

Submitted to Physical Review Special Topic- Accelerator and Beams

SUPERCONDUCTING ACCELERATING STRUCTURES FOR VERY LOW VELOCITY ION BEAMS

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This paper presents designs for four types of very-low-velocity superconducting accelerating cavity capable of providing several MV of accelerating potential per cavity, and suitable for particle velocities in the range $0.006 < v/c < 0.06$. Super-conducting TEM-class cavities have been widely applied to CW acceleration of ion beams. SC linacs can be formed as an array of independently-phased cavities, enabling a variable velocity profile to maximize the output energy for each of a number of different ion species. Several laboratories in the U.S. and Europe are planning exotic beam facilities based on SC linacs. The cavity designs presented here are intended for the front-end of such linacs, particularly for the post-acceleration of rare isotopes of low charge state. Several types of SC cavities have been developed recently to cover particle velocities above $0.06c$. Superconducting four-gap quarter-wave resonators for velocities $0.008 < \beta=v/c < 0.05$ were developed about two decades ago and have been successfully operated at the ATLAS SC linac at Argonne National Laboratory. Since that time, progress in simulation tools, cavity fabrication and processing have increased SC cavity gradients by a factor of 3–4. This paper applies these tools to optimize the design of a four-gap quarter-wave resonator for exotic beam facilities and other low-velocity applications.

PACS numbers: 84.40.-x, 85.25.Am, 29.27.-a, 41.75.-i

1 Introduction

The most efficient production mechanisms for slow radioactive ions yield ions in a $1+$ or a $2+$ charge state [1]. In any future exotic beam facility (EBF), a post-accelerator must, to ensure maximum efficiency, be able to accept such low charge-to-mass ratio ions. Very efficient, low-charge-to-mass-ratio injectors have been proposed for this application [2-4]. This type of injector is based on a low-frequency, CW Radio Frequency Quadrupole (RFQ) injecting a very-low-velocity superconducting (SC) linear accelerator. The latter must be capable to accept and accelerate rare isotopes with charge-to-mass ratio in the range from $1/238$ to $1/6$. The SC linac is required after the gas stripping for $q/A \geq 1/66$ ions in the energy range from 75 keV/u to $\sim 1 \text{ MeV/u}$.

Superconducting four-gap quarter-wave resonators, also known as “fork” or inter-digital cavities, are a proven type of SC cavity for application in the energy range from $\sim 30 \text{ keV/u}$ to $\sim 1.0 \text{ MeV/u}$ [2]. At very low velocities, the greater length of 4-gap cavities compared with 2-gap cavities provides more voltage per cavity, while at the same time, the number of gaps remains small enough to provide a wide velocity acceptance,

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critical in an ion linac designed to accelerate a variety of ion species. Four-gap quarter-wave resonators (QWR) have been used since 1984 in the ATLAS Positive Ion Injector (PII), and presently operate at accelerating gradients of 3-4 MV/m [5]. Current state-of-the-art for TEM-class SC cavities, however, provides substantially higher gradients [6-7]. For several types of quarter-wave, half-wave and spoke-loaded resonators designed for the velocity range $0.1c$ to $0.7c$, residual rf surface resistances as low as $R_s \approx 5 \text{ n}\Omega$ and peak surface electric fields above 30 MV/m have been reproducibly attained. For the cavities discussed here, such performance corresponds to accelerating gradients above 10 MV/m. The “fork” cavities combined with SC solenoid or quadrupole focusing can provide ~ 4 MV/m real-estate accelerating gradients which are higher than accelerating gradients achievable with SC RFQ structures. For example, a recently commissioned SC RFQ [8] can provide from 1.9 to 2.8 MV/m accelerating gradients in the energy range from 37 to 540 keV/u. An advantage of “fork” cavities compared to RFQ structures is a capability for re-phasing to change the velocity profile and for the acceleration of various ion species to higher velocities.

In what follows, we present designs for several types of four-gap quarter-wave resonant cavity optimized for present state-of-the-art superconducting materials and processing techniques. In section 2 we establish cavity design goals by briefly discussing the design of a post-accelerator linac. In section 3, we detail the optimization of the electromagnetic design and in section 4, the mechanical design. Section 5 we discuss the results and conclusions.

2 Post-accelerator for radioactive ion beams

As we proposed in previous publications [2-4], a post-accelerator for radioactive ion beams (RIB) includes three main sections: a normally-conducting (NC) injector capable to accept ions with the lowest charge-to-mass ratio $q/A=1/238$ and accelerate up to ~ 75 keV/u, a superconducting (SC) linac for ions with charge-to-mass ratio $1/66$ or higher up to an energy of ~ 1 MeV/u and a higher energy SC linac including existing ATLAS to produce 10 MeV/u beams up to uranium. The main purpose of NC section comprised of three RFQs is to form low-longitudinal-emittance beams at bunching frequency of 12.125 MHz with an output energy of 75 keV/u. Between the RFQ sections a gas stripper increases the charge state of the heaviest ions to $q/A \geq 1/66$ prior to the injection into the SC section. The SC section CW accelerates the low-charge-state heavy ions to 1 MeV/u, requiring a total voltage ~ 70 MV.

We propose to base the SC section of injector linac on an updated and optimized design of already proven interdigital drift-tube SC niobium cavities. As we show below, such optimized cavities can provide typically ~ 2 MV of accelerating potential per cavity in this velocity range.

Very-low-charge-state beams, however, require stronger transverse focusing [2, 4], particularly at low velocities, than is used in existing SC ion linacs. For the charge states considered here ($q/A = 1/66$) the proper focusing can be reached by the help of SC quadrupoles. The linac FODO lattice will consist of a SC quadrupole following each superconducting four-gap cavity. The FODO lattice is tuned to provide phase advance close to 90° per period to mitigate coupling transverse and longitudinal motions

and avoid noticeable growth of longitudinal emittance as discussed in [2,4]. Three types of four-gap QWRs operating (conservatively) at 8 MV/m accelerating field can form the required linac as an array of 38 cavities operating at -20° synchronous phase, with the voltage gain per cavity along the linac shown in Fig. 1. Such an array would form a very compact and cost-effective RIB injector, which would require just four cryostat vessels.

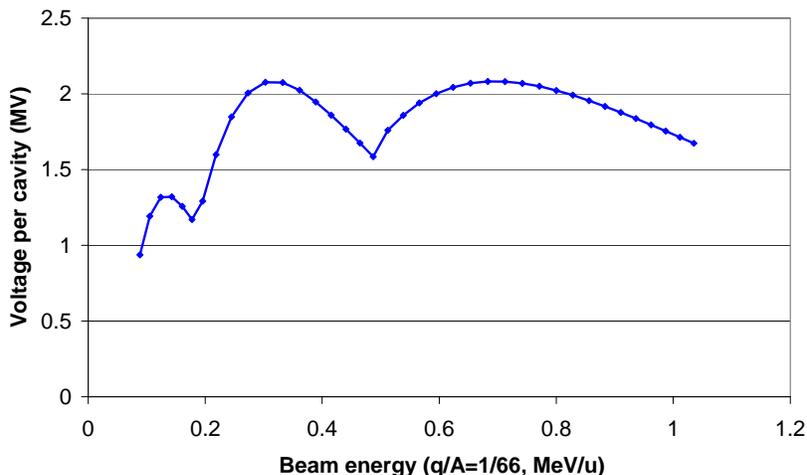


FIG. 1. Voltage gain per cavity as a function of ion beam energy, $q/A=1/66$, Injection energy is 75 keV/u.

Table 1 lists the basic parameters of four different types of four-gap quarter-wave resonators (four-gap QWR). Type I, II and III are intended for use in a low charge-to-mass ratio ($q/A \geq 1/66$) post-accelerator. The type-IV cavity is intended for a multi-ion, multiple-charge-state driver linac for the EBF.

3 Electromagnetic design optimization

To achieve 8-10 MV/m of accelerating gradient in the proposed 4-gap resonators, the following

Table 1. Basic parameters of 4-gap QW resonators for the EBF at ANL

Parameter	Type-I	Type-II	Type-III	Type-IV
Frequency (MHz)	48.5	48.5	72.75	57.5
β_G	0.017	0.026	0.038	0.031
Aperture diameter (cm)	2.0	2.0	2.0	3.0
Number of cavities required for the AEBL	6	12	20	3

criteria were chosen:

- Apply the fabrication technology of SC TEM cavities as developed at ANL for the construction of QWRs. A further design constraint was to minimize prototyping costs for the new four-gap designs by using, to the extent possible, dies previously constructed for 2-gap QWR cavities.
- Minimize the ratio of the peak surface electric field to the accelerating field E_{PEAK}/E_{ACC} .
- Minimize the peak magnetic field.
- Maximize the cavity geometrical factor and shunt impedance.

The code CST MWS 2006B [9] was used as the main electromagnetic design tool. This version provides more accurate eigenfrequencies and surface fields for resonators with complex geometries than previous versions. The Fast Perfect Boundary Approximation (FPBA) available in MWS enabled us to use imported cavity geometries built by the ProE software package [11].

For comparison and a double check on results, another software package, ANALYST, from Simulation Technology & Applied Research, Inc. [12] was also used. Generally, MWS simulations are faster than ANALYST for a similar number of mesh-points. However, ANALYST can achieve higher speeds by running on 32 processors.

3.1. Optimization of cavity parameters

Current state-of-the-art cavities are fabricated from ($RRR \geq 250$) bulk niobium, in the form of ~ 3 mm thick sheets. Die forming and EB welding can produce nearly any desired geometry. A helium vessel is formed between an Nb cavity and a stainless steel (SS) jacket [13].

We started with cavity Type II (from Table 1). A schematic design of the four-gap QWR is shown in Fig. 2. The design of the central drift tube differs from earlier 4-gap cavities, and is now formed as a hollow horizontal bar, allowing direct cooling by liquid helium.

The mechanical stability of a QWR is primarily defined by the length of the central conductor, or stem. The outer diameter of the drift tubes and the stem diameter define the length of the stem and the overall cavity height required for a given frequency.

E_{PEAK} and B_{PEAK} have been minimized by varying the main cavity parameters shown in Fig. 2. To reduce prototype fabrication cost by using the existing dies, the diameter of the cavity $D0$ and stem $D1$ have been chosen as for previously built QWRs [7].

First, the ratio E_{PEAK}/E_{ACC} was minimized by varying the following parameters (shown in Fig. 2):

1. The outer diameter of the Drift Tubes (DT) $D3$.

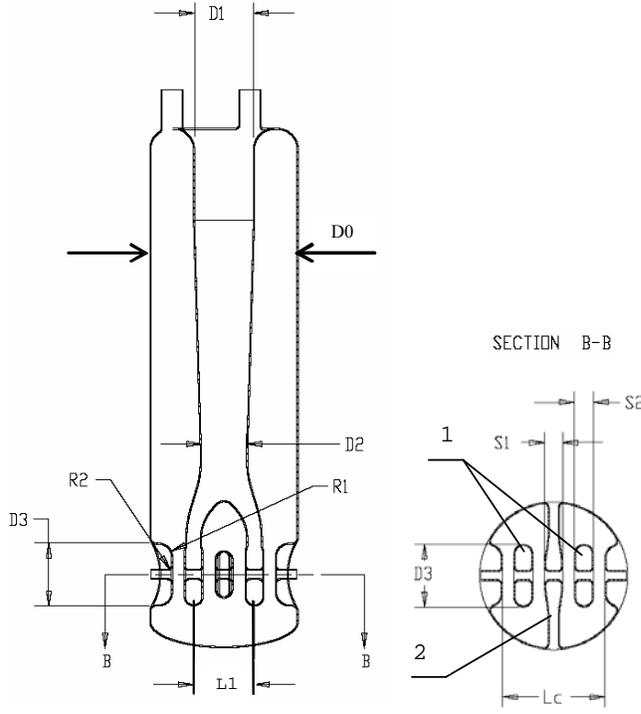


FIG. 2. Main parameters of the cavity to be varied in optimization procedure. 1 – intermediate DTs, 2 – horizontal cross-bar.

final shape of the bar is shown in Fig. 2. Ramping of the bar cross-section along the horizontal axis reduces peak electric surface field.

5. The blending radius $R2$ is optimized.

Secondly, B_{PEAK} was minimized by varying the following parameters (shown in Fig. 2):

1. In early trials, the loft connection between the stem and intermediate drift tubes had a cylindrical cross section. The smallest cylinder radius occurs on the drift tube surface and equal to the half of the drift tube thickness $S2$. The latter is optimized to obtain the lowest E_{PEAK} . The cylinder shape was changed to a racetrack shape, which significantly reduced local B_{PEAK} .

2. The diameter $D2$ of the stem cone (see Fig. 2) was optimized. A conical shape for the stems has been chosen to minimize multipacting, in accord with previous experience with QWR cavities.

The above optimization procedure was iteratively repeated to minimize E_{PEAK} and B_{PEAK} , while keeping the cavity geometrical factor G and the ratio of shunt impedance to quality factor R/Q_0 high.

The shapes of cavity types I, III and IV were obtained by modifications of the type-II geometry applying the following procedures:

2. The thickness of the DTs and distance $L1$. These were varied while maintaining design β_G unchanged as shown in Table 1. Intermediate DTs are attached to the stem through the “fork” therefore their thickness ($S2$) also effect peak magnetic field. During the optimization procedure, we have tried to apply different shapes of the cross-section of the intermediate DTs in horizontal plane. Instead of “racetrack” shape as is shown in Fig. 2, a trapezoid shape has been also applied. However, the latter reduces the blending radius and results in a higher peak surface electric field.

3. The blending radius $R1$ is maximized to be equal to the half of the drift tube thickness.

4. Modification of the horizontal cross-bar which forms the central DT. The

- Type-I: Simple scaling of all dimensions except the height as a ratio of geometrical beta which is equal to 0.017/0.026. The cavity (and stem) height were adjusted to arrive with the correct frequency.
- Type-III: a higher velocity was obtained by increasing the frequency by reducing the stem length to obtain a frequency of 72.75 MHz, the 6th harmonic of the bunching frequency, while the drift tubes and “fork” section of the cavity were kept the same as for the type-II cavity.
- Type-IV: Increasing the distance between the intermediate drift tubes L_I and cavity length L_c . to provide slightly higher β_G and adjusting the cavity height to obtain 57.5 MHz resonant frequency.

The cross-sections of all four MWS models in (y, z) plane are shown in Fig. 3. The optimized electromagnetic parameters of all cavity types are summarized in Table 2. For the comparison, we also list parameters of an earlier four-gap 48.5 MHz cavity design presently used in the existing ATLAS SC linac. In the optimized cavities, both the peak electric and magnetic field are substantially lower than for ATLAS cavity.

Figure 4 shows, for the type-II cavity, the first trial and the final geometry of the cavity, together with the distribution of the surface electric field.

Table 2. Main electrodynamic parameters of four-gap QWRS given for $E_{ACC}=1$ MV/m.

Parameter	Units	ATLAS	Type-I	Type-II	Type-III	Type-IV
E_{PEAK}	MV/m	5.04	3.76	3.41	3.48	3.61
B_{PEAK}	Gauss	117	42	43	55	48
Length, L_c	cm	24.638	17	26	26	26.4
W	mJ	221	72	150	118	149
G	Ω	13.8	11.5	18.1	25.1	20.9
R/ Q_0	Ω	900	1309	1486	1254	1298
β_G		0.025	0.017	0.026	0.038	0.031
Height	cm	110.5	139.5	131.3	80.8	107.3
Diameter	cm	30.48	23.54	37.0	37.0	37.0

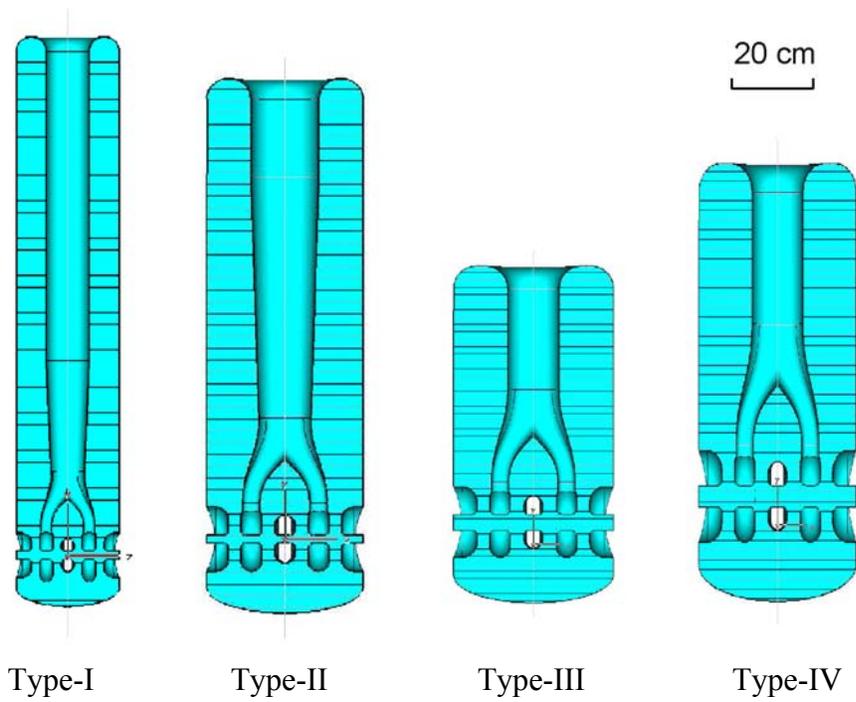


FIG. 3. MWS models of four types of 4-gap quarter-wave resonators.

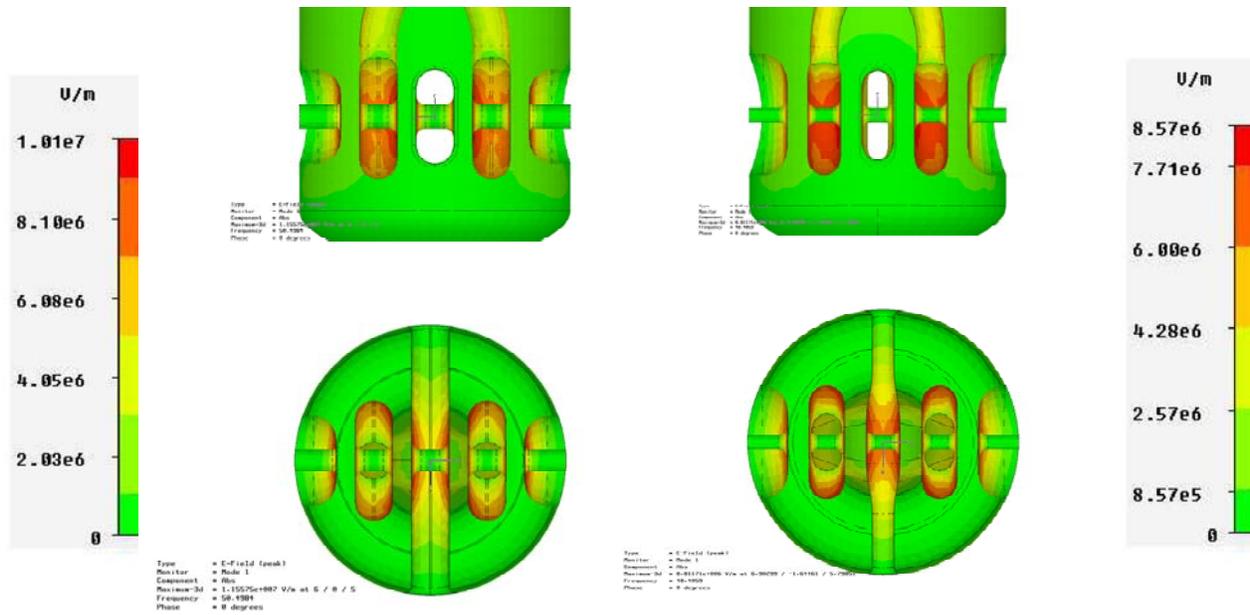


FIG. 4. Surface electric field distribution in (x, z) and (y, z) planes. The preliminary design (on the left) and optimized design (on the right).

3.2. Comparison of MWS and ANALYST results

Peak surface fields in a resonant cavity of complex shape are quite sensitive to the parameters of computer model and simulation technique. Two commercial codes, MWS and ANALYST, have different algorithms to solve Maxwell equations. We have applied the latest versions of both codes with different mesh sizes to compare the simulation results of type-II cavity. The results are summarized in Table 3. It can be seen that the ANALYST results obtained on 1.6 million mesh elements converged to the MWS results. Points A and B indicate

locations of the peak surface electric field. Even with relatively large number of mesh points, MWS produces isolated regions with suspiciously and anomalously high peak surface fields while ANALYST achieves a more continuous approximation of the surface fields with similar number of mesh points.

The computation speed of MWS is much faster than ANALYST: therefore we used the parallel version of ANALYST running on the ANL BG/L supercomputer. Using the parallel version of ANALYST was

important for confirming the MWS simulations. Figure 5 shows the electric field contours in (y, z) plane obtained by both MWS and ANALYST codes. It may be noted that the field approximation near the rounded surfaces is more accurate in ANALYST code which uses the finite element method. The ANALYST software is also more adequate for study of multipacting phenomena in resonators and was applied to identify multipacting in the space between the stem and housing cylinder. This region is of particular interest due to its coaxial shape. In our multipacting simulation, we use enhance counter

function ($e_n(|F|) = \sum_{j=1}^{N_0} N_n(x_0^j)$) to describe the total number of electrons, including original and the secondary electrons emitted from the wall due to the impacts. x_0^j is the initial position for the j^{th} electron.

The total number of secondary electrons due to a single electron launched after n impacts is given by $N_n(p_0) = \prod_{k=1}^n \delta(x_k, E_k)$, where $\delta(x_k, E_k)$ is the ratio of total electrons emitted from the wall to the total number of electrons bombarding the wall at location x_k and at energy level E_k .

Figure 6 show the electron trajectories after 10 impacts between the surfaces of the stem and housing cylinder. Figure 7 shows enhance counter functions after 5, 10 and 20 impacts. It is clear that enhance counter function diminished as the number of impacts grows. This figure indicates there are no multipacting activities over the stem area.

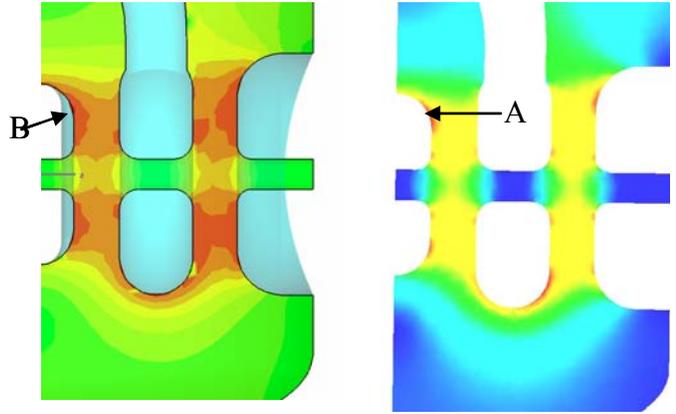


FIG. 5. Electric field contours in (y, z) plane simulated with MWS with 2 million mesh-points (on the left) and ANALYST with 1.6 million mesh elements (on the right).

Table 3. Comparisons of type-II cavity simulations performed with MWS and ANALYST. All data are given for $E_{ACC}=1$ MV/m.

Parameters	Units	MWS (PBA mesh)		ANALYST	
Mesh-points		390K	2M	68K (h1.5)	1.6M (h1.5)
E_{PEAK}	MV/m	3.48	3.41	4.12	3.47
B_{PEAK}	Gauss	40.2	40.5	65	42.3
G	Ω	17.7	18.1	18.1	16.9
R/ Q_0	Ω	1473	1486	1330	1463
f_0	MHz	48.66	48.41	48.88	48.52

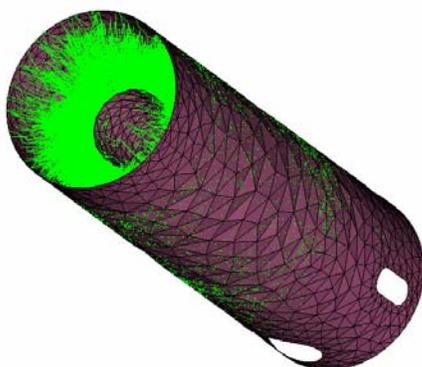


FIG. 6 Electron trajectories between surfaces of the stem and housing cylinder

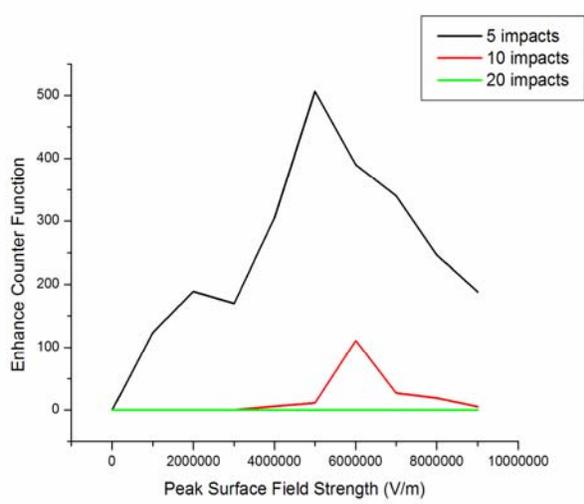


FIG. 7 Enhance Counter Functions after 5, 10 and 20 impacts

4 Structural analysis



FIG. 8. ProE model of the type-II cavity.

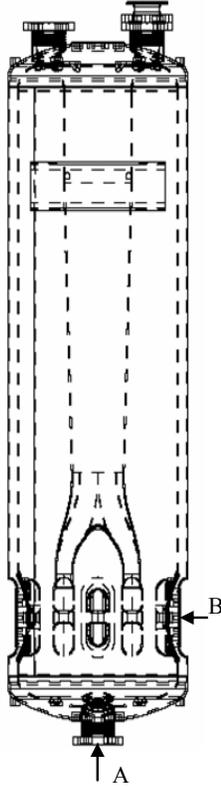


FIG. 9. Cross section of the type-II cavity in the SS jacket.

The frequency and phase stability of high-Q SC cavities are extremely sensitive to mechanical deformation [14]. For CW applications, the dominant driver of mechanical deformations is microphonic vibrations due to various external sources. In QWRs, ambient microphonic noise can also excite low-frequency mechanical resonances of the cavity [15]. One source of microphonics in operation at 4.2K is that RF losses cause appreciable boiling in the liquid helium, resulting in small fluctuations in the local helium pressure [16]. The reduction of the cavity sensitivity to microphonic noise is crucial in CW low-current operation of SC cavities when beam loading is negligible.

Several techniques have been developed to control the cavity RF phase in the presence

of microphonic-noise [14]. Effective damping techniques have been proposed and implemented to damp the mechanical resonance using passive absorbers of energy of mechanical oscillations [15]. Structural strengthening of the cavity during the mechanical design to minimize the resonant frequency sensitivity to the helium pressure is an effective measure to control microphonics [16].

As part of the design process, we performed detailed mechanical

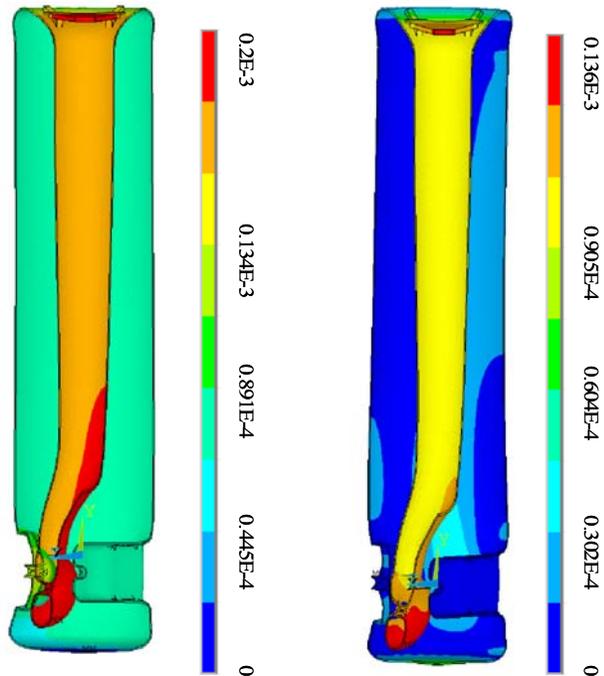


FIG. 10. ANSYS results of deformed geometries for the case 1 (left) and case 2 (right). Only $\frac{1}{4}$ of the cavity is shown.

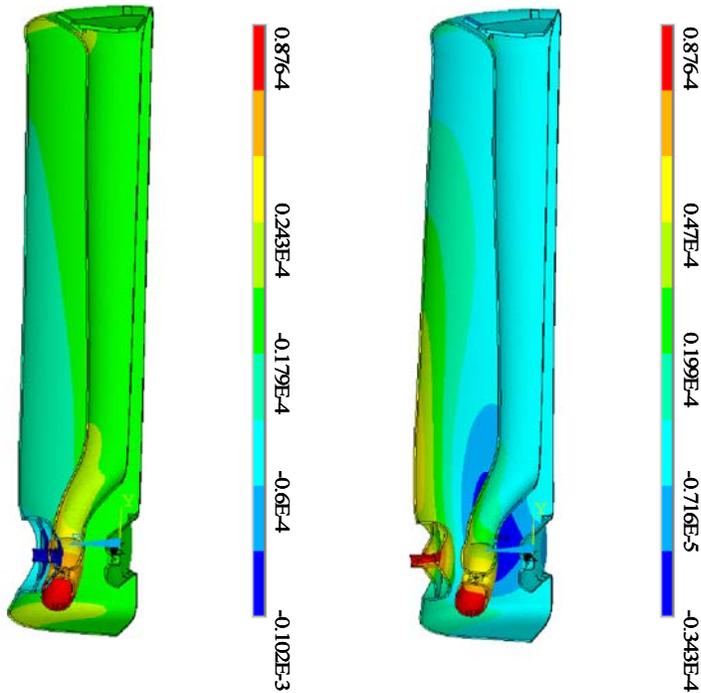


FIG. 11. ANSYS results of the cavity deformations in Z direction along the beamline due to the helium pressure (left) and the combined effect of the helium pressure and mechanical tuner with pulling force (right). Only $\frac{1}{4}$ of the cavit is shown.

large. To reduce this frequency shift, the cavity design was been modified by structurally enhancing the connection of the stem to the cylinder, and by stiffening the horizontal cross-bar. To find the effect of helium pressure on the cavity frequency, two cases were studied: (1) the cavity fixed at one point (point A in Fig. 9) and (2) the cavity fixed at the beampipe surface, surface B (see Fig. 9). The ANSYS results are shown in Fig. 10 and summarized in Table 4. The maximum displacement of the cavity walls is 200 μm and 136 μm for the first and second cases respectively. As is seen from Table 4, the frequency shift is between -13 kHz to -5 kHz for the two cases being studied. During the mechanical design of the cavities, the cavity sensitivity to the helium pressure will be further decreased by further stiffening of the stem support. In addition, the stainless steel jacket will also reduce the sensitivity of the cavity resonant frequency to the helium pressure.

A mechanical tuning mechanism will be applied symmetrically from both sides of the cavity to the surface B as shown in Fig. 9. In ANSYS simulations of the tuner effect, the cavity is fixed at the bottom point A (Fig. 9). A pulling force of 1120 N was applied over the 26 mm diameter of the aperture pipe. The deformed geometries of the cavity are shown in Fig. 11, and frequency shifts are listed in Table 5.

modeling of the type-II cavity. A detailed ProE model of the type-II cavity is shown in Fig. 8. We have performed simulations of the cavity with two symmetry planes using ANSYS multiphysics [17] software package to study the effects of a) a frequency shift due to the helium pressure and b) a frequency response to an external slow-tuning device. The structural analysis of the cavity shown in Fig. 9 under 10^5 Pa helium pressure has been performed using both ProE and ANSYS software packages. Both software packages show significant displacement of the stem, ~ 0.5 mm, in vertical direction. As a result the frequency shift can reach to -27 kHz, which was unacceptably

Sensitivity of the cavity frequency to the tuner force is ~ 12.5 Hz/N. As can be seen from Tables 4 and 5, the applied force approximately compensates frequency shift due to the helium pressure.

Table 4. ANSYS simulation results for frequency detuning due to 10^5 Pa helium pressure.

Mode number	1 (operational)
Initial frequency (MHz)	48.297
Frequency shift, case 1 (kHz)	-13
Frequency shift, case 2 (kHz)	-5

Table 5. ANSYS simulation results for frequency detuning due to the effect of the tuner.

Mode number	1 (operational)
Initial frequency (MHz)	48.297
Frequency shift, pressure is applied (kHz)	1
Frequency shift, no pressure (kHz)	15

5 Discussion and Conclusions

Four-gap interdigital quarter wave superconducting cavities can provide effective and efficient means of accelerating ion beams in the velocity range from $0.012c$ to $0.05c$. Earlier versions of these types of cavities were developed, built and operated in the Argonne heavy-ion linac ATLAS. The ATLAS four-gap QWRs built in 1980s are operated typically at ~ 3 MV/m accelerating field which corresponds to $E_{PEAK} \approx 15.1$ MV/m and $B_{PEAK} \approx 360$ G.

Extensive optimization of four-gap cavity mechanical and electrodynamic properties has been performed using the most recent versions of modern three-dimensional software tools. As a result of these studies, peak magnetic and electric surface fields have been significantly reduced to $E_{PEAK} \approx 3.4$ MV/m and $B_{PEAK} \approx 43$ G per 1 MV/m of the accelerating field. The reduction of peak electric field has been achieved by optimization of the drift tube and horizontal bar shapes. Similarly, magnetic field has been reduced by optimization of the conical stem and lofts connecting the stem to the drift tubes. With modern fabrication technology and cavity processing techniques, peak surface electric fields can be increased to ~ 32 - 35 MV/m which have been demonstrated in numerous prototype TEM-class cavities. Therefore optimally designed four-gap cavities, using modern construction and processing techniques, can provide ~ 10 MV/m accelerating fields, or more than 2 MV of accelerating voltage per cavity. The accelerating gradients provided by four-gap cavities are higher by the factor 3 and 4 compared to the existing accelerators in similar velocity range [8, 18].

Effective use of 3D design and analysis codes allows us to skip prototyping of all types of cavities. Our intention is to build a prototype cavity of type II that can be later used in the accelerator. Main

purpose of cavity prototyping is to resolve engineering issues and to understand the production cost of these cavities.

There are several other issues related to the high-performance cavity design. Reduction of the frequency sensitivity to the variation of the helium pressure is crucial for application in CW low-current accelerators. This parameter has been reduced by the enhancement of the stem connection to the cylindrical body and by strengthening of the horizontal bar which forms the middle drift tube.

High-performance high-gradient four-gap cavities can significantly reduce the number of cavities required to provide ~ 70 MV accelerating voltage for the low charge state post-accelerator. The optimized design, combined with recently developed cavity fabrication and cleaning techniques, will reduce the cost of proposed accelerators for any future EBF project.

6 Acknowledgements

This work was supported by the U.S. Department of Energy, Office of Nuclear Physics and High Energy Physics, under Contract No. DE-AC-02-06CH11357 and No. DE-AC02-07CH11359.

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