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In conventional low energy electron coolers, the electron beam is immersed in a continuous solenoid, which provides a calm and tightly focused beam in a cooling section. While suitable for low energies, the continuity of the accompanying magnetic field is hardly realizable at relativistic energies. A possibility is considered to use an extended solenoid in the gun and the cooling section only, applying lumped focusing for the rest of the electron transport line.

I. INTRODUCTION

Although electron cooling [1,2] has been a routine tool in many laboratories [3], its use has been restricted to low energy accelerators with the kinetic energy <1 GeV/nucleon, i.e. <0.5 MeV of electrons. Currently, there are two relativistic energy range electron cooling projects being developed: at Fermilab, for 8.9 GeV/c antiprotons in the Recycler ring [6] and at DESY, for a 15-20 GeV/c bunched proton beam in PETRA ring [7]. Traditional low energy electron cooling devices follow an original design of the NAP-M [8] employing a continuous longitudinal magnetic field in the kilogauss range for the electron beam transport from the cathode through the cooling region to the collector, see Fig. 1.

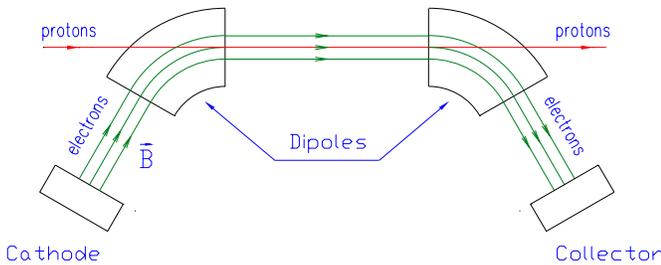


FIG. 1. Sketch of the NAP-M electron cooler EPOKHA. Electrons follow the magnetic field lines (green arrow lines) from the cathode to the collector.

The solenoidal field uniquely provides a focusing property, crucial for electron cooling: it allows to confine tightly the electron beam while keeping its angu-

lar spread small. Although at higher energies the space charge and collective interaction effects become less destructive, the mentioned property of the solenoidal field makes it very beneficial. This was found to be true for the developed medium-relativistic projects [4-7], but not only there. According to Ref. [9,10], the solenoidal field in the cooling section can be very advantageous at much higher energies as well. That is why a necessity of the longitudinal magnetic field in the cooling section is assumed in this paper. This does not mean that a possibility for effective cooling without the solenoidal field is totally denied; rather such possibility, if found, would lie beyond the scope of this paper.

In principle, a continuous solenoid along the whole electron beam line suggested in Ref. [5] would be a good focusing option at any energy. Such a solution though is hardly compatible with the beam acceleration up to relativistic energies and also with design advances (related to cooling of bunched beams) such as electron bunch decompression, incorporation of recirculator rings, etc. [7,10]. However, a different scale of electron energies under considerations allows to modify this approach. Namely, lumped focusing can be used for the beam transport line with an idea to avoid any coherent motion of the beam inside the cooling solenoid [6,7,10].

A beam state required by the electron cooling is characterized by a high ratio between the beam size and the Larmor radius; this state is referred to as calm or magnetized. The transport line can include any separated optical elements such as solenoid lenses, dipoles and quadrupoles. It is shown in this paper that a calm beam in the cooler requires certain matching between a magnetized electron gun and the cooler solenoid. A linear theory of matched 4-dimensional optical transitions is presented which allows to formulate properties of the transport line. The beam transformations are described in terms of the drift and the cyclotron degrees of freedom; a necessity to have them uncoupled is shown. For a beam born at a round cathode, it is proved that the cathode has to be properly magnetized. A possibility to transform a ribbon electron beam in a storage ring into a calm beam in the cooler is discussed. An example of a conceptual design of relativistic electron cooling is shown assuming an electrostatic accelerator as a source of the electrons. In this device, only the gun, cooling section and the collector are immersed in solenoids while the rest of the beam line has a lumped focusing.

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## II. ANGULAR MOMENTUM-DOMINATED BEAM

On entering or exiting the solenoid, the beam acquires a kick that changes its rotational state. Inside the cooling solenoid, the beam is required to be calm, i.e. not to have any angles in excess of the thermal ones (assumed to be negligible in this section). The above point is very important: the cooling rates are inversely proportional to a relative electron-ion velocity cubed; thus, any coherent angle above the thermal level dramatically depresses the cooling process. The question under consideration is whether and how this requirement can be compatible with the lumped focusing scheme.

### A. Solenoids and Acceleration Intervals

First, let the beam line to consist of aligned solenoids and acceleration intervals only. For these straight and axially symmetric lattices, Busch's theorem states that the canonical angular momentum

$$M = xp_y - yp_x = pr^2\theta' - e\Phi(r, z)/(2\pi c) \quad (1)$$

is conserved along any of the electron trajectories (see e.g. [11,12]). Here  $x, y, p_x, p_y$  are the transverse Cartesian coordinates and their canonically conjugated momenta,  $r, \theta, z$  are the cylindrical coordinates, the prime ' denotes a derivative along the axis  $z$ ,  $p = \gamma\beta mc$  is the total momentum,  $\Phi(r, z) = 2\pi \int_0^r B(\tilde{r})\tilde{r}d\tilde{r}$  is the magnetic flux inside a circle enclosed by the electron offset  $r$ , and  $-e$  is the electron charge. The canonical angular momentum (CAM) of any electron is thus determined by its initial value, i.e. by its value at the cathode. Thus, the conservation of the CAM allows to express an electron angular velocity at a given point of its trajectory in terms of the magnetic fluxes enclosed by this electron at this point and at the cathode. In the paraxial approximation, the magnetic field can be considered uniform over the beam cross section, which gives

$$\theta' = e(Br^2 - B_0r_0^2)/(2pcr^2), \quad (2)$$

with  $B_0$  and  $r_0$  as the magnetic field and electron offset at the cathode.

The single particle radial offset is described by the paraxial ray equation [12]:

$$r'' + \frac{\gamma' r'}{\beta^2 \gamma} + \left(\frac{eB}{2pc}\right)^2 r - \left(\frac{eB_0}{2pc}\right)^2 \frac{r_0^4}{r^3} = K \frac{r}{a^2} - \frac{\gamma'' r}{2\beta^2 \gamma} \quad (3)$$

where  $a$  is the beam radius,  $K = 2I/(I_0\beta^3\gamma^3)$  is the generalized perveance with  $I$  standing for the current and  $I_0 = mc^3/e = 17\text{kA}$ . The right hand side takes into account both the space charge and the external transverse electric field. The beam envelope  $a = a(z)$  is found from

Eq. (3) by the substitution  $r = a$ ,  $r_0 = a_0$  with the initial conditions  $a(0) = a_0$ ,  $a'(0) = 0$ . All the trajectories with  $r'(0) = 0$  scale as  $r(z) = r_0 a(z)/a_0$ .

Without the transverse electric fields, the equations (2, 3) have an  $r' = 0$  solution inside an extended solenoid of the cooler. This solution is realized if after the entrance in the cooler

$$a' = 0, \quad Ba^2 = B_0 a_0^2. \quad (4)$$

At the exit of the gun solenoid, the beam acquires an azimuth velocity. During the transport, this velocity changes, partly transforming into the radial velocity. However, if the beam state at the entrance of the cooler is matched with its state at the cathode so that the conditions (4) are satisfied, the beam transverse velocities are finally canceled. Schematically, the beam transport with the matched entrance in the cooling solenoid is depicted in Fig. 2.

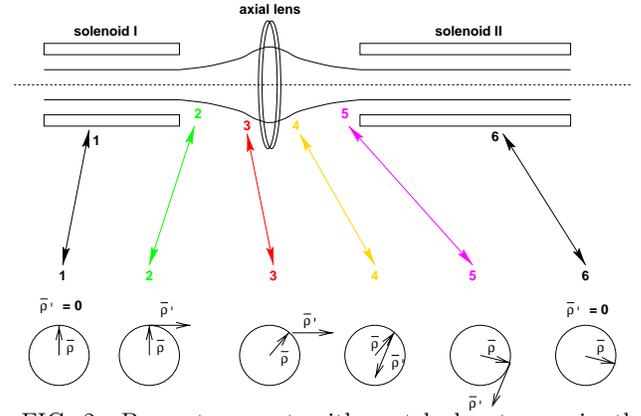


FIG. 2. Beam transport with matched entrance in the cooler. The beam envelope is depicted at the top. Transformation of electron coordinates  $\vec{r} = (x, y)$  and velocities  $\vec{r}' = (x', y')$  are shown at the bottom.

In the cooler, the space charge limits the minimal attainable angle,  $\sqrt{a^2\theta'^2 + a'^2}$ , which cannot be zero. As it follows from (2, 3) the angle is minimized when the cyclotron motion is not excited,  $a' = 0$ , and the angle is given by an azimuthal drift:

$$a\theta' = 2I/(\gamma^2\beta^2 Bac). \quad (5)$$

The drift angles can be neglected if they do not exceed the thermal angles of the cooled ions; this puts the lower boundary on the magnetic field in the cooling section.

With the drift neglected, the electrons do not have any transverse velocity inside the cooling solenoid provided that the matching conditions (4) are satisfied.

If the solenoid radius is much smaller than a period of the Larmor helix, the solenoid entrance can be considered as a thin boundary. In this case, the matching requirements (4) become explicit boundary conditions at the solenoid entrance. Note that in the linear approximation, the matching is satisfied for every trajectory once it is satisfied for one of them.

In the radial equation (3), the last term on the left hand side is determined by the inherited CAM  $M = eB_0 r_0^2 / 2c$ . Radial dependence of this term allows to treat the CAM as effective (unnormalized) emittance

$$\varepsilon_{eff} = M/p = \Phi / (2\pi B\rho) \quad (6)$$

with  $B\rho = pc/e$ . Then, this analogy leads to a concept of an effective beta-function

$$\beta_{eff} = a^2 / \varepsilon_{eff} = \frac{2\pi\gamma\beta ea^2}{r_e\Phi}. \quad (7)$$

The effective beta-function determines a required lens-to-lens distance in the beam transport channel. For a conventional low-energy cooler, assuming the electron kinetic energy  $E_e = 25$  keV, the magnetic flux  $\Phi = 1\pi$  kG cm<sup>2</sup>, and the beam radius  $a = 1$  cm, the effective beta-function is very small,  $\beta_{eff} = 1$  cm. It means that the accompanying magnetic field cannot be actually interrupted in this region of parameters. However, the situation changes for relativistic coolers where the accelerated beam is more rigid, and the magnetic flux can be significantly reduced.

For the Fermilab project, for instance, with the electron kinetic energy in the cooler  $E_e \cong 4.3$  MeV, the space charge limitation (5) allows for a rather small value for the magnetic flux:  $\Phi = 30\pi$  G cm<sup>2</sup> [6]. For the beam radius of  $a = 0.6$  cm, the accompanying magnetic field can be interrupted at early stages of the acceleration: for  $\gamma\beta = 2$  Eq. (7) already gives  $\beta_{eff} = 20$  cm.

When extracted from the magnetic field, the divergence of this cold and low space charge beam is determined by the inherited canonical angular momentum. Beams of such a kind can be referred to as an angular momentum dominated, as distinguished from emittance and space charge dominated beams.

The transport of the angular momentum dominated beam is not completely identical to that of the emittance dominated beams, as it could be concluded from the envelope equation (3). The principal difference is that the CAM-related angles are not random; once acquired, they can be effectively nulled out by a proper beam matching in the downstream solenoid, as it is sketched in Fig. 2. Due to the momentum spread of electrons though, this extraction gets to be imperfect: electrons with different momenta have different phase advances. Note that the mismatch caused by the momentum spread increases with the magnetic field due to a growth of the phase advances and their spread; thus, from this point of view, a lower magnetic field is more beneficial. In this paper that issue is not discussed in more details; the electron momentum spread is supposed to be insignificant, which requires the phase-mismatch electron angles in the cooler to be smaller than the angles of the cooled ions.

## B. Bends

Above, a straight transport line was considered. In practice though, bending parts are normally inevitable. Thus, the next question is whether the bends could be compatible with this lumped focusing. Inside a dipole, the linear electron motion is conventionally described by the following set of equations:

$$x'' + \frac{1-n}{\rho_d^2}x = 0, \quad y'' + \frac{n}{\rho_d^2}y, \quad n = -\frac{\rho_d}{B_d} \frac{\partial B_d}{\partial x}, \quad (8)$$

where  $x$  and  $y$  are the horizontal and vertical displacements from the ideal orbit,  $\rho_d$  is a radius of curvature in the dipole magnetic field  $B_d$  along the  $y$  axis, and the parameter  $n$  is conventionally referred to as the field index. Generally, these equations do not preserve the rotational symmetry of the beam in the transverse  $x-y$  plane. However, for a specific case  $n = 1/2$  the equations are invariant under  $x-y$  rotations, and the angular momentum  $M = pr^2\theta' = p(xy' - x'y)$  is an integral of motion. Thus, for this specific field index, the bending parts are compatible with the lumped focusing scheme: the angular momentum conservation guarantees the same sufficient conditions for the calm beam in the cooler as for the straight transport line (4). For this invariant bending, the electron trajectory can be described in the polar coordinates:

$$r'' + \frac{r}{2\rho_d^2} - \left(\frac{M}{p}\right)^2 \frac{1}{r^3} = 0. \quad (9)$$

Thus, the transport line consisting of solenoids, drifts and the index 1/2 bending magnets would provide the calm beam inside the cooler if the matching conditions (4) were satisfied. From the optical point of view, all these elements are rotationally invariant; below, they are referred to as the invariant elements. Transport lines entirely based on the invariant elements can be called locally invariant; they are considered in the next section. The locally invariant lines have to be distinguished from another kind of a transport, which restores the rotation symmetry at the exit, but does not preserve it for the intermediate points of the trajectory. As a whole, such kind of a transport is described by an invariant mapping, without being locally invariant. Such transport can be referred to as globally invariant. It also can be called as block invariant if it relates to a part of the transport line.

In the succeeding section, the locally invariant transport is described in terms of  $2 \times 2$  linear mapping. For these lines, the Courant-Snyder parameters are found and the matching conditions are reconsidered on a base of this approach.

## III. LOCALLY-INVARIANT MAPPING

A linear mapping can be built in terms of the Cartesian coordinates,  $x$  and  $y$ . In the presence of solenoids, it is

convenient to introduce also a rotating Larmor frame,  $\hat{x}-\hat{y}$ , as

$$\begin{aligned} u &\equiv \hat{x} + i\hat{y} = (x + iy)e^{-i\chi} \\ \chi' &= \frac{1}{2} \frac{eB}{pc} \equiv \Omega/\gamma\beta c. \end{aligned} \quad (10)$$

Due to the symmetry, the equations of motion reduce to a single equation for the complex offset  $u$  (see e. g. [12]). This equation takes a most compact form when the beam frame time  $\tau$ ,  $d\tau = (m/p)dz$  is used as an independent variable instead of the longitudinal coordinate  $z$ :

$$\ddot{u} + \hat{\Omega}^2 u = 0, \quad \hat{\Omega}^2 = \Omega^2 + \frac{1}{2} \left( \frac{eB_d}{mc} \right)^2 - \frac{p^2 K}{m^2 a^2} + \frac{\gamma\gamma''}{2c^2}. \quad (11)$$

which is the Mathieu-Hill equation describing the uncoupled betatron oscillations.

The solution of (11) can be presented in the conventional form:

$$u(\tau) = C_+ \sqrt{\underline{\beta}} e^{i\phi} + C_- \sqrt{\underline{\beta}} e^{-i\phi} \equiv u_+ + u_-, \quad \dot{\phi} = 1/\underline{\beta} \quad (12)$$

where  $C_+$ ,  $C_-$  are two arbitrary complex constants, and the betatron function  $\underline{\beta}$  satisfies the following equation:

$$2\underline{\beta}\ddot{\underline{\beta}} - \dot{\underline{\beta}}^2 + 4\hat{\Omega}^2 \underline{\beta}^2 - 4 = 0. \quad (13)$$

The solution of the equation of motion (11) can be written in a form that presents the constants  $|C_{\pm}|^2$  as the Courant-Snyder invariants:

$$|C_{\pm}|^2 = \frac{1}{4\underline{\beta}} \left| u(1 \pm i\dot{\underline{\beta}}/2) \mp i\underline{\beta}\dot{u} \right|^2, \quad (14)$$

which can be also expressed as

$$\begin{aligned} |C_{\pm}|^2 &= \frac{1}{4\underline{\beta}} \left[ (1 \mp \underline{\beta}\Omega)^2 r^2 + \dot{\underline{\beta}}^2 r^2/4 + \underline{\beta}^2 (r^2 + r^2 \dot{\theta}^2) \right. \\ &\quad \left. \pm 2\underline{\beta}(1 \mp \underline{\beta}\Omega)r^2 \dot{\theta} - \underline{\beta}\dot{\underline{\beta}}r\dot{r} \right]. \end{aligned} \quad (15)$$

From here, it follows that the two squared amplitudes  $|C_{\pm}|^2$  are related to each other by means of the CAM:

$$|C_+|^2 - |C_-|^2 = M/m \quad (16)$$

To be complete, the presentation (12, 13) requires the initial conditions for the beta-function,  $\underline{\beta}(0)$ ,  $\dot{\underline{\beta}}(0)$ . Generally speaking, these initial conditions can be arbitrary chosen for transport lines. However, in the case under study the starting point  $\tau = 0$  corresponds to a surface of the magnetized cathode, and this determines a natural choice for the initial beta-function. There are no transverse fields at the cathode,  $\hat{\Omega}_o = \Omega_o$ , and a trajectory

with zero initial transverse velocities,  $\dot{r} = 0$ ,  $r\dot{\theta} = 0$ , does not have initial cyclotron amplitude. It is convenient to identify this particular trajectory with a pure 'minus' solution, with  $C_+ = 0$  for it, which is realized by a choice of

$$\underline{\beta}(0) = 1/\Omega_o, \quad \dot{\underline{\beta}}(0) = 0. \quad (17)$$

With this choice, the amplitude  $C_-$  is determined by an initial offset, while  $C_+$  is a function of the initial transverse velocity. So the 'minus' solution relates to the position of the Larmor center inside the gun solenoid, and the 'plus' solution describes the cyclotron excitation there. At the cathode, they satisfy the boundary conditions:

$$\dot{u}_{\pm}|_o = \pm i\Omega_o u_{\pm}|_o. \quad (18)$$

As it is shown in the section IV, these 'plus' and 'minus' solutions can be treated as two canonical degrees of freedom, referred to as a drift and a cyclotron motion.

The drift and the cyclotron solutions can be also considered inside the cooling solenoid, where  $\hat{\Omega} = \hat{\Omega}_f = \text{const}$ . These particular solutions satisfy conditions similar to (18):

$$\dot{u}_{\pm}|_f = \pm i\hat{\Omega}_f u_{\pm}|_o. \quad (19)$$

### A. Matched Mapping

Solutions of the Mathieu-Hill equation (11) can be also presented in terms of a transformation with a real  $2 \times 2$  matrix,  $A(\tau)$ :

$$\begin{pmatrix} u \\ \dot{u} \end{pmatrix}_{\tau} = A(\tau) \begin{pmatrix} u \\ \dot{u} \end{pmatrix}_o, \quad |A(\tau)| = 1. \quad (20)$$

When an initially calm beam is finally transformed into a calm state again, it means that the cyclotron mode is not excited both initially and finally or

$$\dot{u}_o = -i\Omega_o u_o, \quad \dot{u}_f = -i\hat{\Omega}_f u_f. \quad (21)$$

This matching imposes the following conditions on the transformation matrix  $A$  (20):

$$\frac{A_{22}}{A_{11}} = \frac{\hat{\Omega}_f}{\Omega_o}; \quad \frac{A_{21}}{A_{12}} = -\hat{\Omega}_f \Omega_o. \quad (22)$$

From here, the matrix  $A$  can be parameterized as

$$A = \begin{pmatrix} \sqrt{\frac{\Omega_o}{\hat{\Omega}_f}} \cos \psi & \frac{1}{\sqrt{\hat{\Omega}_f \Omega_o}} \sin \psi \\ -\sqrt{\hat{\Omega}_f \Omega_o} \sin \psi & \frac{\hat{\Omega}_f}{\Omega_o} \cos \psi \end{pmatrix} \quad (23)$$

with a necessary condition  $\hat{\Omega}_f \Omega_o > 0$ . The single free parameter, a phase  $\psi$ , is determined by all the involved optic elements, with  $\psi = \hat{\Omega}_f$  inside the cooling solenoid.

The presentation (23) can be also obtained in a different manner. The matrix of transformation for the Mathieu-Hill equation has a conventional expression in terms of the initial and final values of the betatron function and its derivative (see e. g. [13]). The initial values of the beta-function and its derivative are considered above:  $\underline{\beta}_o = 1/\Omega_o, \underline{\dot{\beta}}_o = 0$ . If the cyclotron mode is not excited in the cooler, similar conditions are fulfilled there:  $\underline{\beta}_f = 1/\hat{\Omega}_f, \underline{\dot{\beta}}_f = 0$ . With these initial and final values of the betatron function, the above presentation of the matrix A (23) follows.

It results from (21, 23), that if the cyclotron mode is not finally excited, then the initial and final beam sizes are matched:

$$(\hat{\Omega}r^2)_f = (\Omega r^2)_o. \quad (24)$$

A difference between this form of the matching condition and the ‘‘magnetic flux law’’ (4) reflects a beam drift rotation under the space charge effect. It is shown below that the corrected matching condition (24) expresses a restoration of the action related to the drift degree of freedom.

The equation of motion (11) corresponds to the Hamiltonian

$$H(\hat{x}, \hat{p}_x, \hat{y}, \hat{p}_y) = \frac{\hat{\Omega}^2 \hat{x}^2}{2} + \frac{\hat{p}_x^2}{2} + \frac{\hat{\Omega}^2 \hat{y}^2}{2} + \frac{\hat{p}_y^2}{2} \quad (25)$$

with  $\hat{p}_x, \hat{p}_y$  being canonical momenta conjugated to the variables  $\hat{x}, \hat{y}$ . For that part of the trajectory where  $\hat{\Omega} = \text{const}$ ,

$$\hat{J}_x = \frac{\hat{\Omega} \hat{x}^2}{2} + \frac{\hat{p}_x^2}{2\hat{\Omega}}, \hat{J}_y = \frac{\hat{\Omega} \hat{y}^2}{2} + \frac{\hat{p}_y^2}{2\hat{\Omega}} \quad (26)$$

are the corresponding action variables. For the pure drift motion, both actions are equal:

$$\hat{J}_x = \hat{J}_y = \hat{\Omega} r^2 / 2. \quad (27)$$

It can be also seen that the actions are preserved under the transformation A. Generally, the actions do not vary when the system parameters change adiabatically. Although the beam transport is not supposed to be adiabatic, the actions are still preserved here. This property of mapping A can be interpreted in a general way. The conditions (21) express a requirement for the mapping not to mix the two modes of the motion. Keeping the modes uncoupled is also a general property of the adiabatic motion. That is why it is not a surprise that for both cases the action preservation is guaranteed.

As a curious fact, it can be noted that the equation of motion (11) can be associated with a complex Hamiltonian

$$H(u, p_u) = \frac{\hat{\Omega}^2 u^2}{2} + \frac{p_u^2}{2}. \quad (28)$$

Then, the complex action

$$\hat{J}_u = \frac{\hat{\Omega} u^2}{2} + \frac{p_u^2}{2\hat{\Omega}}. \quad (29)$$

is also conserved: initially and finally  $J_u = 0$ .

## B. Temperature Transformation for a Matched Transport

Above, the transformation matrix A (23) was found from the condition of the drift-to-drift transition (21). Since the matrix is invariant with respect to a common sign change of  $\Omega_o$  and  $\hat{\Omega}_f$ , it allows to conclude that matching of the drift component leads automatically to identical matching of the cyclotron component:

$$(\hat{\Omega}|u_{\pm}|^2)_f = (\Omega|u_{\pm}|^2)_o. \quad (30)$$

For the drift mode (+), it gives the conditions (24), while for the cyclotron mode (−) it can be rewritten in terms of the transverse temperature  $T_{\perp}$ :

$$\left(\frac{T_{\perp}}{\hat{\Omega}}\right)_f = \left(\frac{T_{\perp}}{\Omega}\right)_o. \quad (31)$$

It is shown below that the relationships (30) may be interpreted as a preservation of both drift and cyclotron actions when these modes do not transfer to each other.

## IV. MATCHING WITH NON-INVARIANT OPTIC ELEMENTS

The analysis above was related to the locally invariant transportation, i. e. based on such optically invariant elements as the solenoids and dipoles with the index 1/2. However, with increasing the electron energy, the quadrupoles can be more suitable than the solenoid lenses for the beam transport. Also, the conventional uniform-field dipoles may look more preferable than the 1/2 index ones from a technical point of view. Consequently, a question appears whether such optical elements as conventional dipoles or quadrupoles are compatible with the requirement to have a calm beam in the cooling section?

### A. Uncoupled Transformation

In this section, a general form of the transformation matrix is found. An optical transition between the magnetized cathode and the cooler can be treated in terms of the canonically conjugated pairs. Let  $\vec{\rho} = (x, y)$  be the transverse Cartesian coordinate, and  $\vec{p}_{\perp} = (p_x, p_y) = \vec{k}_{\perp} - \frac{e}{c}\vec{A}_{\perp}$  be the canonically conjugated momentum. Here  $\vec{k}_{\perp} = \gamma m \vec{v}_{\perp}$  is the kinematic momentum and  $\vec{A}_{\perp} = \frac{1}{2}\vec{B} \times \vec{\rho}$  is the vector potential in the solenoid. The transformation of a particle state

$$\mathbf{x} = \begin{pmatrix} x \\ p_x \\ y \\ p_y \end{pmatrix} \quad (32)$$

is expressed as  $\mathbf{x}_f = \mathcal{T} \mathbf{x}_o$  with a symplectic  $4 \times 4$  matrix  $\mathcal{T}$ . The mapping symplecticity can be expressed as invariance of the Poisson brackets

$$\{f, g\} \equiv \sum_{i=x,y} \left( \frac{\partial f}{\partial p_i} \frac{\partial g}{\partial \rho_i} - \frac{\partial g}{\partial p_i} \frac{\partial f}{\partial \rho_i} \right)$$

under this transformation for any two functions  $f = f(\vec{p}, \vec{\rho})$ ,  $g = g(\vec{p}, \vec{\rho})$  (see e. g. [14,15]). In particular, there are only two non-zero Poisson brackets between the components of the state vector  $\mathbf{x}_f$  as functions of the components of the initial state  $\mathbf{x}_o$ :

$$\{p_x, x\} = \{p_y, y\} = 1, \quad (33)$$

while the rest four brackets are equal to zero.

For a given point  $\mathbf{x}$  in the 4D phase space, the transverse kinematic momentum  $\vec{k}$  and the position  $\vec{d}$  of the Larmor center are expressed as

$$\begin{aligned} \vec{k}_\perp &= \vec{p}_\perp + \frac{e}{2c} \vec{B} \times \vec{\rho} \\ \vec{d} &= \vec{\rho} - \vec{\rho}_L = \frac{1}{2} \vec{\rho} - \frac{c}{e} \frac{\vec{p} \times \vec{B}}{B^2} \end{aligned} \quad (34)$$

where the vector  $\vec{\rho}_L = c\vec{k} \times \vec{B}/(eB^2)$  describes the position on the Larmor circle relatively to its center. The relationships (34) can be considered as a transformation from the canonical pair  $\vec{\rho}$  and  $\vec{p}$ , to the new variables  $\vec{d}$  and  $\vec{k}$ . The non-trivial feature of this transformation is that the Poisson's brackets between  $\vec{k}$  and  $\vec{d}$  are equal to zero, while

$$\{k_x, k_y\} = -\frac{eB}{c}, \quad \{d_x, d_y\} = \frac{c}{eB}. \quad (35)$$

Therefore, the normalized variables

$$\begin{pmatrix} \kappa_1 \\ \kappa_2 \end{pmatrix} = \sqrt{\frac{c}{eB}} \begin{pmatrix} k_y \\ k_x \end{pmatrix} \quad \text{and} \quad \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} = \sqrt{\frac{eB}{c}} \begin{pmatrix} d_x \\ d_y \end{pmatrix} \quad (36)$$

compose new canonical pairs. The action and phase variables related to these pairs can be introduced as well:

$$\begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix} = \sqrt{2J_D} \begin{pmatrix} \cos \psi_D \\ \sin \psi_D \end{pmatrix}, \quad \begin{pmatrix} \kappa_1 \\ \kappa_2 \end{pmatrix} = \sqrt{2J_C} \begin{pmatrix} \cos \psi_C \\ \sin \psi_C \end{pmatrix}, \quad (37)$$

with

$$\begin{aligned} J_D &= (\xi_1^2 + \xi_2^2)/2 \equiv \xi^2/2 = \frac{eB}{2c} d^2 \\ J_C &= (\kappa_1^2 + \kappa_2^2)/2 \equiv \kappa^2/2 = \frac{c}{2eB} k^2. \end{aligned} \quad (38)$$

(A canonical transformation similar to (34- 38) is mentioned in Ref. [14], p. 432.) In terms of these new variables, the CAM is expressed in a very compact way:

$$M = \frac{eB}{2c} (d^2 - \rho_L^2) = \frac{\xi^2 - \kappa^2}{2} = J_D - J_C. \quad (39)$$

This canonical transformation can be presented as

$$\hat{\mathbf{x}} \equiv \begin{pmatrix} \kappa_1 \\ \kappa_2 \\ \xi_1 \\ \xi_2 \end{pmatrix} = \mathcal{B} \begin{pmatrix} x \\ p_x \\ y \\ p_y \end{pmatrix} \equiv \mathcal{B} \mathbf{x}, \quad (40)$$

with a symplectic  $4 \times 4$  matrix  $\mathcal{B}$ , which can be composed using (34) and (36). Finally, the transformation between the two solenoids can be rewritten as

$$\hat{\mathbf{x}}_f = \hat{\mathcal{T}} \hat{\mathbf{x}}_i, \quad (41)$$

with a new symplectic matrix

$$\hat{\mathcal{T}} = \mathcal{B}_f \mathcal{T} \mathcal{B}_o^{-1}, \quad (42)$$

where the matrices  $\mathcal{B}_o$  and  $\mathcal{B}_f$  belong to the initial (electron gun) and final (cooling section) solenoids, respectively.

The  $4 \times 4$  matrix  $\hat{\mathcal{T}}$  can be presented in a block form as

$$\hat{\mathcal{T}} \equiv \begin{pmatrix} (\text{CC}) & (\text{CD}) \\ (\text{DC}) & (\text{DD}) \end{pmatrix} \quad (43)$$

In the initial state (at the cathode), the beam diameter largely exceeds a characteristic Larmor radii of particles. It can be expressed as a high initial excitation of the drift degree of freedom in comparison with the cyclotron one. To minimize the cyclotron motion in the cooling solenoid, any influence from the drift degree of freedom has to be avoided. In other words, the beam transport should be designed in a way that  $2 \times 2$  block (CD) vanishes. So the Poisson bracket  $\{\kappa_1, \kappa_2\} = 1$  is determined by the matrix (CC) only; therefore,

$$\begin{pmatrix} \kappa_1 \\ \kappa_2 \end{pmatrix}_f = (\text{CC}) \begin{pmatrix} \kappa_1 \\ \kappa_2 \end{pmatrix}_o, \quad |(\text{CC})| = 1. \quad (44)$$

Since  $|\hat{\mathcal{T}}| = 1$ , then  $|(\text{DD})| = 1$ . Finally, it can be shown that the block (DC) vanishes too; it follows from the fact that all the Poisson brackets  $\{\kappa_i, \xi_j\} = 0$ . As a result, the transformation of the drift component reduces to

$$\begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix}_f = (\text{DD}) \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix}_o, \quad |(\text{DD})| = 1.$$

The obtained block-diagonal form of the transformation

$$\hat{\mathcal{T}} = \begin{pmatrix} (\text{CC}) & 0 \\ 0 & (\text{DD}) \end{pmatrix} \quad (45)$$

shows that the mutual uncoupling of the drift and cyclotron degrees of freedom is necessary and sufficient for having a calm beam in the cooling section. Under this uncoupled transformation, both the drift and the cyclotron rms emittances

$$\begin{aligned}\epsilon_D &= \sqrt{\langle \xi_1^2 \rangle \langle \xi_2^2 \rangle - \langle \xi_1 \xi_2 \rangle^2} \\ \epsilon_C &= \sqrt{\langle \kappa_1^2 \rangle \langle \kappa_2^2 \rangle - \langle \kappa_1 \kappa_2 \rangle^2}\end{aligned}\quad (46)$$

are preserved; the brackets  $\langle \dots \rangle$  stand for the ensemble averaging.

If the matched mapping is (globally) rotation invariant, then the matrices (CC) and (DD) are invariant too. The group of rotationally invariant  $2 \times 2$  transformations is the group of rotations itself, so

$$\begin{aligned}(\text{CC}) &= \begin{pmatrix} \cos \psi_C & \sin \psi_C \\ -\sin \psi_C & \cos \psi_C \end{pmatrix} \\ (\text{DD}) &= \begin{pmatrix} \cos \psi_D & \sin \psi_D \\ -\sin \psi_D & \cos \psi_D \end{pmatrix}\end{aligned}\quad (47)$$

with the two phases  $\psi_C, \psi_D$  as free parameters. In this case, the actions  $\xi^2/2 = J_D$  and  $\kappa^2/2 = J_C$  are not changed. This again leads to the relations (24, 31) found above for the locally invariant transport. Here, these relations reveal themselves as conditions of the actions preservation; also they express the restoration of the emittances (46). Indeed, in this case the cross-averages in (46) vanish which results in

$$\epsilon_D = \langle J_D \rangle = eB/c \langle d^2/2 \rangle, \quad \epsilon_C = \langle J_C \rangle = c/(eB) \langle k^2/2 \rangle. \quad (48)$$

Due to the decoupling of the drift and cyclotron degrees of freedom, the 4D emittance follows as

$$\epsilon = \epsilon_D \epsilon_C = d^2 k^2 / 4. \quad (49)$$

The last result can be found in a different way. Generally, the 4D emittance is calculated by means of the  $4 \times 4$  correlation matrix  $\Sigma_{ik} = \langle \mathbf{x}_i \mathbf{x}_k \rangle$ , as  $\epsilon = \sqrt{|\Sigma|}$ . For arbitrary axially symmetric beams, this results in [16]

$$\epsilon = (\langle r^2 \rangle \langle k^2 \rangle - \langle r k_r \rangle^2 - \langle r k_\theta \rangle^2) / 4. \quad (50)$$

with  $k_r$  and  $k_\theta$  being the radial and the axial components of the kinematic momentum. For the matched beam, this expression can be presented in terms of the drift and cyclotron variables (34). When vanishing correlations between the drift and the cyclotron degrees of freedom are taken into account,  $\langle d_i k_j \rangle = 0$ , the previous result (49) follows.

Normally, the hadron beams have equal transverse emittances. Then, the axial symmetry of the transverse momentum distribution of the hadron beam in the cooler is beneficial for the cooling process. Thus, the optimal cross-section of the hadron beam is also axially symmetric there. That is why a round shape of the electron

beam in the cooling section is also optimal. Taking into account that a round shape of the cathode is also preferable, it leads to a conclusion that in the optimum, the drift matrix (DD) is rotationally invariant (45). If the cyclotron motion (temperature) can be neglected in the initial state, no requirements are imposed on the matrix (CC); otherwise, the symmetric (CC) as in (45) is the optimal for the cooling process.

## B. Invariant Matrices

According to the above description, the decoupled invariant beam transformations preserve the CAM. Thus, it would be convenient for the electron transport line to consist of the invariant blocks, i. e. groups of the optic elements described by the CAM-preserving matrices. A group of such linear mappings was considered by E. Pozdeev and E. Perevedentsev ([17,18], discussed in [19]). It was proved that all CAM-preserving matrices are described by the following  $2 \times 2$  block-diagonal form:

$$\mathcal{T} = \mathcal{U}(\psi) \begin{pmatrix} \mathbb{T} & 0 \\ 0 & \mathbb{T} \end{pmatrix}. \quad (51)$$

Here  $\mathcal{U}(\psi)$  is a 4D rotation matrix providing separated rotations in the coordinate and momentum sub-spaces by the same angle  $\psi$ , and  $\mathbb{T}$  is an arbitrary  $2 \times 2$  matrix with  $|\mathbb{T}| = 1$  required by the phase volume preservation. Note that the group (51) can also be described as a group of rotation invariant transformations because of  $\mathcal{U}^T \mathcal{T} \mathcal{U} = \mathcal{T}$  where the superscript  $T$  stands for transposing. This condition is equivalent to a commutation of the matrices  $\mathcal{T}$  and  $\mathcal{U}$  due to the rotation unitarity,  $\mathcal{U}^{-1} = \mathcal{U}^T$ . It follows that the mapping (51) transform any round beam distribution into round again. Note that matrices

$$\mathcal{T} = \mathcal{U}(\psi) \begin{pmatrix} \mathbb{T} & 0 \\ 0 & -\mathbb{T} \end{pmatrix} \quad (52)$$

also transform any round beam into round again, but they change the sign of the CAM. It can be shown that any matrix preserving the beam axial symmetry can be described either by Eq. (51) or Eq. (52).

Without coupling of the transverse degrees of freedom ( $\psi = 0$ ), the invariance requires for  $x$  and  $y$  matrices to be identical, which constitutes 3 independent conditions. Thus, two variable quadruples with one variable drift (or three variable quadruples) are sufficient to transmute any initial mapping into invariant one.

## V. NON-INVARIANT TRANSFORMATIONS

A transport scheme above requires the cathode immersed in a proper solenoidal field. A question arises whether the magnetic field at the cathode is really inevitable? If one assumes the (global) rotation invariance

for the transport mapping, the answer is clearly positive: this immediately follows from the CAM conservation for these transformations. But is it still possible to eliminate this field for some non-invariant transport?

Note that a non-invariant mapping can transform a particular calm and round beam into calm and round state again. An example of such a kind was actually shown in the previous section. It was pointed there that the cyclotron motion is not excited by the decoupled transformations. If this motion were not excited initially, an invariant drift transformation (DD) is sufficient to have final beam round when the initial beam was round too. Invariance of the cyclotron matrix (CC) is not required here, this matrix can be arbitrary. In this case, the total transformation  $\mathcal{T}$  is not invariant, but it still provides a round-to-round beam transformation for a particularly initial state.

### A. Generalized Busch's Theorem

Thus, the problem can be rephrased in a following manner: assuming the beam to be round at the cathode, does it have to be properly magnetized (4) to get the beam quiet and round inside the downstream solenoid? Remember that the mapping invariance is not employed in this section.

A positive answer to this question follows from the generalized Busch's theorem [20]. The theorem states that for a hydrodynamic, or laminar, beam transported by means of arbitrary static electric and magnetic fields, the contour integral

$$\oint_{\Gamma} \vec{p} d\vec{l} = \oint_{\Gamma} \vec{k} d\vec{l} - e\Phi/c \quad (53)$$

is conserved. Here the contour  $\Gamma$  bounds an arbitrary tube of trajectories in the 3D coordinate space  $x, y, z$ . If the initial and final beam states are rotationally invariant, the contour  $\Gamma$  is a circumference in the transverse plane, and the CAM preservation follows. Note that the field linearity is not required here.

Below, this theorem is extended from the electro- and magneto-static fields to arbitrary Hamiltonian systems. This extension, however, requires to assume the linearity of the transformation. Thus, the statement to be proved claims following: if a particular round beam is transformed by a symplectic linear mapping into a round state again, the CAM of every particle is restored. Note that the beam is not supposed to be laminar here.

A property of the symplectic transformations to conserve skew-scalar products is used here (see e. g. [15]). The skew-scalar product of two vectors in the 4D transverse phase space  $\mathbf{x}_1 = (x_1, p_{x1}, y_1, p_{y1})$  and  $\mathbf{x}_2 = (x_2, p_{x2}, y_2, p_{y2})$  is an antisymmetric bilinear form  $[\mathbf{x}_1, \mathbf{x}_2]$ . Expressed in terms of the usual scalar product, it can be written as  $[\mathbf{x}_1, \mathbf{x}_2] = (\mathbf{x}_1, \mathbf{S}\mathbf{x}_2)$  with  $\mathcal{S}$  as a

rotation by  $90^\circ$  in each of the phase planes, or

$$[\mathbf{x}_1, \mathbf{x}_2] = -x_1 p_{x2} - y_1 p_{y2} + x_2 p_{x1} + y_2 p_{y1}.$$

Let  $\mathbf{x}_{1i}$  and  $\mathbf{x}_{2i}$  be two arbitrary vectors of the initial state finally transformed into  $\mathbf{x}_{1f}$  and  $\mathbf{x}_{2f}$ . It can be seen that the angles between their 2D  $x-y$  components are conserved by the transformation. This property is an obvious consequence of the rotation invariance of the both states: without it, there would be an angular asymmetry of the final beam density distribution. However, the sign of this angle can be changed that would not contradict the angular symmetry of the final beam distribution. The two vectors can be taken as 2D-orthogonal:  $\mathbf{x}_{1i} = (r_i, p_{ir}, 0, p_{it})$  and  $\mathbf{x}_{2i} = (0, -p_{it}, r_i, p_{ir})$  having the angular momentum  $M_i = r_i p_{it}$  where  $r_i$  is the initial beam radius. Because of the angle conservation, these two vectors are 2D-orthogonal again after the transformation. Without a lack of generality, the  $x$ -axis can be assumed to go along the vector  $\vec{x}_1$  both for the initial and the final states; this follows from symplecticity of the rotations. So the final states can be presented as  $\mathbf{x}_{1f} = (r_f, p_{fr}, 0, p_{ft})$  and  $\mathbf{x}_{2f} = \pm(0, -p_{ft}, r_f, p_{fr})$  with  $M_f = \pm r_f p_{ft}$  as the final angular momentum. Conservation of the skew-scalar product

$$[\mathbf{x}_{1i}, \mathbf{x}_{2i}] = [\mathbf{x}_{1f}, \mathbf{x}_{2f}]$$

immediately results in  $M_i = \pm M_f$  as was to be shown.

Actually, the statement just proved means that the property of the canonical momentum conservation goes beyond the mapping (or Hamiltonian) invariance. For the invariant mappings, any initially symmetric state of beam transforms into a symmetric state again. But the mapping invariance does not follow from the fact that one particular symmetric state was eventually transformed into other, also symmetric, state. It was proved in fact that the mapping invariance is a somewhat surplus requirement for the momentum conservation; the rotational invariance restoration for a particular initial ensemble is sufficient to claim that every particle of this ensemble restores its CAM as well. However, the sign of the final CAM can be opposite to the initial.

Turning back to the specific question at the beginning of this section, it can be concluded that there is no mapping, invariant or not, transforming a round but not properly magnetized (4) beam at the cathode into a calm round beam in the cooler. No transformation can change an absolute value of the canonical angular momentum of a particle without breaking the rotational symmetry of their ensemble.

### B. Canonical Emittances and Beam Adapters

So the generalized Busch's theorem asserts that a round electron beam at the cathode has to be properly magnetized. However, it says nothing about non-round

beams at the cathode. In particular, what type of non-round non-magnetized beams can be transformed into a calm state in the cooling solenoid? By the definition, the drift emittance of a calm, or a magnetized, state is much higher than the cyclotron emittance. It seems rather obvious that the same ratio between two independent emittances is inherent to any initial beam state. Thus, to become magnetized in the cooler, the beam has to be described initially by the two emittances of very different values. Obviously, a similar statement is related to a reverse transition. In particular, it can be expected that a flat beam  $\varepsilon_x \gg \varepsilon_y$  can be injected into a solenoid with a proper optical adaptation, to become a magnetized beam with solenoidal emittances  $\varepsilon_C$  and  $\varepsilon_D$  [21,22,10] having

$$\frac{\varepsilon_C}{\varepsilon_D} = \frac{\bar{\rho}_L^2}{a^2} = \frac{\varepsilon_y}{\varepsilon_x}. \quad (54)$$

Such schemes can be used in order to optimize the features of electron storage rings and recirculators as coolers for high-GeV hadron beams [9,23–25] and for other applications [26]. The transformation from the ribbon state in a free space into the magnetized state inside the solenoid looks promising for high-energy electron cooling projects ( $\gamma = 100–1000$ ) where a natural flat shape of an electron beam in a storage ring can be utilized. However, it does not look so for the medium energy electron cooling where it would require a thread-like cathode with too high of an aspect ratio ( $\sigma_y/\sigma_x = \rho_L^2/a^2$ ).

## VI. FERMILAB ELECTRON COOLING PROJECT

To increase Tevatron luminosity, Fermilab is developing a high energy electron cooling system to cool 8.9 GeV/c antiprotons in the Recycler ring [6]. A scheme of the electron transport proposed for this project incorporates many of the above ideas. This scheme is presented here as an example of how these ideas can be implemented.

The electron transport line employs an electrostatic accelerator Pelletron with the gun immersed into a longitudinal magnetic field. For the cathode radius of 2.5 mm, the field of 600 G on its surface was chosen to provide the magnetic flux sufficient to suppress the space charge drift motion inside the cooler (5). The magnetic field extends up to an end of the first acceleration section where it is already reduced to 200 G while the electrons have 0.43 MeV of the kinetic energy (see Eq.(7) and estimations after it).

When the electron beam exits this field region, it continues to be accelerated in the Pelletron, having 2 focusing kicks by thin solenoid lenses during the acceleration. After that, the beam is to be delivered to the cooling section. This part of the transport line includes two 90 degree bending blocks with solenoid lenses before and after every of them. To deliver the beam from the accelerator

to the cooling section, it must be turned in two different planes: first in the vertical and then in the horizontal. Each of the two mirror-symmetric blocks consists of two 45 degree bending magnets with a symmetric quadrupole triplet between them and two quadrupoles after (before) the resulting 90 degree bend. This construction allows to reach several goals.

- First, it allows to have zero dispersion downstream the block which is important both for the cooling conditions and for the electron beam stability. To eliminate dispersion, a 90-degree bend has to be separated into two halves with a focusing element inserted in between. In principle, this central focusing element could be either a solenoid, or a single quadrupole, or a symmetric triplet. The triplet is chosen because the required solenoid would be too heavy, while the single quadrupole would give too wide beam inside of the downstream dipole.
- Second, this bending scheme provides an invariant mapping for the whole bending block (the mapping is block-invariant). Beam parameters at the exit of the Pelletron cannot be current-independent. Thus, tunable optical elements are necessary in the beam line for beam matching (4). When the beam line consists of invariant blocks, these tunable elements can be solenoids only.
- Finally, the beam must be small enough inside the dipoles and other elements to suppress nonlinear aberrations.

The two solenoids between the bending blocks allows to have reasonable beam envelope for the second bending block and the matched beam radius at the entrance of the cooling section. The last solenoid upstream of the cooling section provides the zero radial divergence inside the cooler.

The electron transport simulations were done with the program OptiM [27] which is an interactive Windows application allowing a visual optics design. The beam envelopes from the exit of the gun solenoid to the beginning of the cooling section are presented in Fig. 3.

## VII. SUMMARY

The main purpose of this paper was to show how an electron beam for relativistic electron cooling can be transported by means of isolated focusing elements and bends, without any excitation of the cyclotron motion in the cooling solenoid. Introduced concepts of the angular momentum dominated beam and the effective beta-function showed the region of parameters where the lumped focusing can be used. For the beam lines consisted of the optically symmetric elements (local invariant lines), the two Courant-Snyder invariants were found and conditions for the beam matching between the cathode and the electron cooler were discussed.

For general kind of the beam lines, it was demonstrated that the beam matching can be formulated as uncoupling of the drift and the cyclotron canonic degrees of freedom under the beam transportation. For rotationally invariant mappings, it again leads to the same matching condition and temperature transformation as for the locally invariant case. Concept of a block-invariant line was introduced, general form of the invariant matrices was discussed, utility for the whole line that consists of invariant blocks was pointed. It was shown that any transformation can be transmuted to an invariant one by means of three free quadrupoles.

Generalized Busch's theorem was extended to the whole class of linear Hamiltonian systems. It was pointed out that according to this theorem, the identical matching condition is valid when any hydrodynamic round beam is transformed into round beam again. Possibilities were discussed to use initially flat beams converted into round in the cooler. A general condition on the initial beam state was formulated for having a magnetized beam in the cooler. As an example of application of the developed ideas, the electron transport scheme for the Fermilab cooling project was presented.

The described methods of matching between the solenoid of the cooling region and a rest of the electron beam track (with a round or flat beam) can also serve as guiding principles for a design of recirculators and storage rings for high energy electron cooling.

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FIG. 4. Designed layout of the electron cooling beam line at Fermilab.

Parameter	Value	Units
Electron Kinetic Energy	4.3	MeV
Electron Beam Current	0.5	A
Cathode Radius	2.5	mm
Gun Solenoid Field	600	G
Cooling Length	20	m
Cooling Solenoid Field	100	G
Beam Radius	6.1	mm
Electron Beam Angles	< 100	$\mu$ rad

TABLE I. Electron Cooling System Parameters

- [1] G. I. Budker, *Atomnaya Energiya (Soviet Atomic Energy)*, **22**(5), pp. 346-348 (1967).
- [2] G. I. Budker and A. N. Skrinsky, *Sov. Phys. Usp.* **21**, p. 277 (1978).
- [3] I. N. Meshkov, *Phys. Part. Nucl.*, **25**(6), p.631 (1994)
- [4] N. Dikansky, S. Nagaitsev and V. Parkhomchuk, "Electron beam focusing system", FERMILAB-TM-1998-H, Feb. 1996.
- [5] N. Dikansky et al., "Large Linac-Based Electron Cooling Device", *Proc. PAC'97*, p. 1795 (1997).
- [6] S. Nagaitsev, et al., "Status of the Fermilab Electron Cooling Project", *PAC-99*, 1, pp. 521-523, New York, 1999. S. Nagaitsev et al., "FNAL R&D in Medium-Energy Electron Cooling", *Proc. of ECOOL99*, NIM-A, **441**, (1-2), p.241 (2000).
- [7] P. Wesolowski, K. Balewski, R. Brinkmann, Y. Derbenev and K. Floettmann, "An Injector Study for Electron Cooling at PETRA", *ibid.*, p. 281.
- [8] N. Dikansky et al., *Part. Acc.* **7**, p. 197 (1976)
- [9] A. Burov, V. Danilov, Ya. Derbenev and P. Colestock, "Electron Cooling for RHIC", *Proc. of ECOOL99*, NIM-A, **441**, (1-2), p. 271 (2000).
- [10] Y. Derbenev, "Advanced Optical Concepts for Electron Cooling", *ibid.*, p. 223.
- [11] L. D. Landau and E. M. Lifshits, "The Classical Theory of Fields", Pergamon Press and Addison-Wesley (1987).
- [12] M. Reiser, "Theory and Design of Charged Particle Beams", J. Wiley & Sons, Inc. (1994)
- [13] A. Chao and M. Tigner, "Handbook of Accelerator Physics and Engineering", World Scientific, p.49 (1998).
- [14] H. Goldstein, "Classical Mechanics", Addison-Wesley, Mass., Second Edition, 1980.
- [15] V. I. Arnold, "Mathematical Methods of Classical Mechanics", Springer-Verlag (1984).
- [16] S. Nagaitsev and A. Shemyakin, "Emittance of Round Beams", Fermilab-TM-2107, 2000.
- [17] E. Pozdeev, private communication, 1995
- [18] E. A. Perevedentsev, private communication, 1995
- [19] V. V. Danilov and V. D. Shiltsev, "Round Colliding Beams", FERMILAB-FN-655, (1997).
- [20] P. T. Kirstein, G. S. Kino and W. E. Waters, "Space Charge Flow", McGraw-Hill Book (1967).
- [21] Y. Derbenev, "Adapting Optics for High Energy Electron Cooling", UM HE 98-04, University of Michigan (1998).
- [22] A. Burov and V. Danilov, "An Insertion to Eliminate Horizontal Temperature of High Energy Electron Beam", FERMILAB-TM-2043 (1998)
- [23] A. Burov, P. Colestock, V. Danilov Ya. Derbenev and S. Y. Lee, "Electron Cooling for Tevatron", private communication (1998).
- [24] K. Balewski, R. Brinkmann, Y. Derbenev, K. Floettmann and P. Wesolowski, "Studies of Electron Cooling at DESY", *Proc. of ECOOL99*, NIM-A, **441**, (1-2), p. 274 (2000).
- [25] P. Schwandt, "LISS: A 20 GeV Synchrotron/Storage Ring for Spin Physics", in *Proceed. of 16 RCNP Osaka International Symposium on Multi-GeV High Performance Accelerators & Related Technology*, p.185, World Scientific, 1997.
- [26] R. Brinkmann, Y. Derbenev and K. Floettmann, "A Flat Beam Electron Source for Linear Colliders", TESLA 99-09, DESY (1999).
- [27] V. A. Lebedev and S. A. Bogacz, "Betatron Motion with Coupling of Horizontal and Vertical Degrees of Freedom", at <http://host.sybercom.net/users/ldbs>; this site is a home of LDBS Co. developing the "OptiM" beam optics code.

