Feasibility Study of Nb₃Al Rutherford Cable for High Field Accelerator Magnet Application

R. Yamada, A. Kikuchi, G. Ambrosio, N. Andreev, E. Barzi, C. Cooper, S. Feher, V.V. Kashikin, M. Lamm, I. Novitski, T. Takeuchi, M. Tartaglia, D. Turrioni, A. P. Verweij, M. Wake, G. Willering and A. V. Zlobin

Abstract— Feasibility study of Cu stabilized Nb₃Al strand and **Rutherford cable for the application to high field accelerator magnets are being done at Fermilab in collaboration with NIMS.** The Nb₃Al strand, which was developed and manufactured at **NIMS in Japan, has a non-copper Jc of about 844 A/mm2 at 15 Tesla at 4.2 K, a copper content of 50 %, and filament size of** about 50 microns. Rutherford cables with 27 Nb₃Al strands of **1.03 mm diameter were fabricated and tested. Quench tests on a short cable were done to study its stability with only its self field, utilizing a high current transformer. A pair of 2 meter long Nb3Al cables was tested extensively at CERN at 4.3 and 1.9 K up to 11 Tesla including its self field with a high transport current of 20.2 kA. In the low field test we observed instability near splices and in the central region. This is related to the flux-jump like** behavior, because of excessive amount of Nb in the Nb₃Al strand. There is possibility that the Nb in Nb₃Al can cause instability **below 2 Tesla field regions. We need further investigation on this problem. Above 8 Tesla, we observed quenches near the critical surface at fast ramp rate from 1000 to 3000 A/sec, with quench velocity over 100 m/sec. A small racetrack magnet was made using a 14 m of Rutherford cable and successfully tested up to 21.8 kA, corresponding to 8.7 T.**

*Index Terms***— Nb3Al, Rutherford Cable, Superconductivity**

I. INTRODUCTION

HE $Nb₃Al$ strand has been known to withstand higher T HE Nb₃Al strand has been known to withstand higher stress than Nb₃Sn strands, but its application has been limited, because it was difficult to make a long Cu stabilized $Nb₃Al$ strand. Recently stabilized $Nb₃Al$ strands were made by electroplating copper at the National Institute of Material Sciences in Japan, and stabilized $Nb₃Al$ strands over

Manuscript received August 29, 2006. This work is supported by U.S. Department of Energy.

R. Yamada, G. Ambrosio, N. Andreev, E. Barzi, C. Cooper, S. Feher, V.V. Kashikin, I. Novitski, M. Tartaglia, D. Turrioni, and A.V. Zlobin are with Fermi National Accelerator Laboratory, Batavia Illinois, 60510 USA (phone: 630-840-3660; fax: 630-840-3369; e-mail: yamada@ fnal.gov).

A. Kikuchi and T. Takeuchi are with National Institute for Material Science (NIMS), 1-2-1 Sengen, Tsukuba, Ibaraki 305-0047, Japan.

A.P. Verweij and G. Willering are with CERN, European Organization for Nuclear Research, European Laboratory for Particle Physics: CH-1211 Geneve 23, Switzeland.

M. Wake is with High Energy Accelerator Research Organization, 1-1 Oho, Tsukuba, Ibaraki 305-0801, Japan.

1 km were made. The detailed characteristic parameters and production process for this strand are reported [1].

Recently Nb₃Al strands have been used in fusion projects in the field range of 13 Tesla as CICC cables [2], and are being tested for the possible application as the inner coil of the 1 GHz NMR [3]. It is also being considered for use in accelerator magnets [4]-[5].

We have made two different Rutherford cables utilizing two different Cu stabilized $Nb₃Al$ strands. In this paper the $Nb₃Al$ strand, called F1, is briefly described and the test results of Rutherford cables are presented.

II. RHQT (RAPID-HEATING QUENCHING AND TRANSFORMATION) NB₃AL STRAND

The present $Nb₃Al$ strand is made by the 'Jelly Roll' method. The alternate foils of Nb and Al (composition: 75at%Nb-25at%Al) are wrapped around a Nb rod, and on top of it another Nb foil is wrapped. 144 monofilaments are stacked around the central Nb core and placed into a Nb can making a billet. This assembly is hydrostatically drawn into a thin multifilament wire [1].

The Nb/Al multifilament wire is Ohmic-heated rapidly to a very high temperature $(\sim 1900^{\circ}C)$, and then quenched into a molten Gallium bath at \sim 50 $^{\circ}$ C. The ductility of the whole composite is ensured to make a Rutherford cable. The cold reduction of its diameter is essential to increase its eventual Jc value. Next the surface of the precursor strand is Cu ion-

plated under vacuum, and electroplated with Cu to add the thick copper stabilizer [1]. The cross section of the 1.03 mm diameter strand is shown in Fig. 1.

After the Rutherford cabling operation, the strand is transformed into A15 phase by heating at 800°C for only 15 hours.

Fig. 1. 1.03 mm Nb3Al strand: F1.

The non-copper J_c of 844 A/mm² at 15 Tesla at 4.2 K is achieved at an I_c of 352 A. It is expected I_c will be 420 A at 15 Tesla at 1.8 K. The Nb matrix/Nb₃Al ratio is 0.6 and the Cu/non-Cu ratio is 1.04. The detailed description of the tested strand's characteristics is presented at this conference [6].

III. NB₃AL RUTHERFORD CABLING

Using 1 km of F1 Nb₃Al strand we made about 30 meters of 27 strand Rutherford cable, including a 25 meter cable of low compaction (82.5 %) cable. Its cross section is shown in Fig. 2. The cable is of rectangular shape, 14.2 mm wide, 2.0 mm high, and with 15 degree lay angle. In this cable there is a slight separation of copper from the Nb₃Al core at the edge strands. We also made 5 meters of Rutherford cable with high compaction of 89.1 %. At this compaction the central strands' copper is well compressed, but the edge strands have their stabilizing copper more squashed. In general the $Nb₃Al$ cores have kept almost the original round shape, because of its Vicker's hardness of 420. But the electroplated soft copper with a Vicker's number of only 60 took most of the deformation. We did not make a key-stoned cable, because we expected excessive deformation in the copper.

Fig. 2. Cross-section of rectangular $Nb₃Al$ Rutherford cable with low compaction factor 82.5 %. The F1 strands were used. 14.2 mm x 2.0mm.

At the compaction rate of 82.5 %, there is no degradation in Ic values, but we observed some degradation with higher compacted cable due to some detachment of the electroplated copper [6].

IV. CABLE TEST WITH FLUX-PUMP AT SELF-FIELD

A two foot Rutherford cable of low compaction factor was tested at 4.2 K with the flux pump method with full current as described in the previous report [7]. Its training curve is shown in Fig. 3, where the maximum achieved current in the $Nb₃Al$ cable was 27.4 kA, corresponding to 1015 A/strand. This number proved there is no excessive disturbance in the low field region. We estimate its maximum self field is 1.5 Tesla.

Fig. 3. Flux-pump test results for F1 Nb₃Al Rutherford cable. The flux pump was working near its capacity, quenching in the primary many times.

V. CABLE TEST WITH TRANSPORT CURRENT AT CERN

A pair of low compaction factor $Nb₃Al$ Rutherford cables of 173.5 cm length were tested at the FRESCA facility of CERN with high transport current in the high field dipole magnet up to 10-Tesla at 4.3 and 1.9 K [8]. The relative position of the voltage taps are shown in Fig. 4. In the present test we set the

self-field to add to the external dipole field, resulting in additional 0.9 Tesla added. We followed the same test procedure, which was carried out last year with PIT Rutherford cable [9].

The Rutherford cables are wrapped with S-glass tape with 20 % overlapping, and hardened with Ceramic binder. The pair of the cables was stacked without any further insulation between them, and was sandwiched with similarly insulated dummy cables. And a 5 mil Kapton sheet was placed on both sides. They were incased in the sample holder and epoxy impregnated under a pressure of 40 MPa.

Fig. 4. Rutherford Nb₃Al test setup at FRECCA of CERN. The relative position of the taps, splices and the external field distribution is shown.

First the cable was tested at 4.3 K with the external field up to 7 Tesla, and later tested further up to 10 Tesla with the dipole magnet cooled at 1.9 K. The test results of quench current are shown in Fig. 5, where the self field of the transport current is included.

In these measurements, the external field was set first and th e transport current was increased until the cable quenched.

1) Cable Test at 4.3 K below 7 Tesla

Up to 7 Tesla, except at 0 Tesla, a quench always started at **4.2 K** e \overrightarrow{A} \overrightarrow{A} as \overrightarrow{A} as the splices, or near the splices. Even when we increased the ramp rate of the transport current up to 2000 A/s, either the bottom splice connecting the pair of the $Nb₃Al$ cables, or top splices joining a $Nb₃Al$ cable and a $NbTi$ lead cable, heated up first. The resistances of these splices were measured to be in the order of 1 nano- $Ω$. We need to improve the design of these joints for better cooling in future testing.

> But it could be logical to assume that the quench is started at th e low field region next to the joint region as shown in Fig. 4, due to instability caused by the flux-jump like behavior of the excessive Nb in the $Nb₃Al$ strand. This effect is extensively explained in the accompanying papers for the $Nb₃Al$ strand in this conference [6] and [10].

2) Cable Test at 4.3 K at Zero External Field

At 0 Tesla external excitation, corresponding to data points a round 1 Tesla in Fig. 5, we observed many spikes and the Nb in the Nb₃Al strands around 1 to 1.5 Tesla [6] and [10]. quenches started in the central cable region in some cases. These may be related to low field flux-jump like instability of

Fig. 5. Nb₃Al cable test data at 4.3 K done with external field at CERN.

3) Cable Test at 4.3 K above 9 Tesla up to 11 Tesla

In this field region the cable quenched near the splices at the ramp rate up to 400 A/s. At higher ramp rate from 600 up to 30 00 A/s, the cable started its quenches in the higher central field region, not at the splices. These test data points are also shown in Fig. 5.

parallel to the short sample limit curve, which are derived fr om the extracted short sample date multiplied with the strand In this region the quench current values are lined up in number of 27. There is about 10 to 15 % overall degradation over the extracted values, which we can expect from the thermal insulation in the present probe holder.

region is shown in Fig. 6. As we can see the quench current va lues increase up to 2000 A/s, and then decrease. The ramp rate dependency at different external fields in this

Fig. 6. Ramp rate dependency of quench current values at high field region.

4) Quench Velocity in the 8 to 11 Tesla Region

The typical voltage tap signals for this region are shown in Fig. 7 for the quench current at 10.8 Tesla. In this case, it can be seen that the initial quench started at 1ms somewhere in the region (11,13) in the –lead side. At 2.2 ms, the quench front reached at point 13, and at 6.8 ms it reached at point 14. With a distance of 500 mm, we can calculate the quench velocity is 109 m/s. Also it can be seen the quench propagated to the +lead side through the insulation in 0.8 ms, and it propagated along the cable.

Fig. 8. Also in this figure, data points at 0 Tesla external field The calculated quench velocity from the data is shown in

ar e shown at 1 Tesla because of the self field. And 1 Tesla external field data points are also shown at 2 Tesla.

4. 3 K. Ramp rate at 1000 A/s. Iq = 15.81 kA. Vq = 109 m/s for >1.2 ms. Fig. 7. Quench behaviors and quench velocity determination at 10.8 T at

Fig. 8. Calculated quench velocity values above 8 Tesla and below 2 Tesla for both 4.3 and 1.9 K are shown.

5) Quench Current Test at 1.9 K

The cable was tested at 1.9 K at the ramp rate of 100 to 1000 A/s. In general, the quench current at 1.9 K is higher th an the value at 4.3 K, as is shown in Fig. 9. The calculated quench velocities at 1.9 K are also shown in Fig. 8.

Fig. 9. Quench current values of the cable test at CERN at 1.9 K are shown together with values at 4.3K. Also in this figure, the load line for SR04 magnet and its highest quench value at 3.95 K are shown for comparison.

VI. INSTABILITY AT LOW FIELD REGION

Extensive description about the instability of the $Nb₃Al$ strand at the low field region from 1 to 2 Tesla is given in other papers $[6]$ and $[10]$. It could be concluded the excessive am ount about 20 % of Nb in the strand is the cause. The Bc2 of Nb is about 0.4 to 0.6 Tesla, but the interstrand coupling and the resistive transition of Nb may be causing its instability in this field region.

VII. SMALL RACETRACK COIL – SR04

With a 14 m long $Nb₃Al Rutherford cable we made the coil$ of the small magnet SR04, which is shown in Fig. 10, similar to the previous magnet SR03. These magnets have two-layer sm all racetrack coils which are connected in the opposite direction and stacked tight together [11].

In October 2006, the magnet SR04 was successfully tested up to 21.8 kA, corresponding to 8.7 Tesla at the inner edges of the coil blocks, without significant training. Its load line and

the highest current point are shown in Fig. 9. Its detailed test data will be reported later.

treated coil of the SR04 magnet before epoxying. Fig.10. The wound and heat

VIII. FURTHER IMPROVEMENTS

Recent improvements in the current density of the $Nb₃Al$ strand is impressive, but we still want improvement and to have it further increased well above Jc =1000 A/mm² at 15 Te sla at 4.2 K. In order to make a better Rutherford cable, we should like to increase the compaction factor. The electroplating of copper on the $Nb₃Al$ precursor was successfully achieved, but we still have to achieve much stronger bonding between the copper and the precursor to avoid the detachment of copper stabilizer.

IX. CONCLUSION

 We achieved the first successful fabrication in the world of a Rutherford cable with Cu stabilized $Nb₃Al$ strands, producing a viable cable with acceptable Jc degradation. The cable test up to 11 Tesla external field with full transport current, and successful fabrication and excitation of a small model magnet SR04 proved that the Nb₃Al Rutherford cable could be excited to near its short sample data.

Although there are still much more improvements to be made in the Nb₃Al strand and Rutherford Cable, judging from our test results, the Nb₃Al Rutherford cable was shown to be viable for its application for high field accelerator magnets, possibly beyond 15 Tesla Magnets.

beyond 150 MPa, and where $Nb₃Sn$ cables will suffer. The well known advantage of the $Nb₃Al$ strand over the $Nb₃Sn$ strand is its stronger stress-strain characteristics. The $Nb₃Al$ cable could be applied where the compressive force is

Secondly with $Nb₃Al$ cable there is no strong degradation effect due to the Rutherford cabling operation, like the tin leakage in the $Nb₃Sn$ cables. This point will be more important for strands with finer filament strands, below 50 μm size of subelements.

Because of its stronger strain-stress characteristics, $Nb₃Al$ Rutherford cable could be used also for magnets made with React-Wind method.

With further improvements in the current density, Jc, fields as well as in high field accelerator magnets. One reduction of the magnetization with use of Ta matrix, and reduction of its production cost, it could be used in many example could be its application in the detector solenoid where the local magnetic field strength goes beyond 10 Tesla.

ACKNOWLEDGMENT

and NIMS in Japan for their enduring efforts for carrying out our studies. We are grateful to our staff and technicians both at Fermilab

REFERENCES

- Kitaguchi, "Fabrication of Cu Stabilizer into Long-Length RHQT-Processed Nb3Al Round Wire," *IEEE Trans. Appl. Supercond*., vol.16, pp. 1224-1227, June 200 6. [1] A. Kikuchi, K. Tagawa, M. Kobayashi, Y. Iijima, T. Takeuchi, and H.
- [2] N. Koizumi, T. Takeuchi, and K. Okuno, "Development of Advanced Nb3Al Superconductors for a Fusion Demo Plant". *Nuclear Fusion,* vol. 45, pp. 431-438, 2005.
- [3] T. Takeuchi, H. Kitaguchi, N. Banno, Y. Iijima, A. Kikuchi, K. Tagawa, Y. Suzuki, M. Yoshikawa, S. Hayashi, "Fabrication and Operation of a RHQT Nb3Al Insert Coil Generating 4.5 T at 4.2 K in 15 T Back-Up Field", presented in this conference.
- [4] R. Yamada, G. Ambrosio, E. Barzi, V. Kashikin, A. Kikuchi, I. Novitski , T. Takeuchi, M. Wake, and A. Zlobin, "Feasibility Study for 15 Tesla Magnet Using Rapid-Heating Quenching and Transformation Nb₃Al Strand," *Journal of Physics: Conference Series,* vol. 43 pp.714-718, 2006.
- 16, pp. 1204-1207, June 2006. [5] K. Tsuchiya, C. Mitsuda, A. Terashima, T. Takeuchi, N. Banno, S. Nimori , Y. Seki, M. Ohno, K. Okamoto, K. Nakamura, T. Takao, T. Ikeda, T. Higuchi, K. Tagawa, and G. Iwaki, "Nb3Al Wire Development for Future Accelerator Magnets", *IEEE Trans. Appl. Supercond*., vol.
- Rutherford Cable", presented in this conference. [6] A. Kikuchi, R. Yamada, G. Ambrosio, N. Andreev, E. Barzi, C. Cooper, Y. Iijima, M. Kobayashi, H. Kitaguchi, S. Nimori, M. Lamm, K. Tagawa, T. Takeuchi, K. Tsuchiya, D. Turrioni, M. Wake and A.V. Zlobin "Characteristics of Round and Extracted Strands of Nb3Al
- [7] E. Barzi, N. Andreev, V.V. Kashikhin, D. Turrioni and A.V. Zlobin, "Study of Nb₃Sn Cable Stability at Self-field using a SC Transformer", *IEEE Trans. Appl. Supercond*., vol. 15, pp. 1537-406, 2004.
- [8] A.P. Verweij, J .Genest, A. Knezovic, D.F. Leroy, J.-P. Marzolf, L.R. Oberli "1.9 K Test Facility for the Reception of the Superconducting Cables for the LHC", *IEEE Trans. Appl. Supercond*., vol. 9, pp. 153- 156, 1999.
- [9] G. Ambrosio, N. Andreev, E. Bartlett, E. Barzi, C-H Denarie, D. 15, pp. 1545-49, 2005. Dietderich, A.K. Ghosh, A.P. Verweij and A.V. Zlobin, "Critical Current and Instability Threshold Measurement of Nb₃Sn Cables for High Field Accelerator Magnets", *IEEE Trans. Appl. Supercond*., vol.
- [10] R. Yamada, A. Kikuchi and M. Wake "Magnetization Anomaly of Nb3Al Rutherford Cables", presented in this conference.
- [11] Pischalinikov, C. Sylvester, M. Tartaglia, R. Yamada and A.V. Zlobin Racetrack Coils", *IEEE Trans. Appl. Supercond.*, vol. 15, pp. 1550-53, 2004. S. Feher, G. Ambrosio, N. Andreev, E. Barzi, B. Bordini, R. Carcagno, V.I. Kashikin, V.V. Kashikin, M.J. Lamm, I. Novitski, D. Orris, Y. "Cable Testing for Fermilab's High Hield Magnets using Small