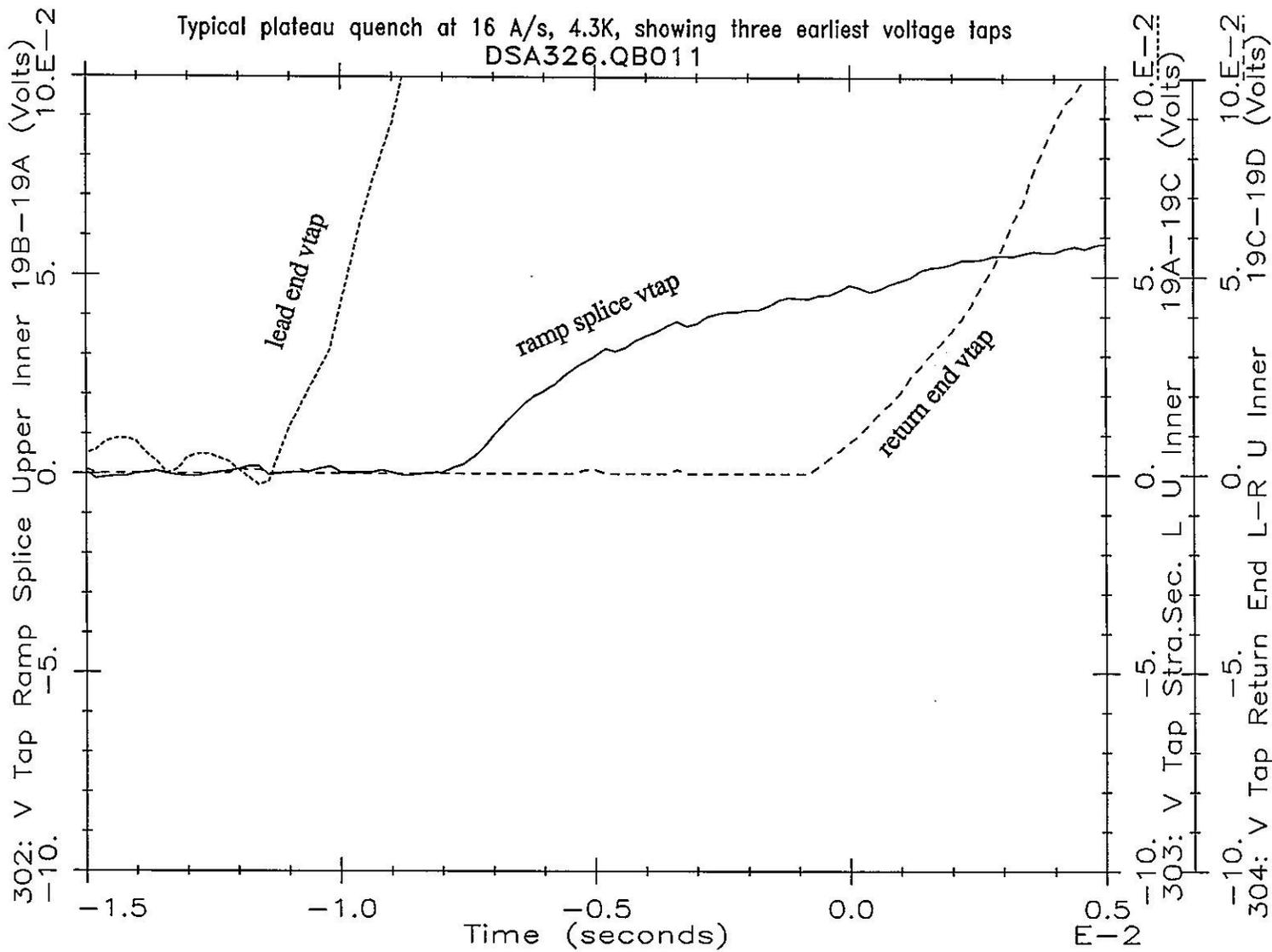
ITEM	PART NO.	DESCRIPTION OR SIZE	QTY.
PARTS LIST			
1	WIRE	ORIGINATOR	19/10/90
2	WIRE	ORIGINATOR	19/10/90
3	WIRE	ORIGINATOR	19/10/90
4	WIRE	ORIGINATOR	19/10/90
5	WIRE	ORIGINATOR	19/10/90
6	WIRE	ORIGINATOR	19/10/90
7	WIRE	ORIGINATOR	19/10/90
8	WIRE	ORIGINATOR	19/10/90
9	WIRE	ORIGINATOR	19/10/90
10	WIRE	ORIGINATOR	19/10/90
11	WIRE	ORIGINATOR	19/10/90
12	WIRE	ORIGINATOR	19/10/90
13	WIRE	ORIGINATOR	19/10/90
14	WIRE	ORIGINATOR	19/10/90
15	WIRE	ORIGINATOR	19/10/90
16	WIRE	ORIGINATOR	19/10/90
17	WIRE	ORIGINATOR	19/10/90
18	WIRE	ORIGINATOR	19/10/90
19	WIRE	ORIGINATOR	19/10/90
20	WIRE	ORIGINATOR	19/10/90
21	WIRE	ORIGINATOR	19/10/90
22	WIRE	ORIGINATOR	19/10/90
23	WIRE	ORIGINATOR	19/10/90
24	WIRE	ORIGINATOR	19/10/90
25	WIRE	ORIGINATOR	19/10/90
26	WIRE	ORIGINATOR	19/10/90
27	WIRE	ORIGINATOR	19/10/90
28	WIRE	ORIGINATOR	19/10/90
29	WIRE	ORIGINATOR	19/10/90
30	WIRE	ORIGINATOR	19/10/90
31	WIRE	ORIGINATOR	19/10/90
32	WIRE	ORIGINATOR	19/10/90
33	WIRE	ORIGINATOR	19/10/90
34	WIRE	ORIGINATOR	19/10/90
35	WIRE	ORIGINATOR	19/10/90
36	WIRE	ORIGINATOR	19/10/90
37	WIRE	ORIGINATOR	19/10/90
38	WIRE	ORIGINATOR	19/10/90
39	WIRE	ORIGINATOR	19/10/90
40	WIRE	ORIGINATOR	19/10/90
41	WIRE	ORIGINATOR	19/10/90
42	WIRE	ORIGINATOR	19/10/90
43	WIRE	ORIGINATOR	19/10/90
44	WIRE	ORIGINATOR	19/10/90
45	WIRE	ORIGINATOR	19/10/90
46	WIRE	ORIGINATOR	19/10/90
47	WIRE	ORIGINATOR	19/10/90
48	WIRE	ORIGINATOR	19/10/90
49	WIRE	ORIGINATOR	19/10/90
50	WIRE	ORIGINATOR	19/10/90
51	WIRE	ORIGINATOR	19/10/90
52	WIRE	ORIGINATOR	19/10/90
53	WIRE	ORIGINATOR	19/10/90
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55	WIRE	ORIGINATOR	19/10/90
56	WIRE	ORIGINATOR	19/10/90
57	WIRE	ORIGINATOR	19/10/90
58	WIRE	ORIGINATOR	19/10/90
59	WIRE	ORIGINATOR	19/10/90
60	WIRE	ORIGINATOR	19/10/90
61	WIRE	ORIGINATOR	19/10/90
62	WIRE	ORIGINATOR	19/10/90
63	WIRE	ORIGINATOR	19/10/90
64	WIRE	ORIGINATOR	19/10/90
65	WIRE	ORIGINATOR	19/10/90
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67	WIRE	ORIGINATOR	19/10/90
68	WIRE	ORIGINATOR	19/10/90
69	WIRE	ORIGINATOR	19/10/90
70	WIRE	ORIGINATOR	19/10/90
71	WIRE	ORIGINATOR	19/10/90
72	WIRE	ORIGINATOR	19/10/90
73	WIRE	ORIGINATOR	19/10/90
74	WIRE	ORIGINATOR	19/10/90
75	WIRE	ORIGINATOR	19/10/90
76	WIRE	ORIGINATOR	19/10/90
77	WIRE	ORIGINATOR	19/10/90
78	WIRE	ORIGINATOR	19/10/90
79	WIRE	ORIGINATOR	19/10/90
80	WIRE	ORIGINATOR	19/10/90
81	WIRE	ORIGINATOR	19/10/90
82	WIRE	ORIGINATOR	19/10/90
83	WIRE	ORIGINATOR	19/10/90
84	WIRE	ORIGINATOR	19/10/90
85	WIRE	ORIGINATOR	19/10/90
86	WIRE	ORIGINATOR	19/10/90
87	WIRE	ORIGINATOR	19/10/90
88	WIRE	ORIGINATOR	19/10/90
89	WIRE	ORIGINATOR	19/10/90
90	WIRE	ORIGINATOR	19/10/90
91	WIRE	ORIGINATOR	19/10/90
92	WIRE	ORIGINATOR	19/10/90
93	WIRE	ORIGINATOR	19/10/90
94	WIRE	ORIGINATOR	19/10/90
95	WIRE	ORIGINATOR	19/10/90
96	WIRE	ORIGINATOR	19/10/90
97	WIRE	ORIGINATOR	19/10/90
98	WIRE	ORIGINATOR	19/10/90
99	WIRE	ORIGINATOR	19/10/90
100	WIRE	ORIGINATOR	19/10/90

- NOTE:
- VOLTAGE TAP WIRES FOR TAPS OA, 19B, AND THE HALF COIL TAP ARE #22 AWG TEFLON INSULATED.
  - THE REMAINING VOLTAGE TAP WIRES ARE #32 AWG TEFLON INSULATED.
  - TAP WIRES WITH THE SAME NUMBER AT EACH END SHOULD FORM A TWISTED PAIR (A-B AND C-D).
  - VOLTAGE TAP WIRE SHOULD FOLLOW THE CABLE TO WHICH THEY ARE SOLDERED UNTIL THEY MEET AND ARE TWISTED WITH THEIR "MATE".
  - COIL AS VIEWED FROM INSIDE.

Figure 2

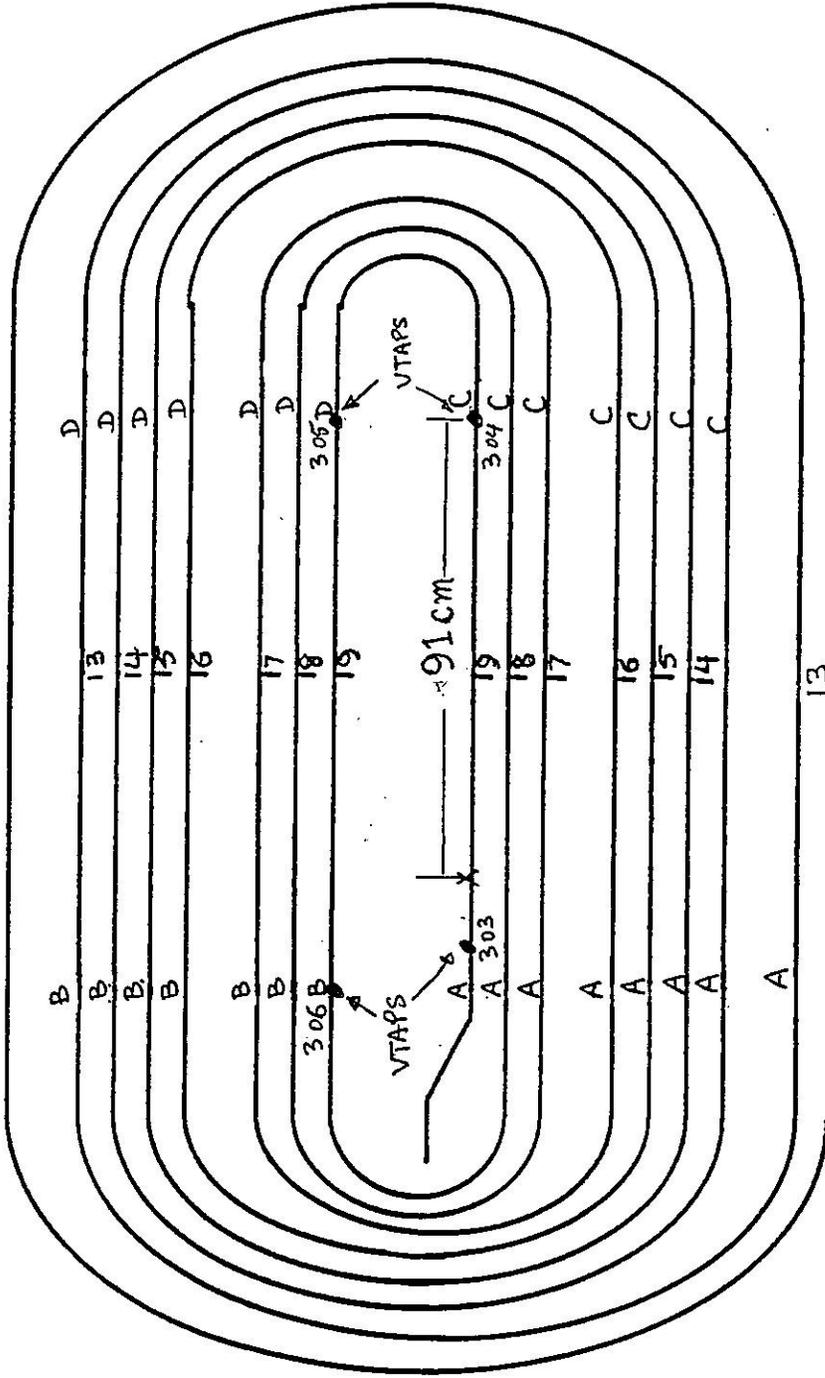
FEDERAL NATIONAL ACCELERATOR LABORATORY UNITED STATES DEPARTMENT OF ENERGY	
DS43XX VOLTAGE TAPS INNER COIL	
REV.	QTY.
NONE	B
0102-MB-263907	
CREATED WITH	USER NAME: SP10

INCHES METRIC



**Figure 3**

LOWER LEFT / UPPER RIGHT



LOWER RIGHT / UPPER LEFT

Figure 4

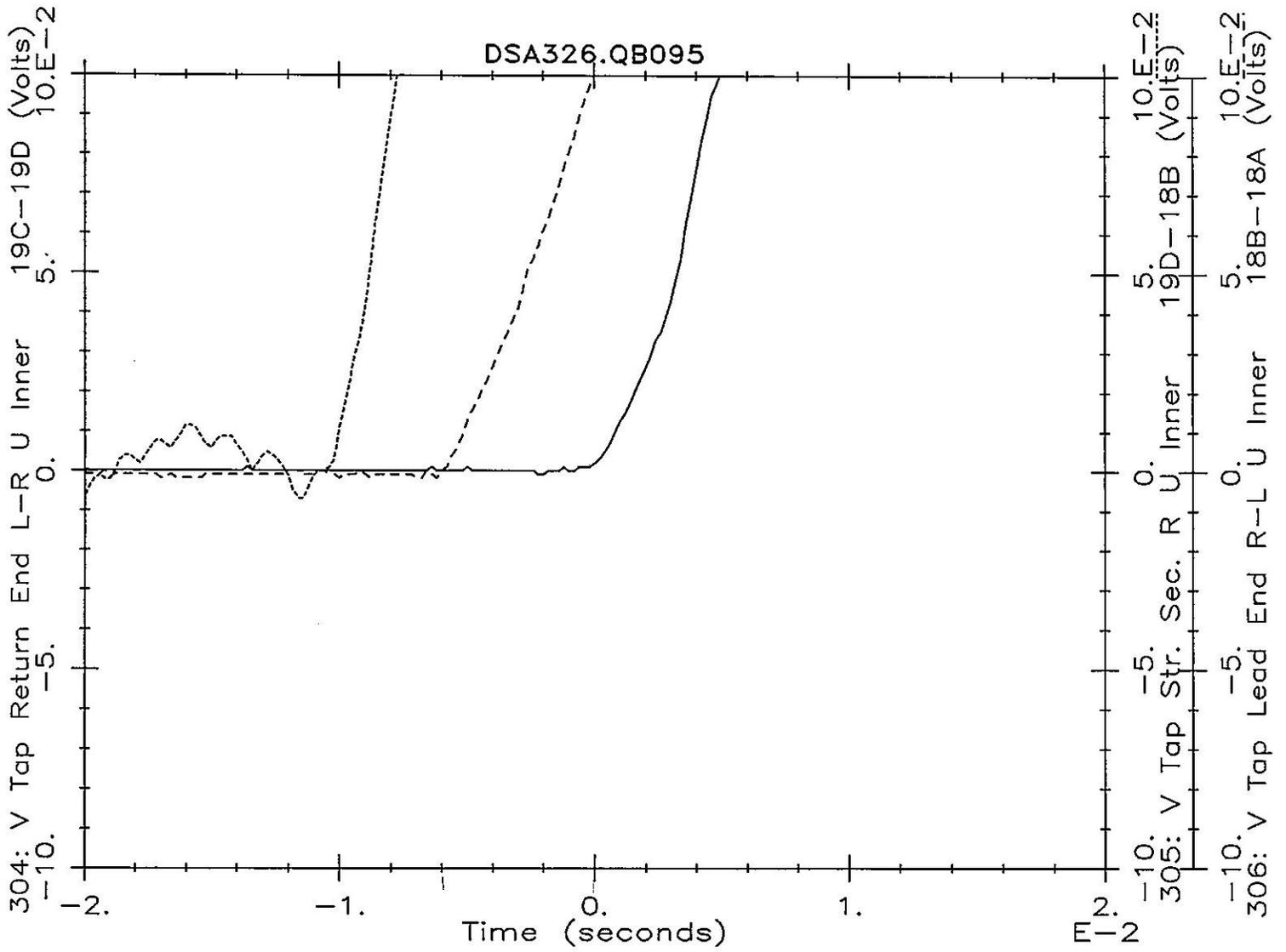


Figure 5: Typical plateau quench on non ramp-splice side of the coil

# SHORT DIPOLE RAMP RATE DEPENDENCE

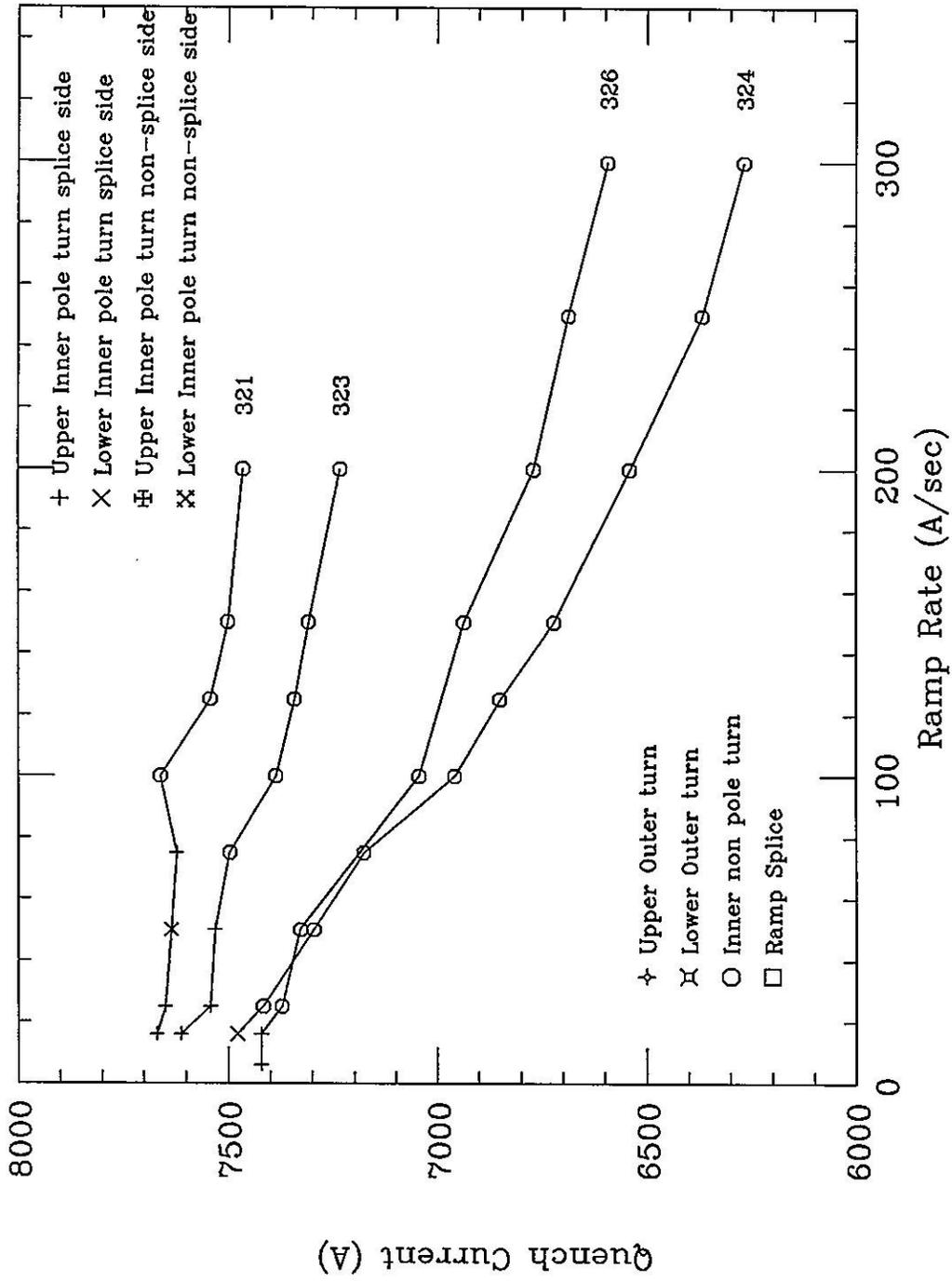
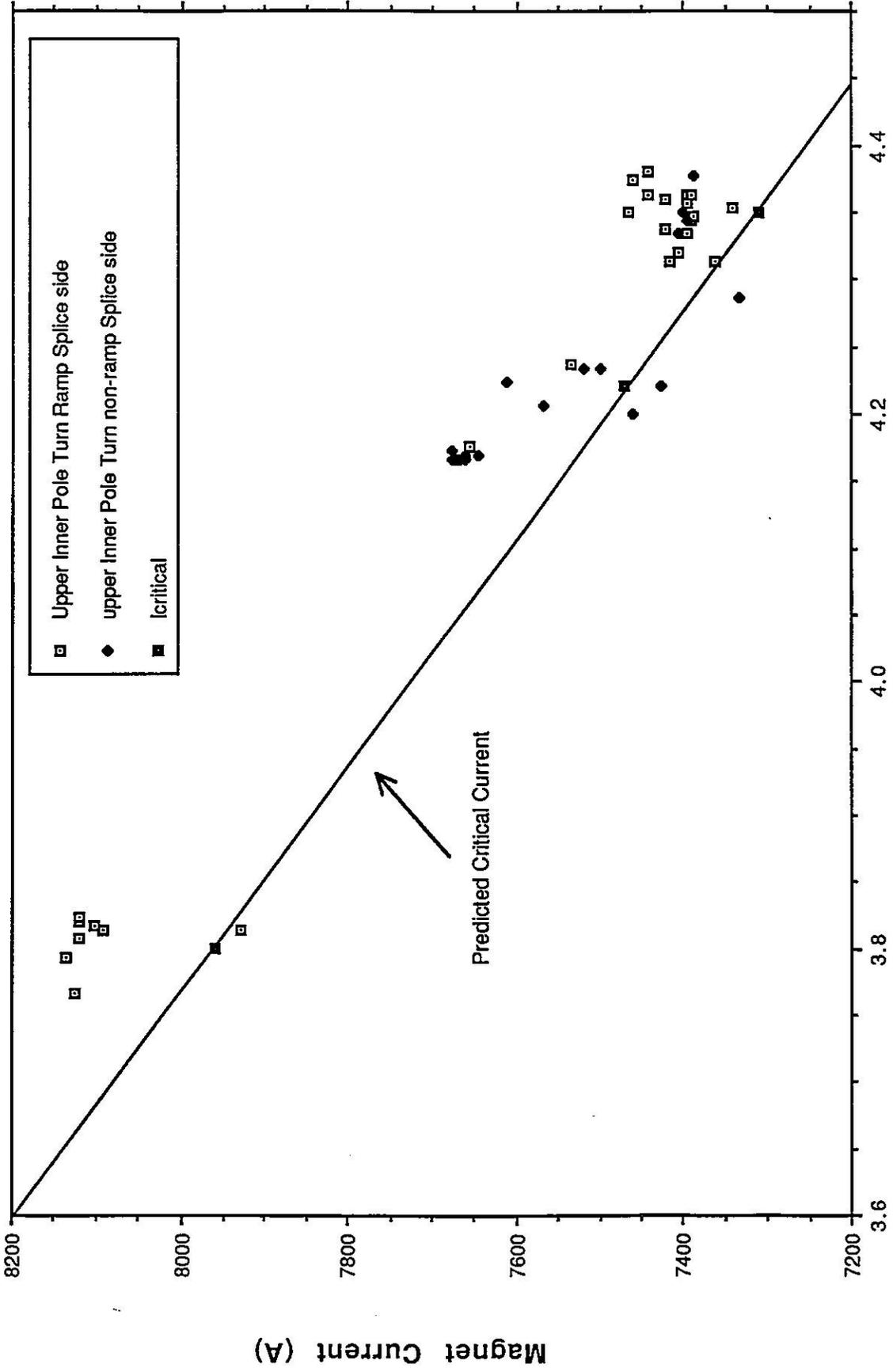


Figure 6

# DSA326 Quench Current vs Temperature



Temperature (K)

Figure 7