



TS-SSC 91-198  
10/15/91  
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### DCA311 End Loads from End Bell Welding

This note presents the end force data from the bullet gauges on DCA311 taken during the welding of the end bell to the end plate and during the loosening of the bullets after the welding was complete. The welding required 31 passes -- 1 root fusion pass and 31 filler passes. The bullets were initially loaded to 100 lbs each[1] and they were read out after each weld pass after the region had cooled to the specified inter-pass temperature[2]. This process spanned a period of about 50 hours.

The data are tabulated in Table I and plotted in Figure 1 (end force versus weld pass) and Figure 2 (end force versus time). When the weld crew broke either for the night or for lunch, measurements were taken both at the time the temperature reached the specified value and before work resumed. The latter reading is always higher because the structure has cooled more. These appear as steps at weld passes 8 (over night between 10/9 and 10/10), 16 (lunch on 10/10) 26 (over night between 10/10 and 10/11) and 31 (over night between 10/11 and 10/12 after the job was complete). The "connect-the-dots" lines in Figures 1 and 2 are broken at the points corresponding to the breaks in the welding operation. After weld pass 27 three sets of readings were taken and the increase with cooling is evident.

The end force increased only very slowly for the first 17 passes, then increased very rapidly for the next several passes, and then slowed down to a more moderate rate after pass 23. There is a significant decrease between passes 27 and 28 which is not understood. The final end force is, on the average, a few hundred pounds higher than on DCA310 despite changes[1] in the procedures.

The cause of the rapid increase, corresponding to about half the final load, between passes 17 and 23 is not known. Several hypotheses have been put forward. John Carson suggests that this corresponds roughly to the point at which as much filler had been added to the outboard (end bell) weld as was previously added to the in board (shell) weld. At this point the end plate is somewhat unstable and "pops" like a Belleville washer from bulging outwards to bulging inwards. It has also been suggested that the change in slope might be caused by a failure of some of the welders to follow the proper schedule. For example, there were changes of welders between, at least, passes 17 and 18 and between passes 19 and 20, corresponding to the periods of steepest slope. (Also the period of most rapid increase is on the day that Bill Higinbotham was at BNL and could not keep a close eye on the process.) My personal view is that it is undesirable that the end loads should be this sensitive to the details of how the ends are welded.

After the welding was complete the bullets were loosened until the end force was reduced to approximately 1000 lbs/bullet. The bullets were loosened

one at a time in increments of 1/32 and then 1/16 of a turn and the force on all the bullets was measured after each incremental turn of one bullet. These data are shown in Table II. The first block of columns indicates which bullet was loosened on each step. The second block shows the net displacement of each bullet in inches using the 16 threads per inch thread pitch. Next are the end forces and then the averages of the displacement and the end force. The same data are displayed in Figure 3 (force versus measurement number) and Figure 4 (force versus displacement). In Figure 3 the solid symbols show the forces and the open circles give the incremental turns of each bullet, indicating which bullet was turned for each measurement. The average force versus displacement is compared in Figure 5 with the previous measurements[1]. The data are normalized to the earlier measurements at 3000 lbs. The slope on unloading is much less steep than on loading. It is not understood why this is.

To reduce the load to 1000 lbs required loosening the bullets by between 1/2 (bullet 1) and 25/32 (bullet 2) turn. To limit the load at the uninstrumented lead end of DCA311 the set screws will first be loaded to a torque of 10 in-lb, corresponding to the initial 100 lbs load at the return end, and then backed out 1/2 turn, the minimum required at the return end. It is currently planned to follow the identical procedure at the return end of DCA312, which will allow a check of its efficacy.

#### REFERENCES

- [1] J. Strait, DCA311 and DCA312 Return End Coil Spring Rates, TS-SSC 91-194, 10/7/91.
- [2] W.A. Higinbotham, End Cap/Extension Assembly Installation, 0102-ES-292405 Rev. None, 7/24/91.

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### DCA311 Return End Bell Welding

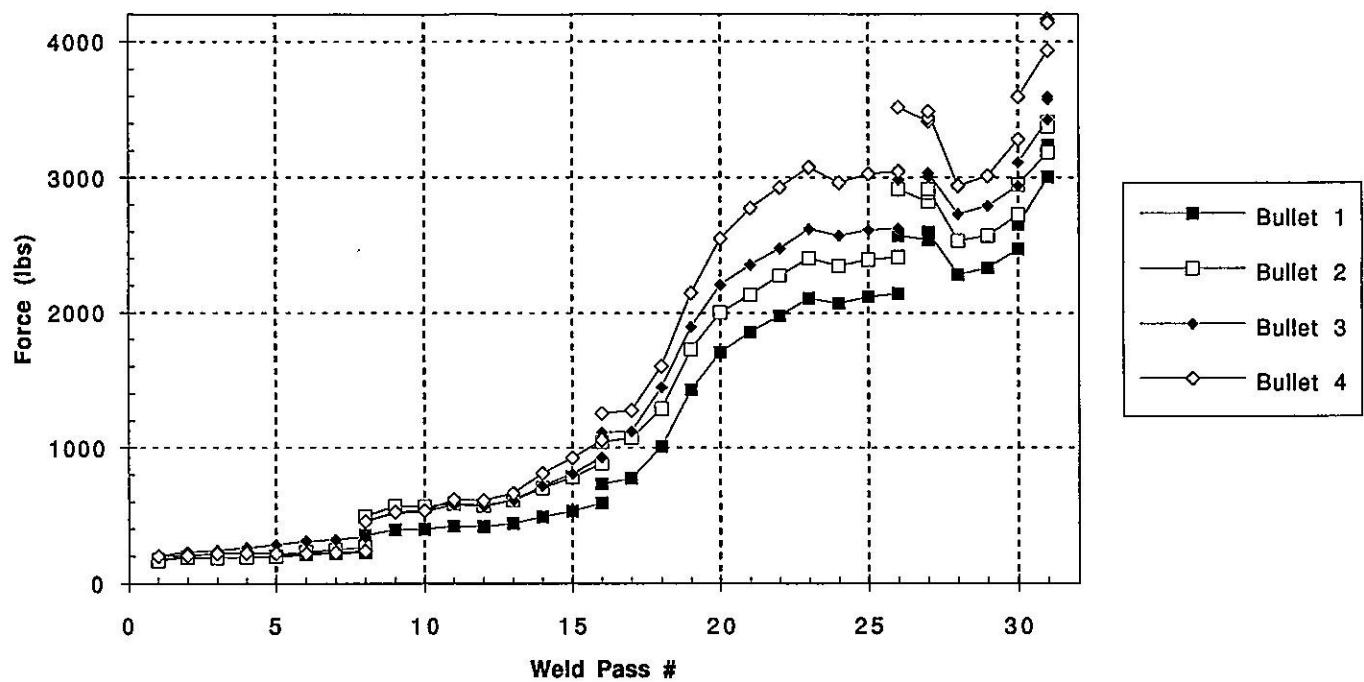


Figure 1

### DCA311 Return End Bell Welding

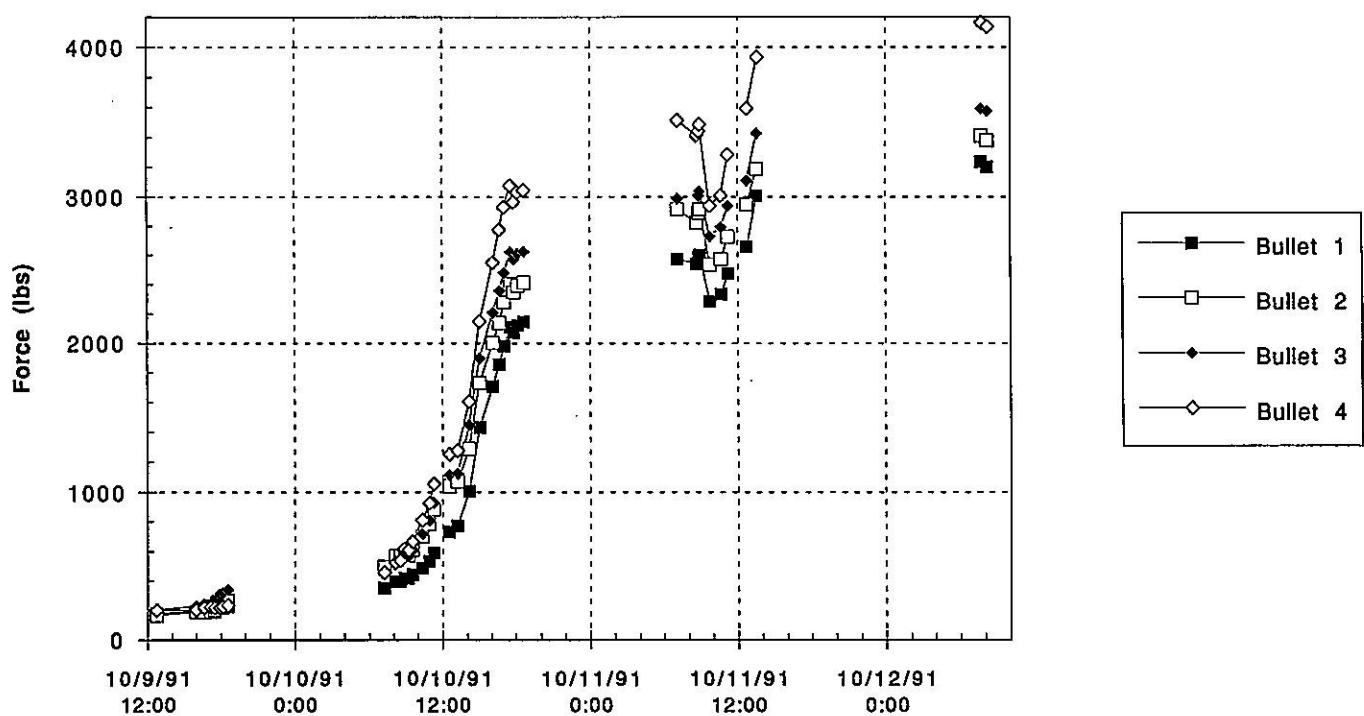


Figure 2

### DCA311 Bullets After End Bell Welding

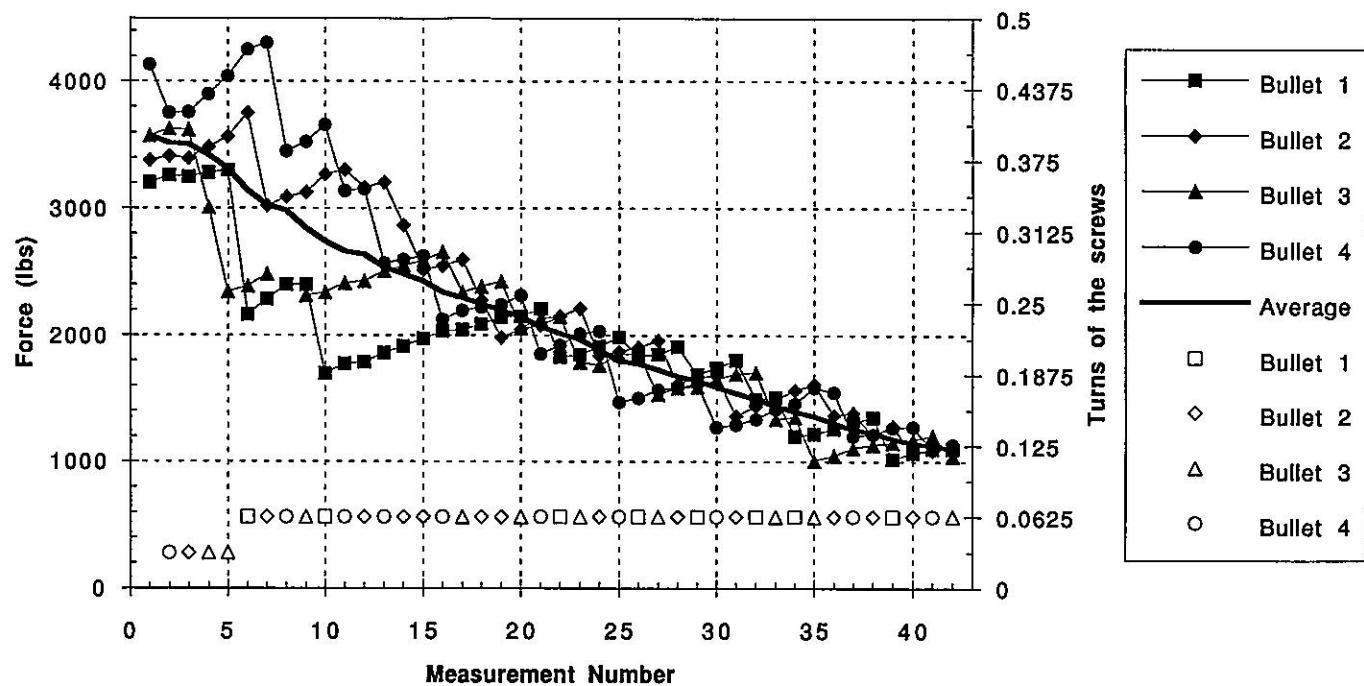


Figure 3

### DCA311 Bullets After End Bell Welding

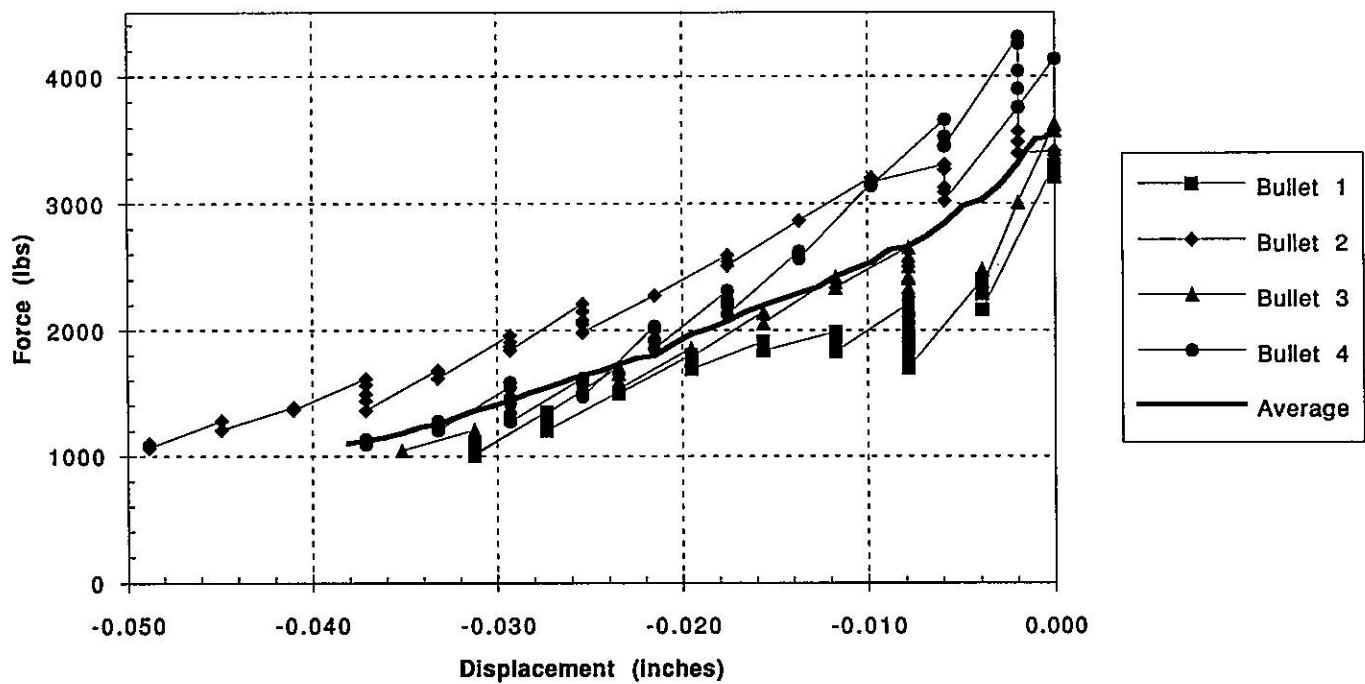


Figure 4

### Long Magnet End Force vs. Displacement

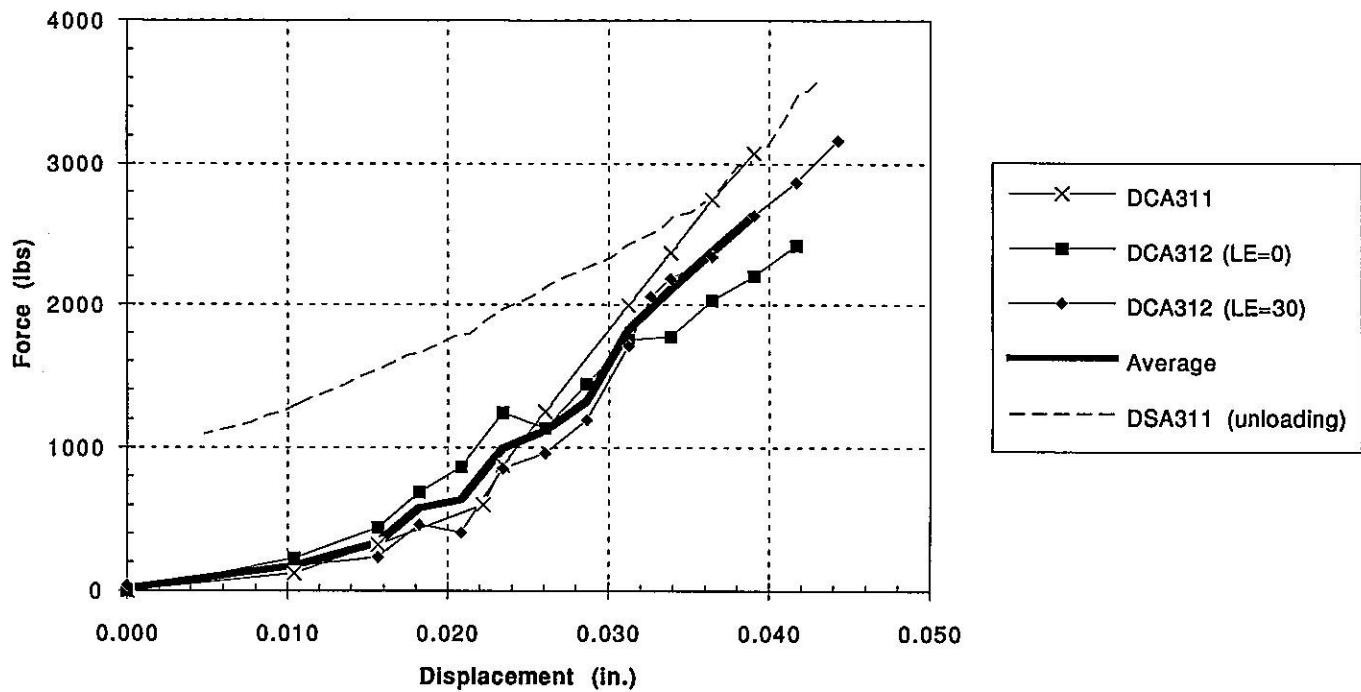


Figure 5